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A Comparative Study of Characteristic Finite Element and Characteristic Finite Volume Methods for Convection-Diffusion-Reaction Problems on Triangular Grids

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Abstract

The paper aims to compare the accuracy and robustness of the characteristic finite element method (CFEM) and characteristic finite volume method (CFVM) for solving convection-diffusion-reaction problems on two-dimensional triangular grids. The tests are performed on a square unit domain, to which an advective field is imposed in a domain. The results show that the CFEM gives less accurate solution than CFVM for the rotation of a slotted-cylinder and rotation of Gaussian cone problems. Moreover, CFEM gives oscillate solution while the CFVM provides an oscillation-free solution for the skew flow to the mesh problem.

Keywords: Characteristic Finite Element Method, Characteristic Finite Volume Method, Convection-Diffusion-Reaction, Triangular Grids

1 Introduction

Many science and engineering applications require the simulation of time-dependent convection-diffusion-reaction equations. The convection is defined as the movement of substance due to the fluid transport medium, the diffusion is referred to the dispersion of a substance involved in the process throughout the physical domain of the problem, and the reaction is the process of interaction through which the substances are generated or consumed. Generally, the scale of the diffusion is smaller by several orders of magnitude compared to the size of the advective flow field. A main feature of the convection- and reaction-dominated is the presence of the sharp layers as a part of the solution. The accurate simulation of such processes requires numerical methods such that able to compute sharp layers without an occurrence of spurious oscillations.

The standard Galerkin finite element method usually yields oscillatory solutions for convection-dominated problems [1]. Many methods have been proposed to overcome the instability and inaccuracy of the solution. The shock-capturing procedure [2] is the usual remedy

for these difficulties. Among the stabilizing schemes, the characteristic Galerkin scheme has been developed by applying the time-stepping technique as the basis [3,4]. The explicit characteristic Galerkin scheme based on the Taylor series expansion is an attractive one due to its simple implementation and fast calculation. The scheme uses a characteristic approximation to trace advection in time and combine with a low-order mixed finite element spatial approximation of the equation. Moreover, the scheme is locally conservative on the discrete level such that fluid is transported along with the approximate characteristics.

Recently, the author proposed an explicit characteristic finite volume method that can provide stabilized numerical solutions for pure advection and advection-dominated diffusion problems [5-7]. The idea of the characteristic-based scheme is used to discrete the Lagrangian derivative as the function of time. An explicit finite volume method based on the cell-centered scheme is employed to derive the discretized equations. The Galerkin finite element technique is applied to estimate the gradient quantities at the cell faces. The finite volume method is applied to discretize the equation because of it some of the important features. Firstly, it may be used on arbitrary geometries, using structured or unstructured grids. Secondly, it is the local conservativity of the numerical fluxes, that is the numerical flux is conserved from one discretization cell to its neighbor [8].

The objective of this research work is to compare the computational efficiency of the CFEM and CFVM for solving two-dimensional convection-diffusion-reaction problems on structured triangular grids. The paper is organized as follows. In Section 2, the governing equations and numerical formulations are presented. Then, the schemes are examined by three benchmark test cases to evaluate their accuracy and robustness in Section 3.

2 The Numerical Scheme

2.1 The characteristic convection-diffusion-reaction equation

The governing differential equation for the two-dimensional convection-diffusion-reaction equation is

$$\frac{\partial \phi}{\partial t} + \nabla \cdot (\mathbf{v} \phi - \varepsilon \nabla \phi) + \kappa \phi = 0 \quad \text{in } \Omega \times T \quad (1)$$

subject to the boundary conditions

$$\phi = g_D \quad \text{in } \partial\Omega_D \quad (2)$$

$$\varepsilon \frac{\partial \phi}{\partial \mathbf{n}} = g_N \quad \text{in } \partial\Omega_N \quad (3)$$

with $\partial\Omega = \partial\Omega_D \cup \partial\Omega_N$ with $\partial\Omega_D \cap \partial\Omega_N = \emptyset$, and the initial condition is defined for $x \in \Omega$ with $\Omega \subset R^2$ by

$$\phi(\mathbf{x}, 0) = \phi_0(\mathbf{x}) \quad (4)$$

where ϕ is the scalar quantity, $\mathbf{v} = \mathbf{v}(\mathbf{x})$ is the given convection velocity vector, $\varepsilon \geq 0$ is the diffusion coefficient, κ is the reaction coefficient, and $t \in (0, T]$ for $T < \infty$.

By applying a characteristic approximation to trace advection in time, as explained in Ref. [5-7] to Eq. (1) yields

$$\frac{\partial \phi}{\partial t} - \nabla \cdot (\varepsilon \nabla \phi) + \kappa \phi = 0 \quad (5)$$

where all terms are to be evaluated at $\mathbf{x}' = \mathbf{x}'(t)$.

Then, by carrying out a Taylor series expansion, the convection term reappears in the equation along with an additional second-order term. This second-order term acts as a smoothing operator that reduces the oscillations arising from the spatial discretization of the convection terms. The fully explicit characteristic convection-diffusion-reaction equation is given by

$$\begin{aligned} \phi^{n+1} - \phi^n = & -\Delta t \left[\mathbf{v} \cdot \nabla \phi^n - \varepsilon \nabla \cdot \nabla \phi^n + \kappa \phi^n \right] \\ & + \frac{(\Delta t)^2}{2} \mathbf{v} \cdot \nabla \left[\mathbf{v} \cdot \nabla \phi^n + \kappa \phi^n \right] \end{aligned} \quad (6)$$

Together with the use of the divergence-free assumption $\nabla \cdot \mathbf{v} = 0$, Equation (6) could be written finally in the conservation form as

$$\begin{aligned} \phi^{n+1} - \phi^n = & -\Delta t \left[\nabla \cdot (\mathbf{v} \phi^n - \varepsilon \nabla \phi^n) + \kappa \phi^n \right] \\ & + \frac{(\Delta t)^2}{2} \nabla \cdot \left[\mathbf{v} (\mathbf{v} \cdot \nabla \phi^n + \kappa \phi^n) \right] \end{aligned} \quad (7)$$

2.2 The characteristic finite element method

Assuming a variation of ϕ within an element can be approximated by

$$\phi^n = \mathbf{N} \phi_e^n \quad (8)$$

$$\phi^{n+1} = \mathbf{N} \phi_e^{n+1} \quad (9)$$

where $\mathbf{N}$ is an element interpolation function. Applying the standard Galerkin weighting technique to Eq. (6) to yield

$$\begin{aligned} \int_{\Omega^e} \mathbf{N} \left(\frac{\phi^{n+1} - \phi^n}{\Delta t} \right) dA = & - \int_{\Omega^e} \mathbf{N} (\mathbf{v} \cdot \nabla \phi^n) dA \\ & + \int_{\Omega^e} \mathbf{N} \left(\frac{\Delta t}{2} \mathbf{v} \cdot \nabla (\mathbf{v} \cdot \nabla \phi^n) \right) dA \\ & + \int_{\Omega^e} \mathbf{N} (\nabla \cdot (\varepsilon \nabla \phi^n)) dA \\ & - \kappa \int_{\Omega^e} \mathbf{N} \left(\phi^n - \frac{\Delta t}{2} \mathbf{v} \cdot \nabla \phi^n \right) dA \end{aligned} \quad (10)$$

Because the hyperbolic nature of the convection-dominated equation, a nonlinear viscous shock capturing operator is added to minimize the oscillations at the discontinuities in the curvature of the front. The operator [9] is given by

$$B_{sc}(\phi) = \nu_{sc}(\phi) \int_{\Omega^e} (\nabla \mathbf{N} \cdot \nabla \mathbf{N}^T) \phi^n dA \quad (11)$$

and

$$\nu_{sc}(\phi) = \sigma_{sc} h^e \left| \frac{\partial \phi}{\partial t} + \mathbf{v} \cdot \nabla \phi^n \right| / \left(\left| \mathbf{v} \cdot \nabla \phi^n \right| + h^e \right) \quad (12)$$

where σ_{sc} is a parameter used to control added viscosity (typically is 0.1), and h^e is a measure of the element e . Finally, applying the Green-Gauss theorem to Eq. (9) also, using Eq. (8) to obtain

$$\begin{aligned} \frac{\mathbf{M}_e}{\Delta t} (\phi_e^{n+1} - \phi_e^n) = & - \mathbf{C}_1^e - \mathbf{C}_2^e - \mathbf{C}_3^e - \mathbf{K}_1^e + \mathbf{K}_2^e + \mathbf{K}_\infty^e \\ & + \mathbf{f}_{K1}^e + \mathbf{f}_{C2}^e \end{aligned} \quad (13)$$

where

$$\mathbf{M}_e = \int_{\Omega^e} \mathbf{N} \mathbf{N}^T dA \quad (14)$$

$$\mathbf{C}_1^e = \int_{\Omega^e} \mathbf{N} (\mathbf{v} \cdot \nabla \mathbf{N}^T) dA \phi_e^n \quad (15)$$

$$\mathbf{C}_2^e = \varepsilon \int_{\Omega^e} \nabla \mathbf{N} \cdot \nabla \mathbf{N}^T dA \phi_e^n \quad (16)$$

$$\mathbf{C}_3^e = \kappa \int_{\Omega^e} \mathbf{N} \mathbf{N}^T dA \phi_e^n \quad (17)$$

$$\mathbf{K}_1^e = \frac{\Delta t}{2} \int_{\Omega^e} (\mathbf{v} \cdot \nabla \mathbf{N}) (\mathbf{v} \cdot \nabla \mathbf{N}^T) dA \phi_e^n \quad (18)$$

$$\mathbf{K}_2^e = \kappa \frac{\Delta t}{2} \int_{\Omega^e} \mathbf{N} (\mathbf{v} \cdot \nabla \mathbf{N}^T) dA \phi_e^n \quad (19)$$

$$\mathbf{K}_{sc}^e = \nu_{sc}(\phi) \int_{\Omega^e} \nabla \mathbf{N} \cdot \nabla \mathbf{N}^T dA \phi_e^n \quad (20)$$

$$\mathbf{f}_{K1}^e = \frac{\Delta t}{2} \int_{\Gamma^e} \mathbf{N} (\mathbf{v} \cdot \hat{\mathbf{n}}) (\mathbf{v} \cdot \nabla \mathbf{N}^T) dS \phi_l^n \quad (21)$$

$$\mathbf{f}_{C2}^e = \varepsilon \int_{\Gamma^e} \mathbf{N} (\hat{\mathbf{n}} \cdot \nabla \mathbf{N}^T) dS \phi_l^n \quad (22)$$

2.3 The characteristic finite volume method

The computational domain is first discretized into a collection of non-overlapping control volumes $\Omega_i \in \Omega, i=1, \dots, N$, that completely cover the domain such that $\Omega = \bigcup_{i=1}^N \Omega_i$, $\Omega_i \neq \emptyset$ and $\Omega_i \cap \Omega_j = \emptyset$ if $i \neq j$. To obtain the finite volume equation, Eq. (7) is then integrated over the control volume Ω_i to yield

$$\int_{\Omega_i} (\phi^{n+1} - \phi^n) dA = \int_{\Omega_i} \left(-\Delta t \left[\nabla \cdot (\mathbf{v} \phi^n - \varepsilon \nabla \phi^n) + \kappa \phi^n \right] + \frac{(\Delta t)^2}{2} \nabla \cdot \left[\mathbf{v} (\mathbf{v} \cdot \nabla \phi^n + \kappa \phi^n) \right] \right) dA \quad (23)$$

Then the divergence theorem is applied to the spatial terms to yield a fully explicit characteristic-based scheme for solving Eq. (7) in the form

$$\phi_i^{n+1} = \phi_i^n - \frac{\Delta t}{|\Omega_i|} \sum_{j=1}^{N_j} |\Gamma_{ij}| \hat{\mathbf{n}}_{ij} \cdot \left[(\mathbf{v}_{ij}^n \phi_{ij}^n - \varepsilon \nabla \phi_{ij}^n) - \frac{\Delta t}{2} \mathbf{v}_{ij}^n (\mathbf{v}_{ij}^n \cdot \nabla \phi_{ij}^n) \right] \quad (24)$$

where N_j is a number of adjacent cell faces, Γ_{ij} is the segment of the boundary $\partial\Omega_i$ between the two adjacent control volumes Ω_i and Ω_j , and the quantities at the time $t = n$ are defined by

$$\phi_{ij}^n = \phi_{ij}(t^n) \quad (25)$$

$$\phi_i^n = \phi_i(t^n) \quad (26)$$

Finally, the scalar quantity at the cell faces, ϕ_{ij}^n , is approximated by applying Taylor's series expansion in space such that

$$\phi_{ij}^n = \phi_i^n + (\mathbf{x}_{ij} - \mathbf{x}_i) \cdot \nabla \phi_i^n \quad (27)$$

For the opposite direction of velocity, the values ϕ_{ij}^n could be computed from Eq. (27), but using the values from the neighboring cells according to the upwinding direction.

Moreover, in this paper, the gradient term, $\nabla \phi_{ij}^n$, is approximated by the weighted residuals method, which is commonly used in the finite element technique [6].

Finally, to ensure the stability of a numerical scheme, the CFL-like stability criterion must be fulfilled. In this paper, the time-step within each control volume i for both the CFEM and CFVM is determined from

$$\Delta t = C \min_i \left(\frac{|\Omega_i|}{\max_{j=1, \dots, N_j} |\mathbf{v}_{n,ij}|}, \frac{|\Gamma_{ij}^c|^2}{2\varepsilon} \right) \quad (28)$$

where $\mathbf{v}_{n,ij}$ is the scaled normal velocity at Γ_{ij} , $|\Gamma_{ij}^c|$ is the cell characteristic length, and $0 < C \leq 1$.

3 Test Problems and Discussion

In order to illustrate the accuracy and robustness of these numerical schemes, three examples are examined by implementing a second-order accurate scheme. These examples are (1) the rotation of a slotted-cylinder, (2) the rotation of a Gaussian cone, and (3) the skew flow to the mesh. All examples presented in this section were tested on structured triangular grids.

3.1 Rotation of a slotted-cylinder

This first problem is adapted from the rotation of a slotted cylinder problem, which was introduced by Zalesak [10]. It is a challenging pure-convection problem because the sudden change of the initial conditions and the shape of the rectangular slot in the domain $\Omega = [0, 1]^2$ are difficult to capture by most numerical schemes. The rotating velocity field is imposed such that $\mathbf{v}(\mathbf{x}) = (y - 0.5, 0.5 - x)$. The initial condition $\phi(\mathbf{x}, 0)$ is given by

$$\phi(\mathbf{x}, 0) = \begin{cases} 1 & (r \leq 0.15) \cap (|x - 0.15| \geq 0.025 \cup y \geq 0.8) \\ 0 & \text{otherwise} \end{cases} \quad (29)$$

where r is the distance from the center of the domain $(0.5, 0.5)$. The time step for this example is set to be equal to the period required for one turn rotation. This example is performed on a uniform grid of 256×256 . The exact solution at the final time step is then equal to the initial condition that is depicted in Figs. (1) and (2).

Figures 3 and 4 show that the CFEM scheme gives a dissipative solution and inaccurate position of a slotted-cylinder. Moreover, Figs. 5 and 6 show that the CFVM scheme gives more sharpen and accurate solution.

Figure 1: Exact solution at the final time of problem 3.1: 2D plot.

Figure 2: Exact solution at the final time of problem 3.1: 3D plot.

Figure 3: CFEM solution at the final time of problem 3.1: 2D plot.

Figure 4: CFEM solution at the final time of problem 3.1: 3D plot.

Figure 5: CFVM solution at the final time of problem 3.1: 2D plot.

Figure 6: CFVM solution at the final time of problem 3.1: 3D plot.

Figure 7: Comparison of the solution along the line $y=0.5$ at the final time of problem 3.1.

Finally, the comparison of the solution along $y=0.5$ is illustrated in Fig. 7. It is seen that the CFVM scheme gives a more accurate solution than the CFEM scheme. It can capture the maximum and minimum values around the slot of the cylinder accurately.

3.2 Rotation of a Gaussian cone

The second example is the rotation of a Gaussian pulse in a square domain where the scalar field is rotated around the domain $\Omega = [-0.5, 0.5]^2$. The rotating velocity field with the angular velocity of 4 rad/s is imposed as $\mathbf{v}(\mathbf{x}) = (-4y, 4x)$. This example has been used widely for testing the numerical artifacts that occur on different schemes [11,6]. The initial condition $\phi(\mathbf{x}, 0)$ is given by

$$\phi(\mathbf{x}, 0) = \exp\left(-\frac{(x + 0.25)^2 + y^2}{2\sigma^2}\right) \quad (30)$$

where $\sigma = 0.0447$. The final time is equal to $\pi/2$, which is the time period required for one turn rotation. this example is performed on a uniform grid of 128×128 . The diffusion coefficient of $\varepsilon = 10^{-4}$, in order to evaluate the robustness and accuracy of the method on a convection-dominated diffusion problem. The 2D and 3D plots of the exact solution as shown in Figs. 8 and 9. Figures 10 and 11 show the numerical solution obtained from the CFEM scheme. Then the numerical solution obtained from the CFVM scheme is also shown in Figs. 12 and 13. Moreover, the comparison of the numerical and exact solutions along the line $y = 0$ are presented in Fig. 14.

Figure 8: Exact solution at the final time of problem 3.2: 2D plot.

Figure 9: Exact solution at the final time of problem 3.2: 3D plot.

Figure 10: CFEM solution at the final time of problem 3.2: 2D plot.

Figure 11: CFEM solution at the final time of problem 3.2: 3D plot.

Figure 12: CFVM solution at the final time of problem 3.2: 2D plot.

Figure 13: CFVM solution at the final time of problem 3.2: 3D plot.

Figure 14: Comparison of the solution along the line $y=0$ at the final time of problem 3.2.

3.3 Skew flow to the mesh

The last example is the skew flow problem presented by Hauke [12,7]. This example considers the behavior of the numerical solutions under the convection-reaction-dominated diffusion condition in a square domain $\Omega = [0,1]^2$, with the initial condition $\phi(\mathbf{x}, 0) = 0$. The four boundary conditions are $\phi(x=0) = \phi(y=1) = 1$ and $\phi(x=1) = \phi(y=0) = 0$. The velocity field is given by $\mathbf{v}(\mathbf{x}) = (\cos(\pi/6), \sin(\pi/6))$. The numerical solutions are examined in the steady-state condition. It is noted that the influence of boundary conditions on the algorithm is remarkable and leads to instability [12]. The parameters for this test are $\varepsilon = 0.005$ and $\kappa = 100$. The analyses of these test cases are performed on the 10×10 grid size.

The 3D plots of numerical solutions of the CFEM and CFVM schemes are depicted in Figs. 15 and 16, respectively. Figure 15 shown that the CFEM scheme provides the oscillate solution along the boundaries $\phi(x=0) = \phi(y=1) = 1$ due to the abrupt change of the solutions. Moreover, the CFVM scheme gives non-oscillate solution along these boundaries. The examples confirmed that the CFVM scheme is an accurate and robust scheme for computing a wide range of convection-dominated diffusion-reaction problems.

Figure 15: CFEM solution at the final time of problem 3.3: 3D plot.

Figure 16: CFVM solution at the final time of problem 3.3: 3D plot.

4 Concluding Remarks

The accuracy and robustness of the CFEM and CFVM schemes for solving two-dimensional convection-diffusion-reaction problems on structured triangular grids are investigated in this paper. The characteristic convection-diffusion-reaction equation is derived. The finite element and finite volume is then used to discretize the characteristic convection-diffusion-reaction equation. Three examples are used to test the accuracy and robustness of both schemes. For the rotation of a slotted-cylinder problem, the CFEM scheme provides the diffusive and inaccurate position of the slotted-cylinder solution while the CFVM scheme gives the sharpen solution with an accurate position of the slotted-cylinder solution. The CFEM scheme provides a less accurate solution than the one obtained from the CFVM scheme for rotation of a Gaussian cone problem. Finally, for the skew flow to the mesh, the CFEM scheme provides the oscillate solution along the boundaries due to the abrupt change of the solutions. Moreover, the CFVM scheme

gives a non-oscillate solution. We can conclude that the CFVM scheme is an accurate and robust method for solving the convection-dominated problems.

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