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Three-Dimensional Trapping and Dynamic Axial Manipulation with Frequency-Tuned Spiraling Acoustical Tweezers: A Theoretical Study

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Holographic acoustical tweezers based on Archimedes-Fermat spiraling interdigitated transducers (SIDTs) are a versatile tool for the selective manipulation of microparticles [Baudoin *et al.*, *Sci. Adv.* 5, eaav1967 (2019)] and cells [Baudoin *et al.*, *Nat. Commun.*, 11, 4244 (2020)] in a standard microfluidic environment. These binary active holograms produce some focused helical wave, with the ability to trap particles at the vortex core. Yet, all the studies conducted with SIDTs have so far been restricted to two-dimensional (2D) manipulation only. Here we show through a theoretical study that (i) a 3D radiation trap for microparticles and cells can be obtained with spiraling tweezers with sufficiently large aperture and that (ii) the particles can be displaced axially by simply tuning the driving frequency, without any motion of the transducer. This work opens perspectives for 3D cells and microparticles manipulation with single-beam acoustical tweezers.

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I. INTRODUCTION

The idea of manipulating objects with the acoustic radiation force was instilled by the early theoretical works of Rayleigh [1,2], Langevin [3,4], and Brillouin [5,6] on the acoustic radiation pressure and the calculations of the force applied by an acoustic field on a spherical particle [7–9]. Experimentally, some early demonstrations of particles trapping at the nodes and antinodes of standing waves depending on their properties were reported at the beginning of the twentieth century [10–12]. Since then, this principle has been refined, e.g., by combining high-frequency surface acoustic wave orthogonal transducers and microfluidics techniques to manipulate microparticles and cells in two dimensions in a microchannel [13,14], or by using static [15] or reconfigurable holograms [16–20] to pattern or manipulate many particles simultaneously in two and three dimensions. In acoustics, the term “acoustical tweezers” was introduced by Wu [21] in analogy with optical tweezers. But in this work, like in all the aforementioned works, the acoustical tweezers lack two essential features of their optical counterpart [22]: (i) *the selectivity*, i.e., the ability to select, trap, and manipulate a single object without affecting other neighboring objects and (ii) *three-dimensional trapping capability with a single beam*, i.e., the ability to produce a three-dimensional

(3D) trap from a beam produced from only one side of the manipulation chamber.

The selectivity requires that the spatial localization of the acoustic energy affects only the targeted object [23]. This localization can be achieved with focused beams, as investigated in optics [22] and later in acoustics [24]. But in acoustics, many particles of interest (in particular, those with positive contrast factors) are expelled, not trapped, at the center of a focused beam, or can be trapped only laterally at very specific frequencies close to the particle resonances [25]. To trap this type of particle, one possibility is to use acoustical vortices [23] (Bessel beams of topological order larger than or equal to one), some helical wavefields spinning around a phase singularity, investigated in acoustics by Hefner and Marston [26]. At first, the potential of cylindrical acoustical vortices to trap particles in two dimensions has been investigated both theoretically [27] and experimentally [28]. Such wavefields can be produced with an array of bulk [28–30] or surface acoustic wave transducers [31–33], passive holograms based on diffraction gratings [34–36], phase plates [37] and metamaterials [38], or finally active holograms based on spiraling interdigitated transducers (SIDTs) [39]. Transducer arrays have the advantage of producing reconfigurable acoustic fields, which can be controlled electronically to move the object. As a counterpart, these systems require a complex array of transducers, which can be complicated to manufacture at ultrasonic high frequencies due to cross-coupling and high-end costly electronics, which both severely limit the

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applicability of this method to trap microscopic particles. Passive holograms based on phased lens and diffraction gratings turn the signal produced by a single plane-wave transducer into the desired wavefield. The advantage is the simplicity of the system. But, due to the diffraction limit, the phased lens or diffraction grating engineering precision d should not be larger than half of the wavelength $d \leq \lambda/2$ [15], which severely limits the frequency range that can be achieved. The SIDTs on the other hand rely on spiraling electrodes patterned at the surface of a transparent piezoelectric substrate with classic photolithography techniques. Hence, they are flat, transparent, easily integrable in a microscope [39], and should enable vortex synthesis up to gigahertz frequency [40].

With tweezers based on cylindrical vortices, (i) the selectivity remains limited [23] since the beam is only focused laterally, leading to spurious secondary rings whose intensity decreases as $1/r^2$; (ii) particles can only be pushed or pulled [41–44] but not trapped in the axial direction, owing to the invariance of the intensity profile in this direction. Three-dimensional tweezers require that the particle is subjected to a restoring acoustic radiation force from all directions at the same time. These two problems (reduced selectivity and 3D trapping inability) can be addressed by using focused acoustical vortices or spherical vortices, as demonstrated theoretically [45] and later experimentally [46] by Baresch *et al.* in water. Levitation with vortex beams was also demonstrated in air by Marzo *et al.* [47], who also investigated the possibility offered by other types of beam such as twin and bottle beams. Applicability of these systems for in-vivo manipulation of millimeter-size objects in the urinary bladders of live pigs has recently been demonstrated [48], as well as the in-vivo collection of microbubbles within mouse capillaries [49].

Nevertheless these systems based on transducer arrays suffer the same limitations as those previously mentioned in the 2D case for micrometric objects in a standard microscopy environment. Jimenez *et al.* [50] and Baudoin *et al.* [51,52] demonstrated that focused vortices can be produced with passive Fresnel spiral zone plates and active SIDTs with Archimedes-Fermat geometry, respectively. In particular, Baudoin *et al.* [51,52] were able to synthesize high-frequency acoustical vortices and demonstrate selective trapping and displacement of microparticles [51] and cells [52] in a standard microscopy environment, with forces several orders larger than their optical counterparts [52]. Nevertheless, the 3D trapping capabilities of these SIDT-based tweezers were not investigated since the experiments were conducted in narrow microfluidic chambers with reduced axial dimension. Also, one difficulty with these integrated systems is that the transducers cannot be displaced axially to keep contact with the microfluidic chamber, hence preventing axial manipulation of the particles. Recently, it was shown in airborne experiments [53] that the focal point of a focused vortex synthesized

with a spiraling structure can be moved axially by tuning the activation frequency, while also leading to some slight distortion of the acoustical vortex.

In this paper, we theoretically show that (i) a 3D radiation trap for microparticles and cells can be produced with single beam SIDT tweezers and that (ii) the 3D trap is maintained and displaced axially when tuning the driving frequency.

II. METHOD: ANGULAR SPECTRUM BASED CALCULATION OF THE 3D ACOUSTIC RADIATION FORCE

The 3D radiation force applied on a microparticle by an acoustic field produced by Archimedes-Fermat spiraling transducers is calculated with an in-house code [52] based on the angular spectrum method (ASM) originally introduced by Sapozhnikov and Bailey [54]. An outline of this method and a comparison to other existing formulas [27,55] of the 3D acoustic radiation force applied on a particle of arbitrary size is discussed in Ref. [56].

The flowchart for using ASM to compute the wave propagation is given and discussed in detail in Appendix A. Here, we briefly review the ASM-based radiation force formulas. The incident field in a source plane is decomposed into a sum of plane waves using the angular spectrum decomposition (the 2D spatial Fourier transform of the incident field). Then the known decomposition of plane waves into spherical harmonics and the Legendre addition theorem are used to express the incident field in the spherical harmonics basis weighted by the ASM-based beam shape coefficients H_{nm} :

$$p_i = \frac{1}{\pi} \sum_{n=0}^{\infty} \sum_{m=-n}^n i^n H_{nm} j_n(kr) Y_n^m(\theta, \varphi) \quad (1)$$

with

$$H_{nm} = \iint_{k_x^2 + k_y^2 \leq k^2} S(k_x, k_y) Y_n^{m*}(\theta_k, \varphi_k) dk_x dk_y. \quad (2)$$

Here $S(k_x, k_y)$ is the so-called angular spectrum, $j_n(kr)$ and Y_n^m are respectively the spherical Bessel function of the first kind and the spherical harmonics, k_x and k_y are the wavevector (\mathbf{k}) components in the x and y directions with the relations to angles $\cos \theta_k = [1 - (k_x^2 + k_y^2)/k^2]^{1/2}$ and $\varphi_k = \arctan(k_y/k_x)$.

The scattering problem is solved by using known results for planed waves [54,57], leading to

$$p_s = \frac{1}{\pi} \sum_{n=0}^{\infty} \sum_{m=-n}^n i^n H_{nm} A_n^m h_n^{(1)}(kr) Y_n^m(\theta, \varphi), \quad (3)$$

where $h_n^{(1)}$ is the spherical Hankel function of the first kind and the A_n^m are the partial wave coefficients, which

depend on the acoustic materials and geometric shape of the scatterer, and the boundary condition between the fluid and the particle. Finally, the force is obtained by integrating Brillouin's tensor [5] on a still surface in the far field

[58,59], leading to the equations of the 3D radiation force applied on a sphere in an arbitrary acoustic field obtained by Sapozhnikov and Bailey [54] and slightly recast here under the form [56]

$$F_x = \frac{1}{4\pi^2 \rho_0 k^2 c_0^2} \operatorname{Re} \left\{ \sum_{n=0}^{\infty} \sum_{m=-n}^n C_n (-b_{n+1}^{-m} H_{nm} H_{n+1,m-1}^* + b_{n+1}^m H_{nm} H_{n+1,m+1}^*) \right\}, \quad (4a)$$

$$F_y = \frac{1}{4\pi^2 \rho_0 k^2 c_0^2} \operatorname{Im} \left\{ \sum_{n=0}^{\infty} \sum_{m=-n}^n C_n b_{n+1}^m (H_{n,-m} H_{n+1,-m-1}^* + H_{nm} H_{n+1,m+1}^*) \right\}, \quad (4b)$$

$$F_z = -\frac{1}{2\pi^2 \rho_0 k^2 c_0^2} \operatorname{Re} \left\{ \sum_{n=0}^{\infty} \sum_{m=-n}^n C_n c_{n+1}^m H_{nm} H_{n+1,m}^* \right\}, \quad (4c)$$

where $C_n = A_n + 2A_n A_{n+1}^* + A_{n+1}^*$, $b_n^m = \sqrt{[(n+m)(n+m+1)]/[(2n-1)(2n+1)]}$, $c_n^m = \sqrt{[(n+m)(n-m)]/[(2n-1)(2n+1)]}$, and ρ_0 and c_0 are the density and sound speed in the outside fluid medium. Note that here the partial wave coefficients A_n^m reduce to A_n owing to the spherical shape of the particle.

III. THREE-DIMENSIONAL TRAPPING WITH SIDT-BASED TWEEZERS

A. HAT design and acoustic field

Most particles of interest for microfluidic applications (e.g., solid microparticles) and biological applications (e.g., cells in water) are stiffer and denser than the surrounding medium and cannot be trapped in three dimensions with a one-sided focused beam [25].

Three-dimensional selective trapping of such particles requires specific wavefields such as focused acoustical vortices [23]. Here we investigate the trapping capabilities of focused one-sided vortex beams resembling the fields synthesized by the SIDTs used in Refs. [51,52,57]. The focused vortex is produced by two Archimedes-Fermat spiraling electrodes of inverse polarity obtained by discretizing the intersection of an acoustical vortex with a plane on two phase levels. The exact transducer geometry

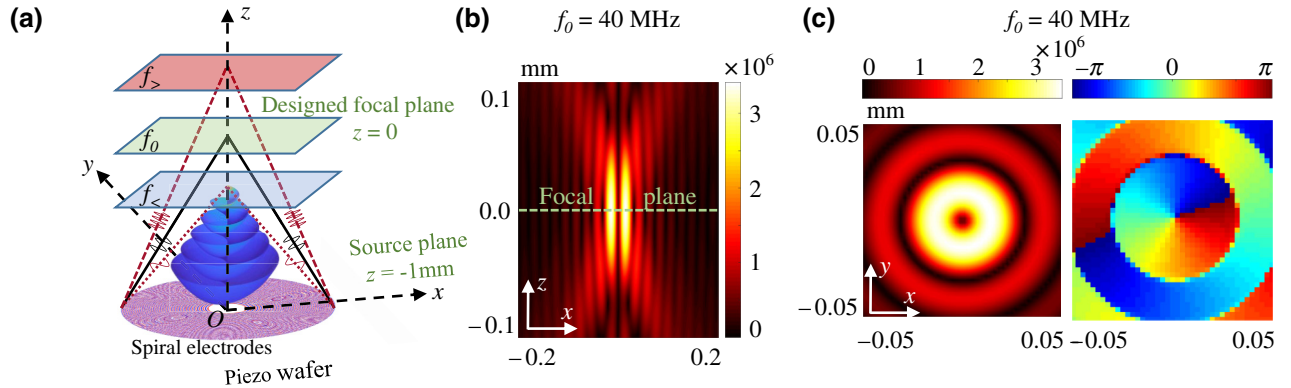


FIG. 1. Field produced by a one-sided holographic acoustical tweezer (HAT) designed to synthesize a focused vortex configuration. (a) The HAT is made of two intertwined spiraling electrodes of inverse polarity whose equations are given in Appendix B. It is designed to synthesize a focused vortex at the original driving frequency $f_0 = 40$ MHz (wavelength $\lambda = 37.5 \mu\text{m}$) and focal plane at heights $z = 0, 1$ mm away from the source plane $z = -1$ mm. The origin in the lateral plane is located at point O that is the center of the spiraling electrodes. The focal plane along the propagation direction can be changed by changing the actuation frequency. When the excitation frequency $f_>$ is higher than the designed frequency f_0 , i.e., $f_> > f_0$, the focal plane moves away from the source plane, while when $f_< < f_0$, the focal plane moves closer to the source plane. (b) Pressure amplitude in the propagation plane ($x, y = 0, z$) at actuation frequency f_0 . (c) Pressure amplitude and phase in the focal plane ($x, y, z = 0$) at actuation frequency f_0 .

and source field used in the present simulations are given in Appendix B and the resulting acoustic field is represented in Fig. 1. The transducer is designed to produce a focused vortex with an aperture of 65° and a focal plane located 1 mm away from the transducer when actuated at the original frequency $f_0 = 40$ MHz. The pressure amplitude in the propagation plane ($x, y = 0, z$) and the focal plane ($x, y, z = 0$) are represented in Figs. 1(b) and 1(c), respectively.

We now investigate (i) the ability of such an acoustic field to trap a particle or a cell in three dimensions at the original frequency f_0 and (ii) the evolution of the trap when the excitation frequency is slightly shifted away from f_0 .

B. 3D cell trapping

The 2D trapping capability of the SIDTs for cells has recently been verified both theoretically and experimentally [52]. Here we investigate the 3D trapping capabilities. The simulations are performed for a cell immersed in water and insonified by an acoustical vortex synthesized at the driving frequency $f_0 = 40$ MHz by a binary spiraling hologram. The maximum pressure amplitude in the focal plane ($z = 0$ mm) is 3.4 MPa. The cell is assimilated to a spherical liquid scatterer whose acoustical properties are provided in Table I and correspond to typical values provided in Ref. [60].

The computed normalized lateral acoustic radiation force (ARF) versus x and axial ARF versus z for a cell with different radii $a = 1, 5, 9, 13,$ and $17 \mu\text{m}$ are calculated and represented in Figs. 2(a) and 2(b), respectively. Note

TABLE I. Acoustic properties.

Material	Density ρ (kg/m^3)	Longitudinal speed of sound c_l (m/s)	Shear speed of sound c_t (m/s)
Cell	1100	1508	...
Pyrex	2230	5640	3280
Water	1000	1500	...

that the lateral force is computed at the axial trap equilibrium position z_{trap} . In addition, the effective restoring forces versus cell radii a in the lateral and axial directions are represented in Figs. 2(c) and 2(d). The effective restoring force is the smallest absolute value of the two positive and negative radiation force extrema located at two sides of the trapping position. These graphs show that the SIDT-based HATs produce a lateral trap for cells with radius up to $a = 17 \mu\text{m}$ (0.45λ), even larger than the radius of the maximum first ring (0.36λ) in the lateral direction, while an axial trap is obtained for radii up to $a = 13 \mu\text{m}$ (0.35λ). That is, the designed HATs produce a 3D radiation trap of the considering typical cell with radius up to $\min\{0.35\lambda, 0.45\lambda\} = 0.35\lambda$. Note that in Fig. 2(b), the axial trapping position is shifted away from the source plane when the size of the cell is increased. Indeed, for small cells (see $a = 1, 5,$ and $9 \mu\text{m}$), the gradient force is dominant and the scattering force is negligible [61]. So the cells are trapped at or near the focal point. When the radius of the cell is increased, the scattering force can no longer be neglected and will push the cell along the propagation direction. The restoring force nevertheless remains sufficient to balance the pushing force for cells smaller than

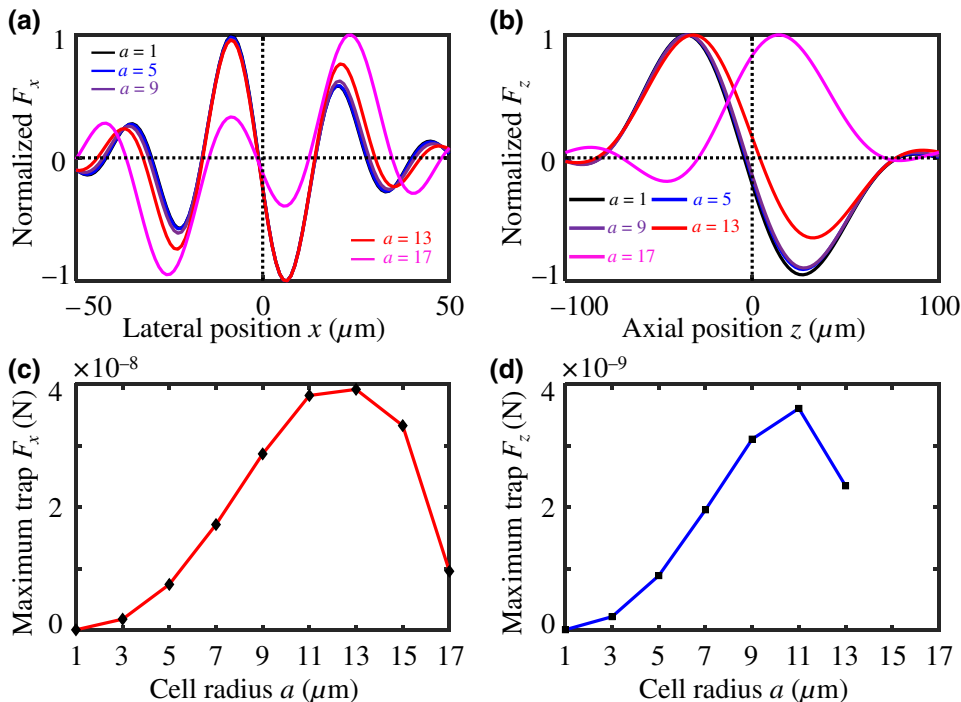


FIG. 2. Three-dimensional cell trapping with a spiraling one-sided HAT driven at the frequency $f_0 = 40$ MHz. The cell is modeled as a liquid sphere with typical acoustical parameters given in Table I. (a) The normalized lateral force versus x position (at axial equilibrium position) and (b) the normalized axial force versus z position for cells with different radii a . The radius of the first ring of maximum intensity of the acoustical vortex is $13.6 \mu\text{m}$ [see Fig. 1(c)], corresponding to 0.36λ . (c) The maximum lateral and (d) axial trapping (effective restoring) forces for cells with radii ranging from $a = 1$ to $17 \mu\text{m}$. Only the stable trapping sizes are represented. The axial trap is lost for cell radii $a = 15$ and $17 \mu\text{m}$.

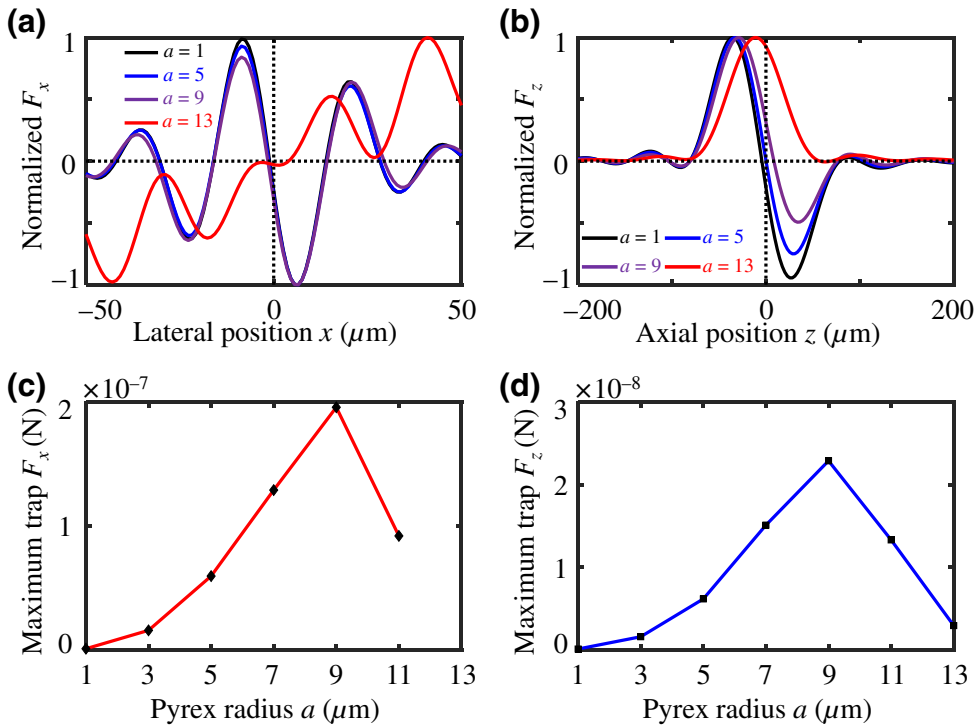


FIG. 3. Three-dimensional Pyrex microparticle trapping with a vortex-based one-sided HAT at the designed frequency $f_0 = 40$ MHz with different radii a . The Pyrex is modeled as an elastic sphere without consideration of the viscosity. The acoustical parameters are given in Table I. (a) The normalized lateral force versus x (at the axial equilibrium position) and (b) the normalized axial force versus z position for particle radii $a = 1, 5, 9,$ and 13 μm . (c),(d) The maximum trapping (effective restoring) force for particle radii ranging from $a = 1$ to 13 μm . The lateral trapping is lost for Pyrex radius $a = 13$ μm at the axial equilibrium position $z_{\text{trap}} = 57.5$ μm .

0.35λ , but the equilibrium position is shifted towards the beam direction of propagation (see $a = 13$ and 17 μm). When the radius is further increased, the cell will escape from the trap.

Note that the axial trapping forces calculated here for a realistic acoustic field are several orders of magnitude larger than the force resulting from the balance between gravity and buoyancy [4.2×10^{-15} Newton (N) for radius $a = 1$ μm , and 9.2×10^{-12} N for radius $a = 13$ μm]. In a flowing microchannel configuration, additional drag forces could also affect the trapping. Hence, it is insightful to compare the acoustic radiation force to the drag force magnitude. For typical velocities in a microchannel of $v_f = 5$ to 500 $\mu\text{m/s}$ [62,63], the drag force $F_d = 6\pi\mu av_f$ (with μ the dynamic viscosity) applied to a cell of radius $a = 11$ μm lies in the order of 1 to 100 pN, which remains significantly smaller than the acoustic radiation force computed here for a pressure level of 3.4 MPa in the focal plane. Note that in Ref. [52] cells were moved (at lower pressure levels) at maximum velocities of 1.2 mm s^{-1} , which corresponds to trapping forces of the order of 200 pN. These calculations and experiments show that the acoustic radiation force is sufficient to manipulate cells in flowing microchannels at moderate flow rates.

C. Three-dimensional Pyrex trapping

In this section, we investigate 3D trapping of spherical Pyrex particles with radii from $a = 1$ to $a = 13$ μm in water with the same acoustic field as that used in the previous section for cell trapping. Since Pyrex support

both longitudinal and transverse waves, an elastic scattering model is considered [46,61]. The acoustic properties of Pyrex used for the simulations are given in Table I. The normalized lateral and axial radiation forces versus the respective positions are given in Figs. 3(a) and 3(b), with the maximum lateral and axial trapping (restoring) forces versus particle radii a given in (c) and (d), respectively. These results show 3D Pyrex particle trapping for radii up to $a = 11$ μm [0.29λ ; see Figs. 3(c) and 3(d)], with a maximum for both lateral and axial trapping obtained around $a = 9$ μm . It is interesting to note that the lateral trapping at the axial equilibrium position z_{trap} is lost for $a = 13$ μm since the axial trapping position is far away ($z_{\text{trap}} = 57.5$ μm) from the designed focus by the large pushing scattering force. Similarly to cells, the gravity effect on a Pyrex sphere is negligible compared to the radiation force since the balance between gravity and buoyancy leads to net forces of 5.2×10^{-14} N for a radius of $a = 1$ μm , and 6.9×10^{-11} N for a radius of $a = 11$ μm .

Note that the influence of the aperture on the 3D trapping capabilities of the tweezers for both Pyrex particles and cells are discussed in Appendix C.

IV. AXIAL DISPLACEMENT OF THE TRAP BY FREQUENCY TUNING

A. Axial displacement of the focal point

The 3D trapping ability of spherical focused vortices produced by HATs has been verified in Sec. III. Now we investigate what happens to the trapping equilibrium position when the actuation frequency of the HAT is tuned,

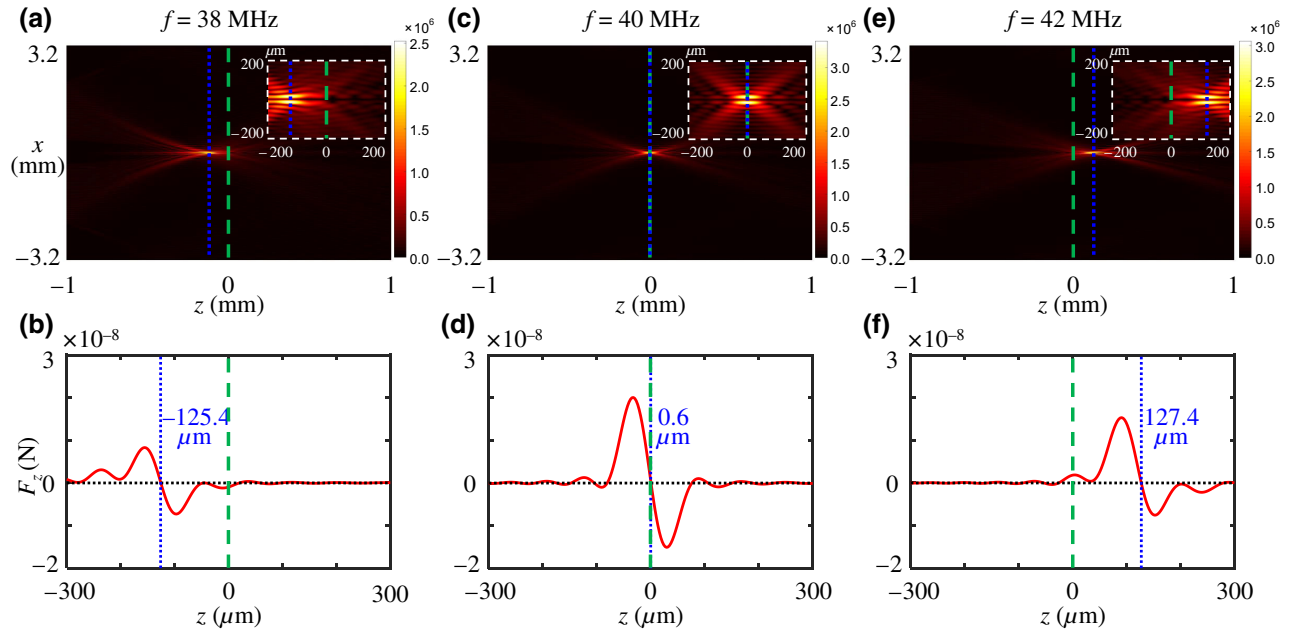


FIG. 4. (a),(c),(e) The acoustic pressure amplitude in the propagation plane ($x, y = 0, z$) with different activated frequencies $f = 38, 40,$ and 42 MHz, respectively. Enlarged insets including the focal plane are shown in the top right corners. (b),(d),(f) The axial radiation force versus different z positions for a Pyrex particle with radius $a = 7 \mu\text{m}$. The Pyrex particle can be trapped in three dimensions (the lateral force versus x position is not shown here for brevity) and the axial equilibrium position is changed with different activated frequencies. The green dashed line describes the originally designed axial focal position ($z = 0$) at $f_0 = 40$ MHz, while the blue dotted line indicates the actual axial position of the focal plane. The effective restoring force decreases when the excitation frequency deviates away from f_0 , e.g., $f = 38$ and 42 MHz.

while keeping the geometric shapes of the IDTs identical. Indeed, recent airborne investigations by Muelas-Hurtado *et al.* [53] revealed that slight frequency tuning of the excitation of a spiraling HAT induce an axial translation of the position of the focal plane, combined with a distortion of the beam since the equations of the Archimedes-Fermat spirals [51] are not invariant by a change in the tuned frequency. However, they did not study the trapping capabilities of these beams and whether the distortion remains sufficiently limited to maintain a 3D trap.

As illuminated in Fig. 1(a), the focal plane is moved toward the source plane (i.e., focal depth decreases) when the excitation frequency $f < f_0$ [see Fig. 4(a) for $f = 38$ MHz], and away from it when $f > f_0$ [see Fig. 4(e) for $f = 42$ MHz].

B. Axial displacement of Pyrex particles

In this section, radiation force simulations are conducted for a Pyrex spherical particle of radius $a = 7 \mu\text{m}$, so that the lateral and axial trapping forces are large and the restoring force around the equilibrium position is more symmetrical (compared to the case $a = 9 \mu\text{m}$). The axial radiation force versus axial position z near the designed focus ($z = 0$) for the excitation frequencies $f = 38, 40,$ and 42 MHz are represented in Figs. 4(b), 4(d), and 4(f), respectively. The Pyrex sphere can be trapped axially at

the new focal plane at $z_{\text{trap}} = -125.4 \mu\text{m}$ for $f = 38$ MHz, and at $z_{\text{trap}} = 127.4 \mu\text{m}$ for $f = 42$ MHz. The axial translation of the trapping point for these two cases is of the order of $18a$, which is large enough for axial control of a particle in a microchannel. Lateral trapping at the axial equilibrium position z_{trap} (not shown here for the sake of brevity) is also fulfilled since the main energy is localized near the focal plane with a large intensity gradient. Hence, these simulations demonstrate controllable axial displacement of trapped Pyrex particles when tuning the excitation frequency.

We further conducted a systematic analysis of the axial translation of the trapping positions and effective restoring forces versus the excitation frequency within the regime $f = [32, 45]$ MHz [see Figs. 5(a) and 5(b), respectively]. When the excitation frequency is close to the designed frequency $f_0 = 40$ MHz, the trapping position z_{trap} linearly depends on the excitation frequencies (see the regime of $[37, 43]$ MHz), while outside this range, the trend is no longer linear due to a large distortion of the acoustic vortex. Meanwhile, the effective restoring force F_z is maximum at the designed frequency $f_0 = 40$ MHz, and then drops rapidly and nearly symmetrically when the excitation frequency is larger or smaller than f_0 , down to less than $1/6$ of its maximum value outside the $[37, 43]$ MHz range. Hence, the range of interest for practical application (linear and hence predictable displacement and sufficient

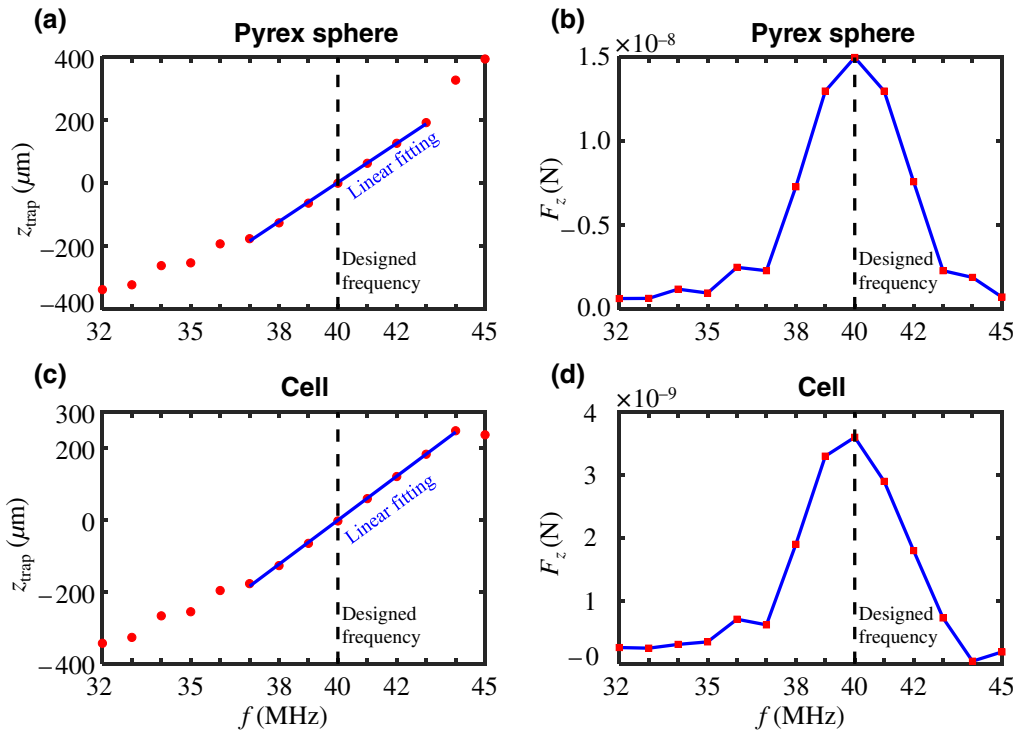


FIG. 5. The axial trapping positions (z_{trap}) along the z direction and the effective restoring force F_z versus excitation frequencies for (a),(b) Pyrex spherical particles with radius $a = 7 \mu\text{m}$ and (c),(d) cells with $a = 11 \mu\text{m}$. The excitation frequencies are selected near the designed frequency $f_0 = 40$ MHz from $f = 32$ MHz to $f = 45$ MHz. In the regime of [37, 43] MHz for (a) the Pyrex sphere, and of [37, 44] MHz for (c) the cell, the axial trapping position z_{trap} agrees exactly with the linear fitting (blue solid line). The effective restoring forces F_z drop when the excitation frequencies are away from f_0 .

axial trapping force) is the [37,43] MHz interval. In this range, the displacement is about $400 \mu\text{m}$, that is, more than 100 times the size of the particle, and 10 times the wavelength.

C. Axial displacement of cells

We conducted a similar analysis for cells with radius $a = 11 \mu\text{m}$ [see Figs. 5(c) and 5(d)]. The analysis shows that cells can also be moved, while keeping a 3D trap when the frequency is tuned in the range $f = [32, 45]$ MHz. This leads to a maximum displacement range of about $650 \mu\text{m}$ with a linear trend observed in the regime $f = [37, 44]$ MHz, which is more than 57 times the size of the cell, and 16 times the wavelength. The trapping radiation force is maximum at the designed frequency $f_0 = 40$ MHz and drops with the excitation frequency away from f_0 , which is similar to the Pyrex particle case.

V. CONCLUSION AND PERSPECTIVES

This work theoretically demonstrates the ability to obtain a 3D acoustic radiation trap for both elastic microparticles and cells with realistic acoustic fields mimicking that produced with spiraling interdigitated transducers. This extends to three dimensions the manipulation possibilities offered by spiraling interdigitated transducers [23,51,52]. In addition, we also demonstrate that the positions of the 3D trapped cells and microparticles can be moved axially in a predictable manner by tuning the excitation frequency near the original frequency used for the design of the spiraling transducers. The magnitude of the

displacement that can be achieved is 2 orders of magnitude larger than the particle radius and more than an order of magnitude larger than the wavelength. This opens possibilities for axial displacement of the trapped particle by a simple shift of the driving frequency without any moving part. This is critical since, for manipulation in microchannels, the tweezers cannot be moved axially. The next steps include (i) experimental verification of these predictions and (ii) investigation of the role played by Eckart streaming [64] and the resulting drag, especially for particles with low acoustic contrast such as cells. From an experimental perspective, some holographic acoustical tweezers based on the Archimedes-Fermat spiral have already been studied in Ref. [52] at 40 MHz. The main challenge to obtaining unequivocal results on 3D trapping and axial manipulation is performing the experiments in a large chamber with absorbing walls to avoid spurious reflections by the walls that could affect the acoustic trap.

Another interesting path would be to investigate fields with optimized properties for 3D trapping and frequency shift driven displacement. Indeed, acoustical vortices combine many interesting properties: they can be synthesized with a 2D phase hologram, enable 3D trapping, and, as shown in this paper, enable z displacement by switching the active hologram driving frequency. But they also have some drawbacks, such as an axial trapping force one order of magnitude weaker than the lateral force. Some other types of beam have been studied in the literature for 3D trapping, such as bottle beams (see, e.g., Refs. [47,65] in acoustics). These beams exhibit, on the opposite, larger axial force and weaker lateral force. Marzo *et al.* [47] also

conducted some optimization procedure to determine optimal fields in the long wavelength regime. But the design of the optimal acoustic field for 3D selective particle trapping beyond this regime still remains an open problem. Also, the addition of interesting frequency-driven displacement properties to a static hologram essentially remains unexplored.

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APPENDIX A: ANGULAR SPECTRUM METHOD

The schematic to understand how to use ASM to calculate the wave propagation in free space is given in Fig. 6. Assume that we know the acoustic pressure field in the source plane or a plane parallel to the source plane, then angular spectrum $S(k_x, k_y)|_{z=0}$ (e.g., at source plane) is easily obtained by using the 2D fast Fourier transform inverse fast Fourier transform (IFFT), which is related to the ASM-based beam shape coefficients H_{nm} [see Eq. (2)]. To calculate the radiation force according to Eqs. (4a)–(4c), it is convenient to expand the incident beam at the origin of the scatterer (x_s, y_s, z_s) . The propagation of the acoustic field from the source to the scatter plane is calculated by using

the propagation factor in Fourier space:

$$S(k_x, k_y)|_{z=z_s} = S(k_x, k_y)|_{z=0} e^{ik_x x_s + ik_y y_s + i\sqrt{k^2 - k_x^2 - k_y^2} z_s}. \quad (\text{A1})$$

This can be used to calculate the ASM-based beam shape coefficients H_{nm} at the scatterer center and further the 3D radiation force. Note that in this paper the viscous attenuation of the wave is not considered in the angular spectrum propagator. At the working frequency (40 MHz) in water at room temperature, the acoustic attenuation length [66] $L_a = 2\rho_0 c_0^3 / [\omega^2 (4/3\mu_s + \mu_b)] \sim 26$ mm, which is much larger than the designed focal depth (about 1 mm). Since the wave amplitude decreases with the propagation distance as e^{-z/L_a} , the pressure magnitude will lose about 3.8% amplitude between the source and the focal plane, which is significant but does not modify the orders of magnitude presented in this paper. Note also that the real pressure field, including the amplitude and phase at the scatter plane, can be obtained by using the 2D inverse Fourier transform (IFFT) of the angular spectrum $S(k_x, k_y)|_{z=z_s}$.

APPENDIX B: PRINCIPLE OF FOCUSED-VORTEX-BASED ACOUSTICAL TWEEZERS

It is difficult to produce an ideal spherical vortex in experiment since the transducers need to be placed all over the 4π steradians enclosing the manipulation area [61]. However, this can be overcome by using a focused spherical vortex with finite aperture (steradian less than 2π) [45,51,52,67]. Similarly to the plane standing waves consisting of two counterpropagating traveling waves, a spherical Bessel beam can be produced by the interference of converging and diverging spherical Hankel beams. This agrees with the mathematical fact that a Bessel function can be written as the addition of Hankel functions of the first and second kinds (with a ratio of 1/2). To coincide with the radiation force derivations [44,56], the time harmonic here is chosen as $e^{-i\omega t}$ so that the converging Hankel vortex is described by the spherical Hankel function of the second kind $h_n^{(2)}$. An ideal converging Hankel spherical vortex is described in spherical coordinates (r, θ, φ) as [51]

$$p^*(r, \theta, \varphi) = p_0 h_n^{(2)}(kr) P_n^m(\cos \theta) e^{i(m\varphi - \omega t)}, \quad (\text{B1})$$

where p_0 is the wave amplitude and the P_n^m are the associated Legendre functions of order (n, m) . Following the same procedure as in Ref. [51] and using the far-field asymptotic expression $h_n^{(2)}(kr) \simeq i^{(n+1)} e^{-ikr} / (kr)$, the geometrical shapes of the two spiral electrodes can be

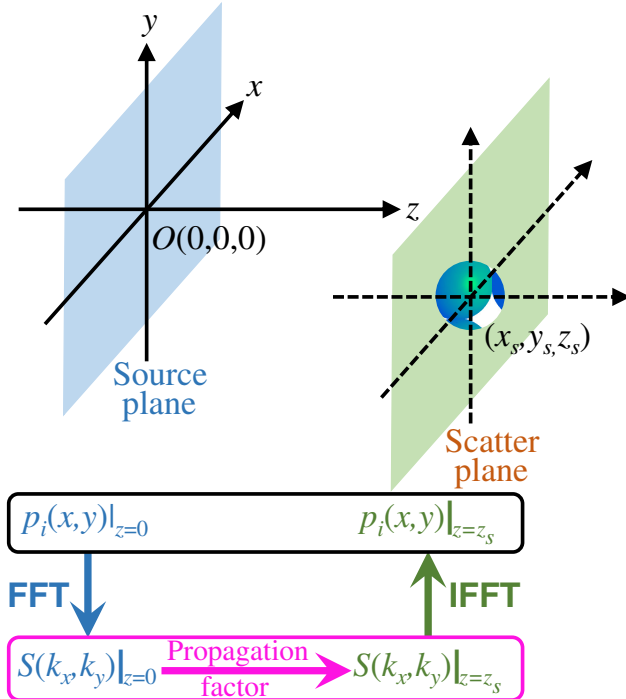


FIG. 6. Flowchart of the angular spectrum method. The acoustic pressure in the black box lies in real physical space and can be measured in experiment, while the angular spectrum in the magenta box lies in Fourier space.

described in cylindrical coordinates (R, φ, z) as

$$R_1 = \frac{1}{k} \sqrt{(\varphi + C_2)^2 - (kz)^2}, \quad (\text{B2})$$

$$R_2 = \frac{1}{k} \sqrt{(\varphi + C_2 + \pi)^2 - (kz)^2}, \quad (\text{B3})$$

where $m = 1$ is for the first-order vortex and C_2 is a constant. The geometrical shapes described by R_1 and R_2 [see, e.g., Fig. 7(a)] are obtained by extracting the intersection between the Hankel beam isophase surfaces and a plane. The phase shift π is applied here for the two isophase shapes R_1 and R_2 since it is easy to achieve by a piezoelectric transducer with positive and negative electrodes. If we set a focal depth (z) for a given frequency (or wave number k), the aperture radius and angle can be defined by choosing appropriate azimuthal angle regimes φ (also the number of spiral turn N) according to Eqs. (B2) and (B3).

APPENDIX C: ROLE PLAYED BY THE APERTURE

In the expressions of the two spiral electrodes given in Eqs. (B2) and (B3), the minimum and maximum azimuthal angles φ_{\min} and φ_{\max} , which determine the aperture angle of the HAT, can be chosen arbitrarily. For manipulation in microscopes, the minimum angle can be chosen to leave some space for observation near the central axis since generally the electrodes are not transparent [51]. The maximum azimuthal angle proportional to the number of spiral turns plays an important role in the axial and lateral trapping capabilities. Here, lateral and axial trapping forces for different numbers of spiral turns with the corresponding aperture radii and angles are given in Table II and three selected patterns are given in Fig. 7(a). The axial radiation force versus the axial position z for a cell with radius $a = 11 \mu\text{m}$ is given in Fig. 7(b), and for a Pyrex sphere with $a = 9 \mu\text{m}$ in Fig. 7(c). The axial trapping force increases with increasing aperture angle. For all the numbers of turns discussed, the cell can be trapped in three

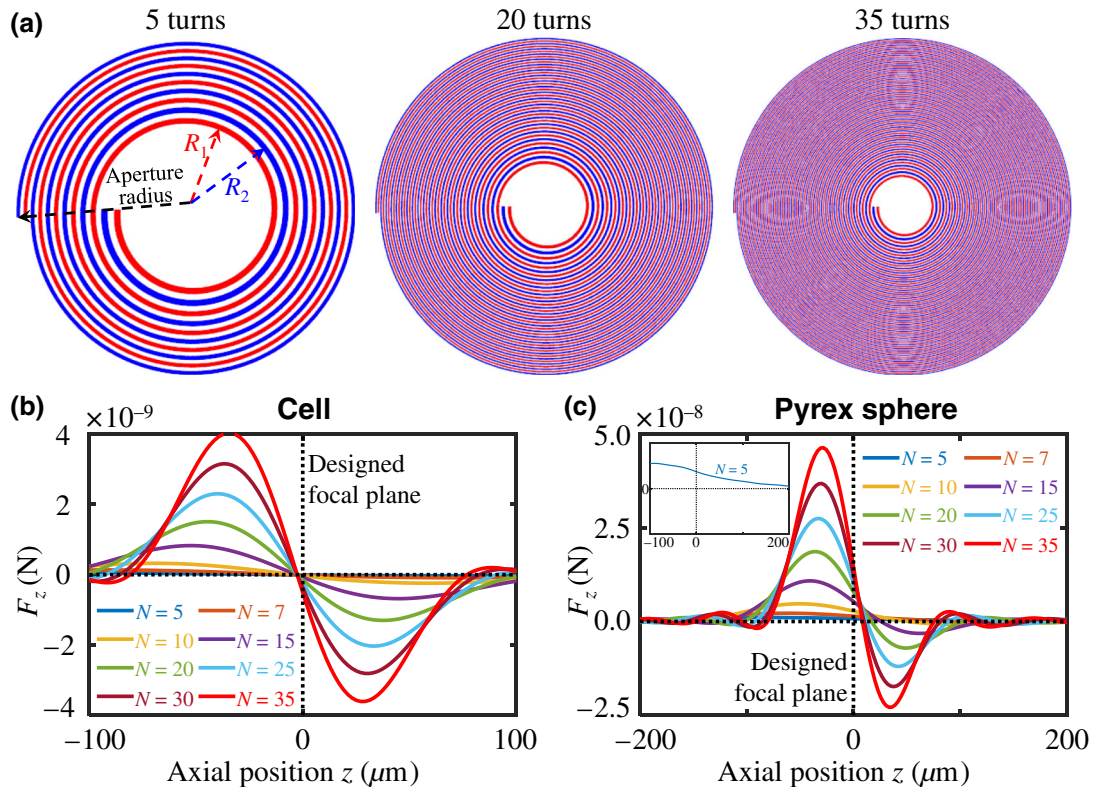


FIG. 7. (a) Geometric shapes of spiral electrodes (IDTs) with different numbers of turns. The aperture radius is the maximum radius of R_1, R_2 , as indicated by the black dashed line. The aperture angle is computed by the arctangent value of the aperture radius over the designed focal depth. The axial radiation force F_z versus different positions z for (b) a cell with radius $a = 11 \mu\text{m}$ and (c) a Pyrex sphere with $a = 9 \mu\text{m}$, with a focused-vortex-based acoustical tweezer at frequency $f_0 = 40$ MHz with different numbers of spiral turns. The scattering force contribution is relatively strong for a Pyrex sphere (elastic model) than for a cell (liquid model). The axial trapping positions for the cell are almost the same, while those for the Pyrex move closer to the designed focal position as the number of spiral turns increase, leading to the increase of focused ability (hence, gradient force). The gravity effect could be ignored compared to the trapping force.

TABLE II. Number of spiral turns N for acoustical tweezers with the same focal length 1 mm and related aperture angles.

	N							
	5	7	10	15	20	25	30	35
Aperture radius (mm)	0.74	0.86	1.02	1.27	1.50	1.72	1.94	2.15
Aperture angle (deg)	36	41	46	52	56	60	63	65

dimensions, while for the Pyrex sphere, the axial trap is lost for the case with five turns [see the enlarged inset in Fig. 7(c)]. Indeed, the acoustic impedance of cells is smaller than that of Pyrex, leading to a weaker scattering contribution that will push the cell or particle outside of the trap center. In addition, the axial trapping position z_{trap} moves closer to the designed focal plane when the number of turns increases. This is because the restoring gradient force is enhanced more than the pushing scattering force.

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