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Effect of testing conditions on the thermal diffusivity measurements of nuclear fuels via the flash method

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Context and objectives

$$\lambda(T) = \alpha(T) \cdot C_p(T) \cdot \rho(T)$$

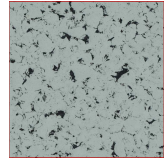
α : thermal diffusivity
 $C_p(T)$: heat capacity
 $\rho(T)$: density

Thermal conductivity of the nuclear fuel :

- A key parameter to understand the performance of the fuel under irradiation
- Highly dependent on microstructure, porosity and its distribution...
- Influences almost all important processes such as fission gas release, swelling...

Knowledge of the nuclear fuel thermal conductivity (derived from a thermal diffusivity measurement) :

- A fundamental data for a better prediction of its performance in reactor
- **Must be measured accurately** (including a reliable uncertainty assessment)



Determination of thermal diffusivity by the flash method with a LFA 467 HyperFlash® NETZSCH apparatus

Principle : heating of the front surface of a **plane-parallel sample** by a **short energy light pulse** and measurement of the **resulting temperature excursion** of the rear face

Technical data

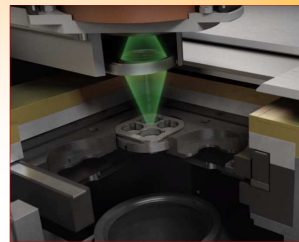
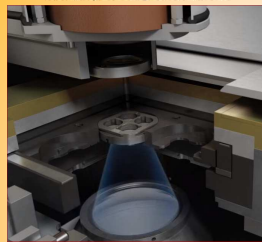
Temperature range from ambient to 500 °C
Xenon-pulse delivery source
Liquid nitrogen-cooled InSb **IR detector**
ZoomOptics system (optimized field of view)
Gas control unit
Range of measurement : 0,01 to 1000 mm².s⁻¹
Accuracy : ± 3 %
Repeatability ± 2 %

Description of the Flash method

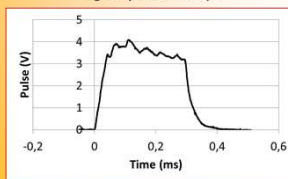
a transient heat flux technique

Heat pulse generation

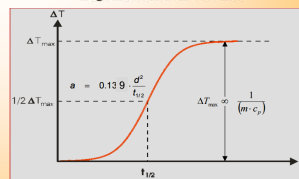
Optical detection



Light pulse shape



Signal measurement



Test specimens

Thin ceramic samples (~ 2 µm thick)

- different shapes (circular, square, rectangular)
- different sizes
(8 to 12.7 mm in diameter or side length)
- Deposit of an opaque layer on both faces to allow full absorption of the energy pulse
↳ tungsten or gold coated and graphite sprayed
dense **Pyroceram® 9606** (BCR -724, standard)
↳ graphite sprayed porous **uranium dioxide** (obtained by a powder metallurgy route)

Sample holders

- ↳ Steel supports, designed for each sample geometry
- ↳ Loosely thermally coupled to the specimen



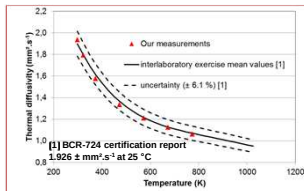
Thermal diffusivity identification

- Fitting of a calculated model to experimental data (**Proteus®** software)
- ↳ Ideal case : **adiabatic model** (no heat loss)
- ↳ **Cowan model**: 1-D mode, purely axial heat transfer (no radial losses)
- ↳ Improved **Cape & Lehman model** : 2-D axial-symmetric mode, (radial and facial losses)

Experimental data

Verification

BCR-724 certified thermal diffusivity

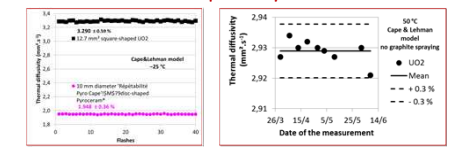


Interlaboratory comparisons

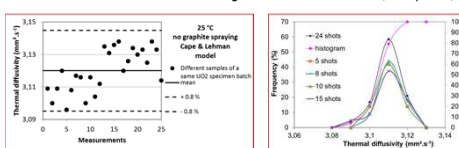
Pyroceram® sample	Our measurements	LINE measurements	Netzsch measurements
10 mm disc-shaped	Cowan model: 1.969 ± 0.003 Cape Lehman model: 1.948 ± 0.004	1.94	/
12.7 mm disc-shaped	Cowan model: 1.940 ± 0.004 Cape Lehman model: 1.926 ± 0.006	/	Cowan model: 1.952 ± 0.007

Good reproducibility

Repeatability



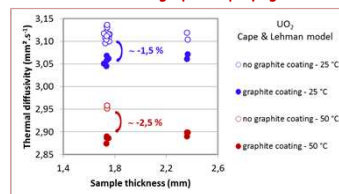
NB: A measurement result is the average of several shot results (usually ~ 20)



Within-batch repeatability better than 1%
Repeatability better than 1%

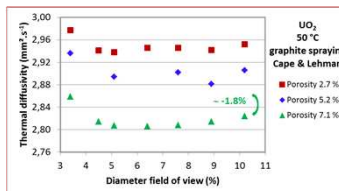
Effect of testing conditions

Effect of graphite spraying

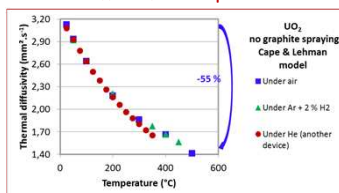


- ✓ Clear dependence on the sample preparation
- ✓ Choice of spraying on both faces of the sample

Effect of the field of view

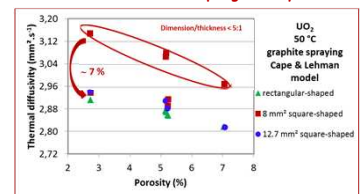


Effect of the temperature



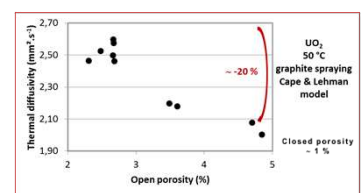
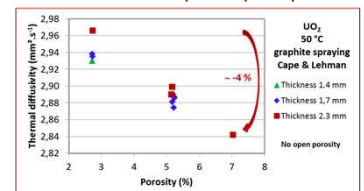
Effect of material characteristics

Effect of the sample geometry



- ✓ Slightly higher apparent diffusivity for 8 mm² square-shaped samples (differences between geometries not taken into account in the proposed models)
- ✓ Dimension to thickness ratio must be > 5:1

Effect of the specimen porosity



Strong dependence on the open porosity

Conclusions

- ✓ Flash method → **Appropriate to discriminate differences in the thermal diffusivity measurements of UO₂ samples** caused by a variation of the porosity
- ✓ **Recommendations for the operating conditions** : geometry (dimension to thickness ratio > 5:1) and preparation of the samples (graphite spraying on both faces)

Perspectives

- ✓ Carrying out of tests under different atmospheres (**prevention of the oxidation of UO₂ at temperatures > 300°C**)
- ✓ Evaluation of the **effect of the fabrication process/material structure**
- ✓ Use of image analysis in order to **quantify the pore size morphology and distribution** and to correlate these data with the thermal diffusivity measurements