

Validity of an instrumented knee brace compared to 3D motion navigation: A cadaveric investigation

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Reneaud Nicolas, Pierre Emma, Zory Raphaël, Chorin Frédéric, Thomas Luc, Chavet Pascale, Coyle Thelma, Truchet Eric, Puech Stephane, Ollivier Matthieu, Chabrand Patrick, Gerus Pauline

1 Title

- 2 Validity of an instrumented knee brace compared to 3D motion navigation: a cadaveric
- 3 investigation

4 Abbreviated title

5 Validity of an instrumented knee brace

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Highlights :

- Reliability of an instrumented knee brace during specific tasks
 - Consideration of soft tissue artifacts on knee brace with cadaveric navigation
- Validity of 3 axis kinematics of instrument knee brace compare to navigation investigation

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31 1. Abstract

The aim of this study was to test the accuracy and the reliability of 3-dimensional angular measurements of an instrumented knee brace compared to the gold standard navigation system optoelectronic cameras-based.

Thirteen cadaveric bodies were used to calculate kinematic knee parameters. Three exercises were performed, 100° flexion (FLEX100), internal/external rotation with a 30° flexion (ROT30), and the pivot shift test (PS).

The reliability was excellent with an ICC (95%) > 0.90. The agreement between the two systems showed excellent correlation in the F/E axis for FLEX100 and PS ($\sigma_{(Flex/Ext)} > 0.95$) and strong correlation in the I/E axis for ROT30 ($\sigma_{(Rot Int/Ext)} > 0.939$). The root mean square error (RMSE) was under 5° for all exercises considering the soft tissue artifact (STA) for the F/E axis.

Consequently, the instrumented knee brace exposed high reliability and accuracy which could
end up on clinical interpretations thanks to the previous measures.

45 2. Keywords

46 Connected knee brace, inertial measurement unit, joint kinematics, navigation, validity,47 reliability

49 **3. Background**

Knee joint function can be altered by several pathologies, such as anterior cruciate ligament 50rupture (ACLr) and knee osteoarthritis (OA) [1–4]. A better understanding of knee pathologies 51has given rise recently to new knee diagnostic and analysis tools [5–7]. Thus, motion capture 52and questionnaires have become the gold standard for practitioners for several pathologies 53[1,2,8]. The optoelectronic camera system (OCS) is the usual tool for quantifying body motion 54[2,9–11]. However, motion capture with OCS has few limitations. Firstly, the gait patterns can 55be affected by the laboratory environment compared to an ecological environment [12–14]. 56Secondly, the OCS is very expensive, restricted to a limited field of view in time and space 57[12,14] and time consuming. Finally, the OCS cannot be used in a home-based rehabilitation 58perspective. 59

To develop systems that overcome these disadvantages, recent research has focused on gait 60 analysis using wearable sensors [15], and new systems have been developed to quantify human 61motion. For example, accelerometers are valid and reliable for the recording of activity, energy 62 expenditure and acceleration data [16]. Nevertheless, the precision of kinematic measurements 63 64 is poor with an accelerometer sensor only due to the presence of drift during fast accelerations [17,18]. Combining a gyroscope with an accelerometer may solve this problem. Indeed, 65gyroscopes can estimate sensor orientation by integrating the angular velocity on the X, Y, Z 66 axes relative to the sensor. Yet this sensor is subject to a drift in angular velocity due to signal 67 integration, a well-known problem in robotics and motion analysis. By mixing the 68 complementary data from accelerometers and gyroscopes, the two drifts can be minimized with 69 a fusion algorithm like a Kalman filter [16,19,20]. The association of the two sensors is called 70 an inertial measurement unit (IMU). Body sensor networks with IMUs such as Xsens MVN 71(Xsens Technologies BV, Enschede, NL) [21] or Perception NEURON Pro (Noitom, Miami, 72FL, USA) [22] provide quantitative movement analysis in ecological environments. 73

In a home-based rehabilitation perspective, the knee motion analysis has become necessary to 74supervise patients through biofeedback. To deal with that, a new instrumented knee brace with 75two IMUs was developed. These sensors calculated the movement of the thigh relative to the 76shank. Moreover, this integrated system compares to simple IMU sensors described previously 77did not necessitate clinicians or physiotherapist for calibration or anatomical placement due to 78its ease of use. Indeed, once the connected knee brace is in place, it is possible to quantify knee 79motion in an ecological environment to reduce bias in laboratory conditions with a smartphone 80 [23-25]. Palpation to find anatomical landmarks is not required, nor is it necessary to fix 81 markers or IMUs with different systems, as it is the case with other systems [2,26]. Moreover, 82 this technology offers free use of a workstation for motion computation through cloud 83 computing on the smartphone app, and biofeedback can be displayed in real time with 84 smartphone computation. All these data allow a quantified rehabilitation for physiotherapists 85 or clinicians via success scores and pain scale charts. Then, this system enhance physical 86 rehabilitation by motivating the user with visual data of progression and informative videos 87 [27]. 88

However, this knee brace, like IMU systems or OCS, is sensitive to soft tissue artifacts (STA), 89 a problem inherent to all skin-mounted tracking system. A systematic review noted the effects 90 91of STA in the lower limb, finding that several factors influence the results, including sensor orientation [28]. STA was found to reach more than 30 mm of magnitude on the thigh segment 92and more than 15 mm on the tibia [28]. To overcome this problem, OCS investigation with 93 bony pins would be highly accurate [29,30], but this procedure is unethical and should not be 94 applied to living patients. Along the same lines, the fluoroscopic 3D-matching technique is 95 96 invasive due to radiation exposure [31]. Recently, several studies have used commercial navigation devices to assess knee kinematics during surgical procedures for ACL reconstruction 97 or total knee arthroplasty [32-34]. Navigation is composed of three parts: computer platform, 98

tracking system, and rigid body marker. Tracking system visualizes the rigid body markers through OCS and calculates motion in real time with the tracking systems. Markers are fixed to the patient's bones surgical instruments to track joint motion or target objects after a referencing procedure which consists in determining bone positions compared to marker positions [35]. For example, this system via bony pins and OCS is a computer-assisted surgical navigation device to help tunnel placement during ACL reconstruction and can quantify knee laxity and validate the surgical procedure [33,36].

A more ethical solution might be considered to begin with cadaveric investigations. Indeed,
tibiofemoral motion in the unloaded cadaveric knee is almost the same as that in the living knee
[37,38].

Given the innovative aspect of the knee brace, its accuracy and reliability must be confirmed before the system can be used more extensively. In the present study, we thus investigated the accuracy and reliability of this new system of knee motion quantification and compared it to the gold standard during specific movements well-known to physiotherapists and orthopedic surgeons.

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115 **4. Material and methods**

116 **4.1.** Subjects

Thirteen intact knees from seven frozen cadaveric males were used for this study. The specimens were thawed at room temperature for at least three hours and they showed no sign of degeneration. Exclusion criteria were signs of knee instability (Lachman test) and signs of surgical procedures on knee or hip, evidence of a knee or hip prosthesis, ACL reconstruction, etc. The mean age of the specimens was approximated at 85 years-old approximately due to a lack of anthropological information.

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4.2. Material and instrumentation

Three clusters of four reflective markers were fixed by one screw on the pelvis and two screws 124on the femur and tibia to record the knee kinematics. The femoral and tibial screws were fixed 125in the bone diaphysis outside the joint capsule with a 2-cm incision to avoid influencing the soft 126tissue. After fixing the three clusters, seven anatomical landmarks were identified with 127reflective markers fixed onto the skin with cvanoacrylate glue. The medial malleolus (MM), 128the lateral malleolus (LM), the medial and lateral epicondyle of the femur (MF, LF), the medial 129and lateral epicondyle of the tibia (MT, LT) and the greater trochanter (GT) were located. 130Kinematic data were simultaneously obtained with seven cameras (Vicon Motion Systems Ltd. 131132Oxford, UK): four MX-T20 and three MX-T40 and with the instrumented knee brace with a sampling frequency of 100 Hz. The instrumented knee brace is composed with two IMU ICM-13320948. The knee sleeve was designed to reduce compression around the knee by using soft 134tissue in opposition to medical knee sleeve designed to change the knee joint kinematic [39]. 135The knee sleeve compression around the knee was minimal to avoid change in knee joint 136movement but enough to limit the movement of the IMU sensors. IMU's knee brace had a 16 137bits resolution for accelerometers and gyroscope. However due to Bluetooth Low Energy 138communication, these resolutions were downgrade to 10 bits with respectively, a sensitivity of 1397.81 mg/LSB for a ± 4 g range and a sensitivity of 0.98 dps/LSB for a range of ± 500 dps. 140

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Figure 1: View of the instrumented knee brace, reflective markers and clusters placement on the cadaver's lower limb. The torso was strapped to the table to minimize artifacts on the hip cluster position.

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1494.3.Experimental protocol

To evaluate the position of the clusters relative to the bones, a functional movement protocol 150was generated with the leg extended on the table in a static position then with the leg fully 151extended realizing hip circular movement. The hip joint can be modeled as a ball-and-socket 152joint, and the hip joint center (HJC) location is characterized by a point invariant in any position 153of the joint [40]. The coordinates of the femoral head location were obtained by an optimization 154method to minimize the HJC movement in the circle movements compared to the hip reference. 155The distal femur location was determined at the middle of the MF and LF markers. The 156proximal and distal tibia locations were calculated between the MT and LT markers and the 157MM and LM markers, respectively. 158

The mechanical axis of the femur was defined by the line containing the femoral head location 159and the distal femur location. The femoral condular axis was defined by the MF and LF markers. 160 The femoral frontal plane was defined by the plane containing the mechanical axis and the 161femoral condylar axis. The femoral sagittal plane was defined with the femoral axis and the 162cross-product of the femoral axis and the femoral condylar axis [40]. The mechanical axis of 163the tibia was defined by the line containing the proximal and distal locations of the tibia. The 164tibial condylar axis was defined by the MT and LT markers. The tibial frontal plane was defined 165by the plane containing the mechanical axis and the tibial condylar axis. The tibial sagittal plane 166was defined with the tibial axis and the cross-product of the tibial axis and the tibial condylar 167168axis. To estimate the orientation of the two IMUs of the instrumented knee brace, we used a 169procedure implemented in a smartphone application.

The operator performed four movements, five times each: a flexion with a full extension to 170 flexion (FLEX100), a maximal internal/external rotation with a flexion of 30° (ROT30), 172 a pivot shift test (PS) and a flexion from full extension to maximal knee flexion under constraint 173 (FLEXMAX).

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175 **5. Calculation**

176 **5.1.** Analysis

The synchronization of the two systems was performed by a wand with three reflective markers on it. The maximum acceleration detected when the wand hit the thigh IMU was synchronized with the trajectory of the wand's reflective markers. Data from the OCS were analyzed and the angles were computed in Python. The data from the instrumented knee brace were collected and the angles were computed in Python with a data fusion algorithm based on Valenti et al. filter applied to the accelerometric and gyroscopic data [20]. However, data analysis revealed problems with the calibration protocol for the instrumented knee brace due to the dorsal decubitus position of the cadavers. A better alternative estimation was to find the IMU orientation by comparing clusters and IMU movements when there were small flexions in FLEXMAX. This estimation of the IMU orientation was used for all other exercises. Then, some acquisitions were not processed because of the abnormal movement of some of the anatomical marker fixed on the knee brace (MF, LF, MT and LT), which resulted in the selection of only 23 acquisitions in all. Due to motion differences between operators, only 13 acquisitions for pivot shift test were selected among the 23.

191 **5.2.**

Statistical analysis

Statistical analysis was performed on the FLEX100, ROT30 and PS exercises. The variables 192extracted for reliability were the intraclass correlation coefficient (ICC) and Bland & Altman 193plots. ICC was considered poor (<0.50), moderate (between 0.5 and 0.75), good (between 0.75) 194and 0.90), or excellent (>0.90) [41]. The variables extracted for validity were Pearson's 195correlation coefficient (σ), the root mean square error (RMSE), and the mean confidence 196 interval (CI). Pearson's coefficient was evaluated as excellent (>0.95), very good (0.85-0.95), 197198good (0.75-0.85), moderate (0.65-0.75) or weak (<0.65) [42]. Error (RMSE) <5° was considered excellent, and between 5 and 10° it was considered good [16]. RMSE was measured 199without offset on the abduction/adduction (A/A) axis and the internal/external rotation (I/E) 200axis because of the poor accuracy of the alternative IMU orientation procedure. To deal with 201STA [43], we extracted two types of variables for the validity: the validity on the standard knee 202motion and the validity on the knee motion with consideration of STA on the flexion/extension 203(F/E) axis through a linear regression on FLEXMAX acquisitions. 204

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6. Results

211	The ICC (95%) for the kinematic parameters recorded with the instrumented knee brace showed
212	excellent reliability for all exercises. In terms of concurrent validity, Pearson's r coefficient for
213	the instrumented knee brace kinematics compared to the navigation kinematics showed the
214	following for all exercises: very good to excellent correlations for the F/E angles, poor to
215	excellent correlations for I/E rotation, and poor to excellent correlation for A/A (Table 1).
216	RMSE was less than 5° between systems except for the F/E axis. Table 2, Figure 3, Figure 4
217	and Figure 5 show the impact of STA. The Bland & Altman plots showed the difference in the
218	range of motion (RoM) between the two systems (Figure 2). 3D kinematics of the knee during
219	the three exercises are depicted in Figure 3, Figure 4, and Figure 5. Rates of flexions for
220	FLEX100 and PS were 78.3 ± 12.4 dps and 55.5 ± 8.9 dps, rates of rotations for ROT30 were
221	19.4 ± 2.8 dps. Coefficients of variation (CV) were respectively: 15.8%, 16.0%, 14.3%.

Table 1.

ICC and Pearson's correlation coefficient (σ) between instrumented knee brace and navigation. (CI = confidence interval.)

Exercise	FLEX100	ROT30	PS
ICC (CI 95%)	0.979 (0.959 – 0.990)	0.957 (0.918 – 0.980)	0.976 (0.944 – 0.992)
σ _(F/E) (CI 95%)	0.999 (0.999 – 0.999)	0.888 (0.794 - 0.981)	0.991 (0.984 - 0.997)
σ _(I/E) (CI 95%)	0.700 (0.621 - 0.780)	0.956 (0.939 - 0.972)	0.725 (0.506 - 0.944)
σ _(A/A) (CI 95%)	0.820 (0.723 - 0.917)	0.649 (0.624 - 0.895)	0.860 (0.789 - 0.931)
σ _(I/E) (CI 95%) σ _(A/A) (CI 95%)	0.700 (0.621 – 0.780) 0.820 (0.723 – 0.917)	0.956 (0.939 – 0.972) 0.649 (0.624 – 0.895)	0.725 (0.506 – 0.944) 0.860 (0.789 – 0.931)

Table 2.

229	RMSE of F/E.	, F/E with STA	regression,	I/E, ar	nd A/A	with 95%	confidence	interval
		/						

Exercise	FLEX100 (°)	ROT30 (°)	PS (°)
F/E (CI 95%)	8.26 (6.77 – 9.77)	4.65 (3.11 - 6.18)	6.06 (4.86 - 7.27)
F/E Reg (CI 95%)	2.96(2.31 - 3.61)	1.01 (0.83 - 1.20)	2.72(2.08 - 3.35)
I/E (CI 95%)	2.25 (1.99 - 2.52)	3.12 (2.67 - 3.58)	3.89(3.03 - 4.75)
A/A (CI 95%)	3.82 (3.25 - 4.38)	1.83 (1.57 – 2.10)	3.53 (2.45 - 4.61)



Figure 2: Bland & Altman plots of RoM from both systems for FLEX100 (a), ROT30 (b) and

- 235 PS (c). Each graph represents the mean difference (black line) and the CI 95% of the
- 236 difference (dashed lines) as recorded by the instrumented knee brace and navigation.



Figure 3: Mean knee joint kinematics over all trials and all subjects with a standard deviation cloud to compare the two systems (Instrumented knee brace in blue, Instrumented knee brace without STA regression in red, Navigation with Vicon in orange) for flexion 100° in F/E (a), I/E (b), A/A(c)

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Figure 4: Mean knee joint kinematics over all trials and all subjects with a standard deviation cloud to compare the two systems (Instrumented knee brace in blue, Instrumented knee brace without STA regression in red, Navigation with Vicon in orange) for internal/external rotation at 30° of flexion in F/E (a), I/E (b), A/A(c)





Figure 5: Mean knee joint kinematics over all trials and all subjects with a standard deviation cloud to compare the two systems (Instrumented knee brace in blue, Instrumented knee brace without STA regression in red, Navigation with Vicon in orange) for pivot shift test in extension in F/E (a), I/E (b), A/A(c)

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- 260 **7. Discussion**
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This study compared a new instrumented knee brace based on two IMU sensors aligned to the lateral side of the pelvis and the leg with an OCS to evaluate the accuracy and reliability of the new system during specific tasks. The study showed the excellent reliability of the knee brace and the strong concordance between the two systems. The difference in the RoMs was acceptable. The RMSE values of the OCS and the knee brace for the three angles remained under 5° for all exercises.

The reliability of the IMU system was tested for each exercise and demonstrated ICC>0.918 268for all exercises, indicating excellent reliability. Moreover, the results are in line with the 269literature. Indeed, the ICC of the FLEX100 exercise was similar to the results found by 270Maderbacher's study, which showed an ICC of 0.92 for knee flexion [44]. The results for I/E 271272rotation with our knee brace were similar to those found by Musahl et al., who reported ICCs from 0.94 to 0.99 for measured rotational knee laxity with a noninvasive system [45]. Other 273274studies of gait analysis using IMU systems have found similar results, with excellent reliability for the flexion angle [46,47]. These studies are consistent with findings of the excellent 275reliability of IMU systems for several tasks. 276

The correlations between the two systems were excellent in the major axis of each exercise. 277These results are in line with the Pearson's correlation coefficient of 0.96 reported by Kayaalp 278et al. and the agreement between 0.82 to 1.0, depending on the task, for knee F/E reported by 279Lebel et al. [42,48]. However, the correlations for the minor axes were not as conclusive with 280Pearson's correlation coefficients ranging from weak to excellent. Favre et al. brought this trend 281to light with measurements of IMUs and the knee exoskeleton during a gait test, finding the 282major axis $\sigma = 1.00 (0.00)$ in F/E and the minor axes $\sigma = 0.76(0.18)$ in A/A and $\sigma = 0.85(0.11)$ 283in I/E [49]. Then, additional measurements revealed agreement levels between poor and 284

excellent, depending on the axis and joint, for squats (SQ), single-leg squats (SLS) and countermovement jumps (CMJ). For the knee joint, the minor axes for these exercises showed less agreement, ranging from poor to excellent, compared to the major axis (F/E), which showed excellent agreement [43]. These findings underline the weaker correlation of the two minor axes of the knee and the strong correlation in F/E found in this study, except for the ROT30 exercise due to a major axis in the I/E axis.

The accuracy of the instrumented knee brace as assessed by RMSE was under 5° in the three 291axes (F/E without STA). Lebel et al. reported comparable mean RMSE varying between 1.1° 292and 5.5°, depending on the segment tracked and the task performed [48]. The same results were 293found by Kayaalp et al., with a mean RMSE of 5.17° in F/E during a gait test [42]. A systematic 294review by McGinley et al. confirmed these results and noted that most studies reported error of 295less than 5° for all gait variables, excluding hip and knee rotation [50]. The study by Robert-296Lachaine et al. was in line with these results, with RMSE between 3° and 6° for knee rotations 297in the F/E, I/E, and A/A axes [51]. These authors thus agreed on the clinical relevance of IMU 298299systems with RMSE values under 5°.

Bland & Altman analysis revealed a similar RoM with a mean error under 2° in F/E due to the 300 STA regression used in the computation angles of the instrumented knee brace. These results 301 are similar to the findings of Teufl et al. for SQ, SLS and CMJ with a mean error of 2° [43]. 302Another study on Sit To Stand (STS) test with visual feedback showed a mean difference 303 ranging from -1.7° to 3.2° in the F/E axis between the IMU system and OCS [52]. More 304 specifically, Leardini et al. highlighted a mean RoM error of 3.9° for knee flexion between 0 to 30595° [27]. However, the RoM error for our ROT30 exercise revealed an underestimation in the 306 307I/E rotation axis due to STA. Unfortunately, no significant regression was found to minimize STA on this axis. Indeed, Stagni et al. also observed a simple overestimated flexion in F/E but 308 a more complex artifact for I/E and A/A rotations [53]. 309

A few limitations of this study should be noted. First, the outcomes were marred by STA, which 310311 impacted each axis of rotation, but more specially the I/E and A/A rotations because there was no compensation for STA. More studies are required to identify the best approach to minimize 312STA and reduce RMSE between the connected knee brace and bone placement [31,54]. Indeed, 313 the results of the ROT30 exercise contradicted the findings of Moewis et al. (Figure 2; Figure 3143), who suggested a linear overestimation of I/E rotation with skin-mounted markers compared 315316to knee fluoroscopy [55,56]. Second, the alternative procedure for estimating the IMU orientation with optimization introduced inaccuracy into the measurement of I/E and A/A 317 rotations due to the exercise of flexion used by the optimization algorithm [57,58]. In fact, the 318319 I/E and A/A rotations had a small range of motion and were in general less valid due to the projection of the F/E rotation, caused by small errors in IMU orientation estimation during the 320calibration phases [16,58,59]. Further studies should elucidate the most appropriate calibration 321322methods to estimate joint kinematics [42,57]. Third, even if navigation system allows a motion capture without STA, mechanical properties between cadaveric and living knee may differ due 323 to difference in soft tissue tension, capsule, ligaments and neglecting the influence of muscle 324contractions [38,60]. Then, passive kinematics may differ from active kinematics [38,60]. Not 325least of all, rates of flexion and rotation for FLEX100, PS and ROT30 highlighted limitations 326 327in reliability of movements due to a CV close to or even higher than 15% [61]. Acquisition performed with a robotic arm would acquire better data with repetitive ranges and rates [62]. 328 However, acquired data performed with clinicians is closer to field data acquisitions. 329

331 8. Conclusion

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The present work investigated the reliability and accuracy of a new instrumented knee brace compared to a gold standard navigation system without STA. The new brace showed excellent reliability and sufficient accuracy for clinical interpretations. However, STA induced errors in the axes without artifact consideration algorithm. In conclusion, this study highlights the clinical validity of the instrumented knee brace. Further investigations are necessary to develop new algorithms to minimize STA in the I/E and A/A

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9. Declaration of competing interest

The institutes of the Authors have received funding from the marketing company the instrumented knee brace Ted Orthopedics to cover the costs involved in the execution of this study. I, Nicolas Reneaud, declare that Zory Raphaël, Chorin Frédéric, Chavet Pascale, Coyle Thelma, Puech Stephane, Ollivier Matthieu, Chabrand Patrick, Gerus Pauline have no proprietary, financial, professional or other personal interest of any nature of kind of any product, service and/or company that could be construed as influencing the position presented in the manuscript.

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355 **11. References**

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