Comprehensive study on chip-integrated germanium pin photodetectors for energy-efficient silicon interconnects

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Abstract—Optical interconnects are promising alternatives to copper-based wirings in on-chip communications. Recent advances in integrated group-IV nanophotonics should address a range of challenges related with speed, energy consumption and cost. Monolithically integrated germanium pin photodetectors on silicon-on-insulator (SOI) waveguides are indispensable devices in this buoyant research field. Here, we comprehensively investigate the opto-electrical properties of hetero-structured pin photodetectors. All photodetectors were fabricated on top of 200-mm SOI substrates using industrial-scale semiconductor manufacturing processes. Under a low-bias voltage supply of 1 V, pin photodetectors exhibit dark-currents from 5 nA to 100 nA, dark current densities from 0.404 A/cm² to 0.808 A/cm², responsivities in a range of 0.17 A/W to 1.16 A/W, and cut-off frequencies from 7 GHz to 35 GHz, respectively. Such achievements make them promising for use in power-efficient optical links operating at 40 Gbps, with a device energy dissipation of only few fJ per bit.

Index Terms—Complementary metal-oxide-semiconductor technology, germanium photodetectors, inter- and intra-chip interconnects, optical communications, silicon nanophotonics.

I. INTRODUCTION

OPTICAL interconnects has superseded electrical wirings for inter and intra-chip links due to the performance limits of the latter. Driven by the exponential growth in Internet traffic and portable digital communications, optical solutions are looking increasingly promising not only for long-haul fiber systems, but also in emerging industries such as short-reach data centers, clouds or high-performance

computing, amongst other. Therefore, optical interconnects at the chip-scale level are presently used to address a range of challenges associated with affordable speed, energy consumption and cost [1-6].

Recent advances in nanophotonics yielded compact and high-performance devices on a single chip [5, 6]. Nanophotonics is notably based on a class of materials known as group-IV elemental semiconductors such as silicon (Si) and germanium (Ge) [7-12].

Si, an indirect bandgap material with an energy of 1.1 eV, is an excellent material for low-loss waveguides and high-performing passive devices at near- and mid-infrared (near- and mid-IR) wavelengths [1, 9-11]. In contrast, Ge with its direct bandgap energy of 0.8 eV only, provides several distinctive advantages and complementarities over Si chips and addresses major Si limitations [1]. Optical absorption is indeed high in Ge over the 1.3 – 1.55 μm wavelength range used for fiber-optic communications. The epitaxy of Ge over Si has otherwise progressed tremendously over the last twenty years. Finally, mature process steps using complementary metal-oxide-semiconductor (CMOS) tools and procedures are nowadays available to process Ge-based devices [11, 12]. Intensive efforts are underway to use Ge and/or Ge-based alloys for light emission [13], modulation [14, 15], and detection [16]. In this active research field, the synergy between mature semiconductor manufacturing infrastructure, high fabrication yield, and low fabrication cost is the key for future monolithic integrated circuits [7, 8].

Ge-based photodetectors have been extensively studied since the late 1990s [17-39]. Nowadays, Ge photodetectors have performance metrics, which are close to that of III-V materials. Ge detectors are currently available in open-access platform offerings through foundry sharing initiatives [8], as they are compatible with other passive and active devices on standard silicon-on-insulator (SOI) platforms.

Ge photodetectors integrated at the end of optical waveguides are more appealing for nanophotonics than surface-illuminated devices. In a wave-guided on-chip detection scheme, the optical absorption path is indeed decoupled from the carrier collection path. In other words, light absorption occurs along the optical mode propagation direction and perpendicularly to the carrier collection path.

Manuscript received June 4, 2019. This work was supported by the European Union's Horizon 2020 research and innovation program (ERC POPSTAR – grant agreement no. 647342).

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This approach advantageously circumvents the conventional design trade-off between device responsivity (quantum efficiency) and device speed (opto-electrical bandwidth) and fits modern CMOS processes [1, 16]. Since the first successful implementation of this concept by Ahn, *et al.*, a large number of architectures have been proposed and experimentally demonstrated. Ge homo-junction [17-31] and Si-Ge-Si hetero-junction [32, 35-40] photodetector arrangements have notably been evaluated. Both types of devices consist in pin junction arrangements, with a light absorption occurring in the intrinsic regions. The performances of full-Ge devices are hindered by process issues and optical considerations (i.e. no light confinement in the intrinsic detector region). In homo-junctions photodetectors, ion implantation is used to fabricate heavily *n*-type and *p*-type doped side regions, which then have to be contacted to metal via. Both process steps are not as performant in Ge as in Si. This results in slower responses, reduced photo-responsivities, and higher dark-currents in homo-junction structures [17-31]. In contrast, hetero-structured Ge photodetectors with full Si via-contacts and doping scheme avoid Ge processing issues and might substantially simplify the process flow [32, 35-40]. For example, the same masking, ion implantation, and metal contacting steps can be used for the fabrication of active optical link components such as Si modulators and Si-Ge-Si photodetectors [41]. This architecture also leads to the flexible control of the light confinement in the intrinsic region. Such photodetectors have been realized and demonstrated with significantly improved performances in near-IR wavelengths [32,35-40].

All photodetectors are integrated at the end of conventional Si waveguides on 200 mm SOI substrates and are readily compatible with industrial-scale semiconductor manufacturing processes. Capitalizing on our previous efforts [39, 40], in this work, we provide a detailed experimental study of optical photodetectors of different waveguide geometries. The resulting Ge photodetectors exhibit promising opto-electrical performances in terms of dark-currents, responsivity, bandwidth and power consumption. Those devices are suitable for the future needs in high-speed links operating at 40 Gbps.

II. DESIGN, INTEGRATION AND FABRICATION

In this work, the Ge photodetectors, shown in Fig. 1, were integrated on top of regular SOI waveguide platforms, with 220 nm thick Si layer on top of 2 μm thick buried oxide (BOX) layer. As schematically illustrated in Fig. 1(c), the Ge photodetector is a pin diode structure (made of *p*-doped-type / intrinsic (*i*) / *n*-doped-type regions) at the end of the Si waveguide. The waveguide-integrated Si-Ge-Si pin photodetector consists in a Ge light-absorbing layer (intrinsic Ge zone, *i*-Ge) with a thickness of about 260 nm. The Ge layer is selectively grown in slits (with ~60 nm thick Si bottom layers just above the BOX) sandwiched between *n*-type and *p*-type doped Si slabs (*p*-Si and *n*-Si, respectively) with metal via contacts on top.

Surface grating couplers (Fig. 1(b)) were used to inject light from a standard optical fiber into the on-chip Si waveguides. A C-band wavelength (i.e. 1.55 μm) was selected and a transverse electrical (TE) waveguide mode evaluated. Strip waveguides were used for low-loss butt-coupling light injection into the Si-Ge-Si photodetectors. The input strip waveguides, 220 nm thick and 500 nm wide, were designed to preserve single-mode propagation. Light funneling into the Ge photodetector via the butt-coupling approach is a robust injection scheme with no further optimization needed, as the Ge intrinsic zone is in direct contact with the input waveguide.

Devices were fabricated with a simplified process flow and conventional CMOS tools in CEA LETI's cleanroom. We used 200 mm SOI wafers, with 220 nm thick Si layer on top of 2 μm thick BOX. The process was initiated by fabricating the passive devices such as fiber couplers and waveguides. The main process steps used were: (i) Si waveguide fabrication: cap layer formation, ion implantations and Si cavity formation; (ii) intrinsic Ge selective epitaxial growth, followed by passivation and insulation; and (iii) back-end-of-line standard CMOS metallization with tungsten (W-type) metal plugs and aluminum copper (AlCu) electrodes. The detailed description of the fabrication flow can be found in Refs. [39, 40]. Optical micrograph images of fabricated optical photodetectors are shown in Figs. 1(a) - full detectors array and 1(b) - enlarged view with a few devices and surface grating couplers. A cross-sectional Scanning Electron Microscopy image of a photodetector cross-section can be found in the inset of Fig. 1(c).

Fig. 1. Optical micrograph images of waveguide-integrated pin photodetectors with lateral silicon-germanium-silicon hetero-junctions: (a) Full array of devices and (b) close-up view of some structures. (c) Cross-sectional schematics of the photodetector with a lateral silicon-germanium-silicon heterojunction integrated at the end of the silicon-on-insulator waveguide. Light coming from an input strip waveguide is injected into the intrinsic Ge region perpendicularly to the schematics. Inset: Scanning electron microscopy image of a fabricated pin photodetector.

In this work, we comprehensively investigate the properties of optical photodetectors with lateral Si-Ge-Si heterojunctions.

III. PHOTODETECTOR PERFORMANCE: RESULT AND DISCUSSION

In the following, we describe the various experimental characterization techniques and quantify the opto-electrical performances of our waveguide-integrated hetero-structured Si-Ge-Si pin photodetectors.

A. Leakage dark-current measurements

Dark-currents were evaluated through static current-voltage (I - V) measurements without light illumination, as a function of the applied reverse bias voltage for various waveguide-integrated photodetectors. Low-reverse-bias voltages were selected for device operation, as they do not degrade the opto-electrical performances in terms of responsivity and cut-off frequency response. Minimizing the operation bias is also desired for integration with CMOS circuitry. I - V tests were conducted on devices with different widths (w_{ge}) and lengths (l_{ge}) of the intrinsic Ge zone. More specifically, Ge detector widths of 0.3, 0.5, 0.8 and 1.0 μm and lengths of 5, 10, 20 and 40 μm were considered. Figs. 2 shows the best dark-current levels for the various photodetectors.

Fig. 2. (a) Conventional static current-voltage characteristics of hetero-structured pin photodetectors with different junction areas ($a_{\text{ge}} = w_{\text{ge}} \times l_{\text{ge}}$) under dark-illuminated conditions. Ge detector widths of 0.3, 0.5, 0.8 and 1.0 μm and lengths of 5, 10, 20 and 40 μm were investigated. Evolution of the leakage dark-currents versus photodetector junction area under 1 V reverse bias voltage for Ge widths of (b) 0.3 μm and 0.5 μm , and (c) 0.8 μm and 1.0 μm , respectively.

Fig. 2(a) shows conventional dark-current curves for pin photodetectors with the largest Ge areas ($a_{\text{ge}} = w_{\text{ge}} \times l_{\text{ge}}$). Under low-bias (in particular, at -1 V bias), dark-currents remain low, of the order of a few tens of nA only. The maximum dark-currents were consistently measured on the largest devices ($a_{\text{ge}} = 40 \mu\text{m}^2$), with values approaching 150 nA. The measured dark current levels are comparable [32, 33] or slightly higher than those achieved with other hetero-structured pin photodetectors [34-38], yet they are substantially lower than many pure homo-junction devices [19, 21, 22, 24, 26, 28, 30]. To reach the highest signal-to-noise ratio (SNR) possible, the dark-current levels should be as low as possible. As confirmed above, small-sized photodetectors favor low noise operation as dark-currents scale with the detector active volume. It is also worth to mention that conventional pin photodetectors operated under low-bias supplies are typically connected to additional receiver electronic circuits with a trans-impedance amplifier (TIA) and a limiting amplifier (LA) [30]. In those situations, the dark current is not a dominating noise source, as the input-referred noise of TIA is comparatively larger than the dark

current. Photodetectors presented in this work exhibit low dark current levels, typically well-below 1 μA . This is promising for the development of high-speed optical receivers based on group-IV nanophotonic platform. Indeed, the dark-current also directly increases with the reverse bias and/or the shrinking the intrinsic width of the Ge detector. The later trend is due to the stronger electric field within the intrinsic Ge zone, as for a given reverse bias the electric field increases as the intrinsic Ge region width decreases. As shown in Fig. 2(a), there is a significant increase of the dark-current with the electric field ($a_{\text{ge}} = 6, 20$ and $32 \mu\text{m}^2$ devices). Meanwhile, the relatively weak electric field present in the largest devices does not yield such bias dependence ($a_{\text{ge}} = 40 \mu\text{m}^2$ device). Figures 2(b) and 2(c) show that the dark-current leakage increases linearly with the detector area, this whatever the intrinsic width. All devices were biased with a 1 V reverse bias. The mean dark current densities for the smallest and the largest devices are in a range of $0.404 \pm 0.019 \text{ A/cm}^2$ to $0.808 \pm 0.129 \text{ A/cm}^2$, respectively. The large dark current densities are attributed to the small junction area, as the Ge layer is only $\sim 260 \text{ nm}$ thick, and to the low to moderate dark current values.

B. Photo-responsivity measurements

To characterize the device responsivity (quantum efficiency), we performed additional I - V measurements, this time under light illumination. The light generated by a tunable laser source was injected from a single-mode optical fiber into the Si chip using surface grating couplers. Prior to coupling, a polarization controller was used to maximize the grating coupler transmission for TE-like waveguide mode and a central operating wavelength of 1.55 μm . The output power was monitored thanks to an optical power meter, with a measured level of about -11 dBm and an estimated uncertainty of $\pm 0.25 \text{ dB}$. The device photo-responsivity (r_p) was calculated as follows [1]:

$$r_p [\text{A/W}] = \frac{(i_{\text{pc}} - i_{\text{dc}})}{P_c} \quad (1)$$

Here, i_{pc} and i_{dc} stand for generated photo- and dark-currents, respectively, and P_c is the average optical power coupled into the waveguide photodetector.

Fig. 3. Responsivities for a set of waveguide-integrated pin photodetectors with lateral silicon-germanium-silicon heterojunctions as functions of the applied reverse voltage. The measurements were conducted at a nominal wavelength of 1.55 μm . (a) Photodetectors with different junction areas ($a_{\text{ge}} = w_{\text{ge}} \times l_{\text{ge}}$) and photodetectors with various lengths and widths of the intrinsic Ge region: (b) $w_{\text{ge}} = 0.3 \mu\text{m}$ and (c) $w_{\text{ge}} = 1.0 \mu\text{m}$. The measured photo-current resulted from an average optical power injected in devices of about -11 dBm.

Figure 3 shows responsivities of hetero-structured

photodetectors with different geometries as functions of the applied reverse bias. Fig. 3(a) shows the evolution of the photo-responsivity for the largest device areas ($a_{\text{ge}} = w_{\text{ge}} \times l_{\text{ge}}$), which have the following in-plane geometries: $a_{\text{ge}} = 0.3 \mu\text{m} \times 20 \mu\text{m}$; $0.5 \mu\text{m} \times 40 \mu\text{m}$; $0.8 \mu\text{m} \times 40 \mu\text{m}$ and finally, $1.0 \mu\text{m} \times 40 \mu\text{m}$. Meanwhile, Figs. 3(b) and 3(c) show device photo-responsivities for various Ge lengths, this for $0.3 \mu\text{m}$ - and $1 \mu\text{m}$ -wide devices.

Under 0 V bias, the responsivity of hetero-structured Si-Ge-Si photodetectors remains low, because of the weak built-in electric field. In particular, as shown in Fig. 3(a), for device junction areas of $a_{\text{ge}} = 0.3 \mu\text{m} \times 20 \mu\text{m}$; $0.5 \mu\text{m} \times 40 \mu\text{m}$; $0.8 \mu\text{m} \times 40 \mu\text{m}$, and finally, $1.0 \mu\text{m} \times 40 \mu\text{m}$, measured responsivities are equal to 0.14 A/W, 0.27 A/W, 0.47 A/W, and 0.63 A/W. As expected, the responsivity increases with the reverse voltage. This is due to a high electric field within the intrinsic Ge region of the photodetector. Such a behavior is also associated with a very fast and sharp responsivity increase. The responsivity maximum is typically reached at a low-bias voltage of -0.5 V. The extracted responsivities in Fig. 3(a) devices are substantially larger, then: 0.17 A/W, 0.44 A/W, 0.73 A/W, and 1.16 A/W. Excellent operation at low-bias shows that Si-Ge-Si pin photodetectors have a marked ability to sweep out the vast majority of electron-hole pairs within their lifetime. Indeed, high responsivities (>1 A/W) were also demonstrated in both full-Ge [19, 21, 22, 24, 25] and hetero-structured devices [32, 33, 35]. The responsivity increases with the width and the length of the intrinsic Ge region. Beyond 0.5 V reverse bias, responsivities reach a plateau for the largest devices, with a negligibly low or a moderate dependency on the applied reverse bias voltage. The evolution of the photo-responsivity with an applied bias is more pronounced in devices with narrower widths of the Ge intrinsic region. This can likely be attributed to the following, jointly acting, factors: (i) The built-in electric field, which is higher in narrow than in wide intrinsic regions, results in a higher voltage dependency. (ii) The increase of the electric field at the interface between the doped Si regions and the intrinsic Ge zone enables the E-field to penetrate in the Si regions, which can lead to collection of carriers generated within the Si-doped slabs and can also initiate a local impact ionization process, producing a small gain of the generated current. (iii) A reduced modal confinement within the narrow intrinsic Ge region. The later aspect may decrease the absorption efficiency in Ge and increase adverse losses coming from the higher overlap between the TE-like waveguide mode and the heavily doped Si regions.

It is obvious, when looking at Fig. 3 data, that waveguide-integrated pin photodetectors with hetero-structured lateral junctions yield very high levels of quantum efficiency (η), approaching the theoretical limit of 100%. In other words, pin photodetectors built upon lateral Si-Ge-Si heterojunctions transform very efficiently incident photons into electrons and therefore photo-currents. The quantum efficiency is defined as follows [1]:

$$\eta[\%] = \frac{1.24 \cdot r_p}{\lambda} \quad (2)$$

Here, r_p is the experimentally determined photo-responsivity and λ is the reference wavelength of $1.55 \mu\text{m}$. Similarly to device photo-responsivity, the quantum efficiency scales with the lengths and widths of the intrinsic Ge region. Quantum efficiency, at $1.55 \mu\text{m}$ wavelength and with 0.5 V reverse bias, is equal to 13.75% for $a_{\text{ge}} = 6 \mu\text{m}^2$, 35.1% for $a_{\text{ge}} = 20 \mu\text{m}^2$, 58.7% for $a_{\text{ge}} = 32 \mu\text{m}^2$, and 92.8% for $a_{\text{ge}} = 40 \mu\text{m}^2$.

C. Opto-electrical bandwidth assessments

The opto-electrical properties of Si-Ge-Si hetero-structured pin photodetectors have been investigated through small-signal radio-frequency (RF) measurements. A standard RF-test set-up and a commercial Lightwave Component Analyzer (LCA), including an internal laser source and a modulator, provided responses of the S_{21} parameter over the 0.1 GHz to 50 GHz range, the latter frequency being the upper limit of the LCA. Off-chip light coupling was done thanks to a fiber-chip surface grating coupler. The photodetectors under study were reversely biased via a bias-tee connected to a source measurement unit.

Fig. 4. Radio-frequency responses of the normalized S_{21} parameter for waveguide-integrated pin photodetectors with different widths of the intrinsic Ge region under a reverse bias of (a) 1 V and (b) 2 V, respectively. Frequency measurements of S_{21} parameter were performed at a wavelength of $1.55 \mu\text{m}$ with a power coupled into the photodetectors of about -11.4 dBm. Insets: Reference and retrieved eye diagrams for $0.8 \mu\text{m}$ - and $1 \mu\text{m}$ -wide devices under 0 V at a bit rate of 10 Gbps.

Figure 4 shows a collection of normalized S_{21} traces from small-signal RF tests on hetero-structured pin photodetectors with different intrinsic zone geometries ($w_{\text{ge}} / l_{\text{ge}} = 0.3 \mu\text{m} / 20 \mu\text{m}$, $0.5 \mu\text{m} / 40 \mu\text{m}$, $0.8 \mu\text{m} / 40 \mu\text{m}$ and $1.0 \mu\text{m} / 40 \mu\text{m}$). Devices were biased at reverse voltages of 1 V (Fig 4(a)) and 2 V (Fig. 4(b)), respectively. The power coupled to the photodetectors was estimated to be -11.4 dBm. 10 Gbps eye diagrams (reference and retrieved) of $0.8 \mu\text{m}$ - and $1 \mu\text{m}$ -wide devices probed at 0 V bias are included in insets of Figs. 4(a) and 4(b), respectively. The reference diagrams correspond to optical input signals. Retrieved eyes remain closed due to the small -3 dB cut-off frequency. The extracted zero-bias -3-dB bandwidths are: 4.8 GHz, 2.8 GHz, 1.3 GHz, and 1.1 GHz respectively to the intrinsic Ge region dimensions given above. Such small cut-off responses are due to the long transit carrier time and the weak built-in electric field. This hinders the device ability to efficiently collect photo-generated pairs of electrons and holes under 0 V bias. Moreover, this is also in line with the low responsivities at 0 V.

In opposition, as shown by RF responses in Fig. 4, biasing at 1 V and 2 V considerably enhanced the -3-dB bandwidths

of pin photodetectors compared to reference bandwidths at 0 V bias. The -3-dB cut-off frequency also drastically increases as the photodetectors become narrower. Bandwidths for all tested devices as functions of the applied reverse bias are provided in Figs. 5(a) and 5(b), respectively. The extracted -3 dB bandwidths under a low-bias voltage of 1 V are equal to 35.0 GHz, 24.2 GHz, 15.7 GHz, and 6.7 GHz for 0.3, 0.5, 0.8, and 1.0 μm -wide intrinsic Ge regions. Fast responses achieved with our hetero-structured Si-Ge-Si devices well match the speed performances in the state-of-the-art full-Ge and hetero-structured photodiodes [17-38]. As shown in Fig. 5(a), the -3 dB bandwidth does not really depend on the length of the intrinsic Ge region (here, for a fixed device widths of 0.3 μm and 1.0 μm , respectively). Indeed, only marginal ripples were observed inside the measured bandwidth. This reveals that the bandwidth properties of the hetero-structured Si-Ge-Si photodetectors remain constant with the variation in device lengths and that the main bandwidth limitation is driven by the transit time.

Fig. 5. Opto-electrical bandwidth properties for different lengths (a) and widths (b) of the intrinsic Ge region. (c) Product of quantum efficiency and -3-dB opto-electrical bandwidth as a function of applied reverse bias voltage for different junction areas of the pin photodetectors with lateral silicon-germanium-silicon heterojunctions. The small-signal radio-frequency tests were carried out at a wavelength of 1.55 μm and the average optical power coupled to the devices was estimated to be -11.4 dBm.

Figure 5(c) shows the product of the quantum efficiency by the -3-dB optical bandwidth as a function of the applied reverse bias voltage for the largest Ge areas of hetero-structured pin photodetectors. These Ge areas are the same as before. The efficiency-bandwidth product provides a figure-of-merit suitable for photodetector design in terms of opto-electrical performance and footprint.

Device areas of 6 μm^2 (the smallest one: $w_{\text{ge}} = 0.3 \mu\text{m}$ and $l_{\text{ge}} = 20 \mu\text{m}$) and 40 μm^2 (the largest one: $w_{\text{ge}} = 1.0 \mu\text{m}$ and $l_{\text{ge}} = 40 \mu\text{m}$) result only in moderate opto-electrical performances. The former type of device enables fast operation (beyond 50 GHz, potentially). However, its

responsivity under 1 V bias is 0.19 A/W only (15.03% in quantum efficiency). Those values are not high enough to use in nanophotonics. Meanwhile, the latter detector layout has an outstanding responsivity to incident photons of 1.17 A/W (approaching 100% quantum efficiency). However, the device speed is lower and fundamentally restricted by the large cross-section, i.e. transit time limited operation.

As shown in Fig. 5(c), the best opto-electrical performances under a low-bias condition were achieved for 20 μm^2 and 32 μm^2 photodetector areas. The corresponding in-plane dimensions of the Ge region are as follows: 0.5 μm x 40 μm and 0.8 μm x 40 μm . Both devices provide opto-electrical performances that fit for high-speed applications, including high-rate data networks, while their compact footprint allows a high density integration of multiple opto-electronic devices on a single Si chip. Their specific responsivities of 0.47 A/W and 0.76 A/W (37.7% and 60.84% in quantum efficiency) are coupled with fast responses of the order of tens of GHz.

D. Large-signal data link measurements

To assess the viability of waveguide-integrated pin photodetectors with lateral Si-Ge-Si heterojunctions in optical data links, we have also carried out large-signal measurements via detailed eye diagram inspections. To that end, data were transmitted in a non-return-to-zero (NRZ) modulation format. The pseudo-random-binary-sequence (PRBS) pattern of length $2^7 - 1$ was used for different data rates. Due to the frequency limitation of the pattern generator, we could not provide high-speed tests beyond 40 Gbps. A DFB laser at a wavelength of 1.55 μm was modulated with an external modulator, followed by an optical amplifier, an optical filter, and a fibered coupler. One output of the coupler was connected to a 60 GHz photodiode of an oscilloscope to display the modulated respective input signal as a reference. The other output signal of the coupler was transmitted towards the device through an optical attenuator and an in-line power meter to control the optical power level. The polarization of the input light was controlled to match the TE-like mode of the Si waveguide and optimize the signal intensity. Finally, the signal was sent into the chip thanks to a fiber-to-chip surface grating coupler and detected by hetero-structured pin photodetectors, without the use of subsidiary electronic stages with trans-impedance amplifier or limiting amplifier. Electrical data were collected with a RF set-up and sent to the high-speed oscilloscope [40].

Figure 6(a) - 6(c) show eye diagrams for 40 μm -long pin photodetectors with different intrinsic Ge widths (1.0 μm , 0.8 μm , and 0.5 μm) under a 0.5 V reverse bias state and at a data rate of 10 Gbps. Reference 10 Gbps eye diagram aperture is shown in Fig. 6(d). In all cases, eye diagrams are clearly open under such conditions. Low-voltage operation is desirable to keep dark-currents as low as possible and be compatible with CMOS circuits. On the other hand, it is worth noting that simple pin photodiodes typically yield low electrical output levels. As a consequence, the implementation of trans-impedance amplifier with pin photodiodes is foreseen to be an essential step to access full transmission system assessments with the presented devices [30].

Besides low-bias operation and affordable high-speed transmission ability, the amount of energy consumed by each active device, in this case, an optical photodetector, is essential in an optical communication system design. The energy consumption, denoted here as ec , is estimated as follows [30]:

$$ec[fJ/bit] = \frac{1}{br} \cdot (i_{pc} \cdot v). \quad (3)$$

Here, br is the transmission bit rate, i_{pc} is the measured current (including photo- and dark-currents), and v is the reverse bias.

Fig. 6. Eye diagram apertures under low-reverse-bias of 0.5 V and a fixed data rate of 10 Gbps for 40-μm-long waveguide-integrated pin photodetectors with varying Ge intrinsic region widths: (a) 1.0 μm, (b) 0.8 μm, and (c) 0.5 μm. (d) Reference eye diagram for a bit rate of 10 Gbps. The power coupled into the photodetectors was estimated to be -8.9 dBm. Here, x [ps/div] and y [mV/div] are horizontal and vertical axes of the scope, respectively. (e) Calculated energy consumption per transmitted bit of the studied pin photodetectors as a function of the Ge intrinsic width under different reverse voltages and a fixed 10 Gbps optical link rate.

Figure 6(e) shows the evolution of the consumed energy versus the width of the intrinsic Ge region. Here, the pin Ge photodetectors were 40-μm-long and were probed under several reverse bias states (0.5 V, 1 V, and 2 V). The considered link data rate was 10 Gbps. We may state that wider Ge detectors yield higher energy consumption and that the increase consumption remains roughly proportional to the reverse voltage increase for each width. This trend is more perceptible under higher bias voltages. More specifically, under a 0.5 V bias point, doubling the width of the intrinsic Ge region (from 0.5 μm to 1.0 μm) yields moderate increase of consumed energy (from 3.1 fJ/bit to 7.7 fJ/bit), while under a 2 V bias state, this increase is from 11.5 fJ/bit to 31.2 fJ/bit. Nevertheless, in all cases, the energy consumption remains reasonably low, typically units or few tens of fJ/bit under low-bias states. This makes hetero-structured Si-Ge-Si pin photodetectors promising for use in energy-efficient Si-based optical interconnects.

Fig. 7. Eye diagram apertures of 0.8 μm-wide by 40 μm-long pin photodetector under a 1 V reverse bias and an optical input power coupled into the device of -9 dBm. Large-signal data link inspections are performed for different data rates of (a) 10 Gbps, (b) 20 Gbps, (c) 25 Gbps, (d) 28 Gbps, (e) 32 Gbps, and (f) 40 Gbps. Insets: Reference eye diagrams. Here, x [ps/div] and y [mV/div] are horizontal and vertical axes of the scope, respectively.

Figure 7 shows the eye diagrams of a 0.8 μm-wide and 40 μm-long hetero-structured pin photodetector biased at -1 V for different transmission data rates, from 10 Gbps up to 40 Gbps. Reference eye diagram apertures are shown as insets in Fig. 7. Eye diagrams remain open, even for data rates beyond 25 Gbps, which is promising for the future on-chip detection of high-speed signal traffic. At a data rate of 40 Gbps, the pin photodetector operates in the voltage-limited regime, since the eye diagram begins to close. Indeed, the small-signal RF measurements have reported that the -3-dB bandwidth was around 16 GHz (under -1 V). This result explains the eye diagram aperture trends and perfectly agrees with performed large-signal optical link measurements. For 32 Gbps (see Fig. 7(e)), the eye diagram is still clearly open, while for 40 Gbps, it starts to have a closure. Moreover, energy consumption is predicted to be, for this photodetector and under a 1 V reverse bias, as low as 9.8 fJ/bit and 2.4 fJ/bit for 10 Gbps and 40 Gbps optical link rates, respectively.

IV. CONCLUSION

To summarize, we comprehensively studied the optoelectrical properties of waveguide-integrated pin detectors with lateral Si-Ge-Si heterojunctions. Such devices take full advantage of an easier integration scheme than that of Ge homo-junction photo-detectors. Such photodetectors are promising for use in nanophotonics as they are (i) built upon abundantly available materials, (ii) power-friendly and (iii) easily driven by low-voltage supplies, resulting in competitive

opto-electrical performances. They are promising for use in future energy-efficient 40 Gbps optical communication links.

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