Combined face based and nodal based discretizations on hybrid meshes for non-isothermal two-phase Darcy flow problems

Laurence Beaude, Roland Masson, Simon Lopez, Pierre Samier

To cite this version:
Laurence Beaude, Roland Masson, Simon Lopez, Pierre Samier. Combined face based and nodal based discretizations on hybrid meshes for non-isothermal two-phase Darcy flow problems. 2018. <hal-01832659>
Combined face based and nodal based discretizations on hybrid meshes for non-isothermal two-phase Darcy flow problems

L. Beaude, R. Masson, S. Lopez, P. Samier

Abstract

In the last 20 years many discretization schemes have been developed to approximate the Darcy fluxes on polyhedral cells in heterogeneous anisotropic porous media. Among them, we can distinguished cell based approaches like the Two Point Flux Approximation (TPFA) or the Multi Point Flux Approximation (MPFA) schemes, face based approaches like the Hybrid Finite Volume (HFV) scheme belonging to the family of Hybrid Mimetic Mixed methods and nodal based discretizations like the Vertex Approximate Gradient (VAG) scheme. They all have their own drawbacks and advantages which typically depend on the type of cells and on the anisotropy of the medium. In this work, we propose a new methodology to combine the VAG and HFV discretizations on arbitrary subsets of cells or faces in order to choose the best suited scheme in different parts of the mesh. In our approach the TPFA discretization is considered as an HFV discretization for which the face unknowns can be eliminated. The coupling strategy is based on a node to face interpolation operator at the interfaces which must be chosen to ensure the consistency, the coercivity and the limit conformity properties of the combined discretization. The convergence analysis is performed in the gradient discretization framework and convergence is proved for arbitrary cell or face partitions of the mesh. For face partitions, an additional stabilisation local to the cell is required to ensure the coercivity while for cell partitions no additional stabilisation is needed. The framework preserves at the interface the discrete conservation properties of the VAG and HFV.

*we would like to thank the BRGM and the Provence-Alpes-Côte d’Azur Region for co-funding the PhD of Laurence Beaude as well as the support of the CHARMS ANR project (ANR-16-CE06-0009)
schemes with fluxes based on local to each cell transmissibility matrices. This discrete conservative form allows to naturally extend the VAG and HFV discretizations of two-phase Darcy flow models to the combined VAG-HFV schemes. The efficiency of our approach is tested for single phase and immiscible two-phase Darcy flows on 3D meshes using a combination of the HFV and VAG discretizations as well as for non-isothermal compositional liquid gas Darcy flows on a vertical 2D cross-section of the Bouillante geothermal reservoir (Guadeloupe) using a combination of the TPFA and VAG discretizations.

**Keywords:** Finite Volume, Gradient discretization, Darcy flow, two-phase Darcy flow, hybrid meshes

### Introduction

The simulation of compositional multi-phase Darcy flow in heterogeneous porous media plays a major role in many applications. In the oil and gas sector, compositional multi-phase Darcy flow simulations are paramount to predict and optimize reservoir production. In sedimentary basin modelling, such models are used to simulate the migration of hydrocarbon phases, over geological space and time scales, from source rock to traps in geological formations. In CO₂ geological storage, compositional multi-phase Darcy flow models allow to optimize the injection of CO₂ and to evaluate the integrity of the storage. Two-phase compositional Darcy flow models are used to study the gas migration and to assess the long term safety of nuclear waste storages. Finally, coupling such models with the energy conservation equation lead to practical applications for both exploration and production phases of geothermal operations.

The standard industrial answer to cope with the strong coupling of both an elliptic (or parabolic) unknown, the pressure, and hyperbolic (or degenerate parabolic) unknowns, the volume and mole fractions, is based on finite volume spatial discretization, which is efficiently combined with an Euler implicit time integration to allow for sufficiently large time steps [4, 22]. A major difficulty is linked to the finite volume discretization of the Darcy fluxes on the complex geometry and geology encountered in practical problems typically including fault networks, pinch-out, heterogeneities and spatially varying anisotropies of the medium. The classical cell-centred Two-Point Flux Approximation (TPFA) widely used in industrial simulators is cheap and robust but its consistency requires strong orthogonality conditions on the mesh which cannot be achieved for complex geological models. In the last 20 years, these restrictions have motivated an active research on the de-
velopment of new discretization schemes to approximate the Darcy fluxes on polyhedral cells and in heterogeneous anisotropic porous media [18, 13]. Still relying on the cell-centred approximation, Multi-Point Flux Approximations (MPFA) extend TPFA to consistent discretizations on general meshes with anisotropic heterogeneous media [1, 14]. Yet, MPFA schemes are mesh and anisotropy conditionally stable and exhibit a very large stencil on simplictic meshes. Alternatively, nodal discretizations such as the Control Volume Finite Element (CVFE) method [19] and the Vertex Approximate Gradient (VAG) scheme [15, 18, 23] are unconditionally coercive and very efficient on simplictic meshes thanks to their nodal based approximation. Finally, face based discretizations such as the Hybrid Finite Volume (HFV) scheme [16] belonging to the family of Hybrid Mixed Mimetic (HMM) methods [12], or the Mixed Hybrid Finite Element method, have been developed and adapted to multi-phase Darcy flows in [3, 2]. They provide accurate and unconditionally stable discretizations of the Darcy fluxes but, due to the large number of faces, remain rather expensive compared with nodal or cell-centred approaches.

Roughly speaking, all these discretizations of the Darcy fluxes have their own drawbacks and advantages which typically depend on the mesh characteristics and on the anisotropy of the medium. In this work, we propose a new methodology which combines nodal based and face based discretizations on arbitrary subsets of cells or faces in order to adapt the choice of the scheme in different parts of the mesh. In our approach, the TPFA is considered as a face based HFV scheme for which the face unknowns can be eliminated assuming that the mesh satisfies the superadmissibility property with anisotropy aligned with the mesh directions (see Lemma 2.1 of [16]). The VAG scheme is chosen as our nodal approximation since it shares a common data structure with the HFV scheme based on local to each cell transmissibility matrices. It has also the advantage, compared with more classical nodal discretizations such as CVFE, to avoid the mixing of rocktypes at nodal control volumes [18, 23].

We consider two types of strategies to couple the VAG and HFV (TPFA) discretizations. The first one is based on a partition of the cells, each cell using either nodal or face unknowns. The second approach can be extended to more general partitions of the mesh based on faces, each face using either face or nodal unknowns. In both cases, the coupling is performed using a node to face interpolation operator at interfaces which must be chosen to ensure the consistency, the coercivity and the limit conformity properties of the combined VAG-HFV discretizations. The convergence analysis is performed in the gradient discretization framework [15, 12, 10] and convergence
is proved for arbitrary cell or face partitions of the mesh. For face partitions, an additional stabilisation is required to ensure the coercivity while for cell partitions no additional stabilisation is needed and the stability is obtained at the interface thanks to the neighboring VAG cells.

At the interface, the framework preserves the discrete conservation properties of the VAG and HFV schemes with fluxes based on local to each cell transmissibility matrices which size is the number of selected nodes or/and faces on the shared boundary. This discrete conservative form leads to a natural extension of the VAG and HFV discretizations of multi-phase Darcy flow models to the combined VAG-HFV schemes.

The remainder of this paper is organized as follows. Section 1 focuses on the discretization of second order diffusion problems. It introduces our framework based, to fix ideas, on a partition of the cells into VAG, HFV and interface cells. Then, two gradient schemes are built combining the VAG and HFV schemes in their respective subset of cells coupled with two possible choices of matching discretizations in the interface cells. The stability and convergence of both discretizations are proved using the gradient discretization framework and the convergence is assessed numerically on various types of hybrid 3D meshes and compared with the standalone VAG and HFV discretizations. Using the discrete fluxes connecting each cell to its node or/and face boundary degrees of freedom, the VAG-HFV discretizations are extended to immiscible two-phase Darcy flows in Section 2. Then, numerical tests investigate, on a 1D two-phase flow reference solution, the convergence and efficiency of the VAG-HFV schemes compared with the standalone VAG and HFV discretizations. Section 3 considers the extension of the VAG-HFV discretizations to non-isothermal compositional liquid gas Darcy flows based on the formulation introduced in [5]. Finally, the model and its VAG-TPFA discretization are tested on a simplified two dimensional cross-section of the Bouillante high temperature geothermal reservoir with an hybrid cartesian triangular mesh. A reference solution, computed on a refined mesh, is compared in terms of accuracy and CPU time with the solutions obtained with the VAG scheme on a triangular mesh and the TPFA scheme on a Voronoi mesh.
1 Two Gradient discretizations combining the VAG and HFV schemes

Let us consider a domain $\Omega \subset \mathbb{R}^d$, with $d = 2, 3$ the space dimension, and the following second order diffusion equation looking for the potential $u \in H^1_0(\Omega)$ and the velocity $q \in \text{H}_{\text{div}}(\Omega)$ such that

$$\begin{cases} \text{div}(q) = f & \text{on } \Omega, \\ q = -\Lambda \nabla u & \text{on } \Omega. \end{cases}$$

(1)

In (1), $f \in L^2(\Omega)$ is the source term and $\Lambda \in L^\infty(\Omega)^{d \times d}$ is the diffusion tensor such that there exist $\underline{k} \geq \overline{k} > 0$ with

$$\underline{k} |\xi|^2 \leq (\Lambda(x)\xi, \xi) \leq \overline{k} |\xi|^2 \text{ for all } \xi \in \mathbb{R}^d, x \in \Omega.$$

The primal weak formulation of (1) amounts to find $u \in H^1_0(\Omega)$ satisfying the following variational equality for all $v \in H^1_0(\Omega)$

$$\int_{\Omega} \Lambda(x) \nabla u(x) \nabla v(x) dx = \int_{\Omega} f(x)v(x) dx.$$  (2)

It admits a unique solution from the Lax Milgram theorem.

1.1 Polyhedral mesh and partition of the mesh

Following [15], we consider generalized polyhedral meshes of $\Omega$. Let $\mathcal{M}$ be the set of cells that are disjoint open subsets of $\Omega$ such that $\bigcup_{K \in \mathcal{M}} K = \overline{\Omega}$. For all $K \in \mathcal{M}$, $x_K$ denotes the so-called “centre” of the cell $K$ under the assumption that $K$ is star-shaped with respect to $x_K$. Let $\mathcal{F}$ denote the set of faces of the mesh. The faces are not assumed to be planar for the VAG discretization, hence the term “generalized polyhedral cells”, but they need to be planar for the HFV discretization. We denote by $\mathcal{V}$ the set of vertices of the mesh. Let $\mathcal{V}_K$, $\mathcal{F}_K$, $\mathcal{V}_\sigma$ respectively denote the set of vertices of $K \in \mathcal{M}$, faces of $K$ and vertices of $\sigma \in \mathcal{F}$. The set of edges of the mesh is denoted by $\mathcal{E}$ and $\mathcal{E}_\sigma$ denotes the set of edges of the face $\sigma \in \mathcal{F}$. Let $\mathcal{M}_\sigma$ denote the set of cells sharing the face $\sigma \in \mathcal{F}$. We denote by $\mathcal{F}_{\text{ext}}$ the subset of faces $\sigma \in \mathcal{F}$ such that $\mathcal{M}_\sigma$ has only one element and we set $\mathcal{E}_{\text{ext}} = \bigcup_{\sigma \in \mathcal{F}_{\text{ext}}} \mathcal{E}_\sigma$ and $\mathcal{V}_{\text{ext}} = \bigcup_{\sigma \in \mathcal{F}_{\text{ext}}} \mathcal{V}_\sigma$. The mesh is assumed to be conforming in the sense that for all $\sigma \in \mathcal{F} \setminus \mathcal{F}_{\text{ext}}$, the set $\mathcal{M}_\sigma$ contains exactly two cells. It is assumed that, for each face $\sigma \in \mathcal{F}$, there exists a so-called “centre” $x_\sigma$ of the face such that

$$x_\sigma = \sum_{s \in \mathcal{V}_\sigma} \beta_{\sigma,s} \ x_s, \text{ with } \sum_{s \in \mathcal{V}_\sigma} \beta_{\sigma,s} = 1,$$
where $\beta_{\sigma,s} \geq 0$ for all $s \in \mathcal{V}_\sigma$. The face $\sigma$ is assumed to match with the union of the triangles $T_{\sigma,e}$ defined by the face centre $x_\sigma$ and each of its edge $e \in \mathcal{E}_\sigma$.

A tetrahedral submesh of $\mathcal{M}$ is defined by

$$\mathcal{T} = \{T_{K,\sigma,e}, e \in \mathcal{E}_\sigma, \sigma \in \mathcal{F}_K, K \in \mathcal{M}\},$$

where $T_{K,\sigma,e}$ is the tetrahedron joining the cell centre $x_K$ to the triangle $T_{\sigma,e}$. Let $\rho_T$ denote the insphere diameter of a given tetrahedron $T$, $h_T$ its diameter and $h_T = \max_{T \in \mathcal{T}} h_T$. We will assume in the convergence analysis that the family of tetrahedral submeshes $\mathcal{T}$ is shape regular. Hence let us define the following shape regularity parameter of the mesh by

$$\theta_T = \max_{T \in \mathcal{T}} \frac{h_T}{\rho_T}. \quad (3)$$

The following combination of the VAG and HFV discretizations is based on the choice of a subset of cells $\mathcal{M}^v \subset \mathcal{M}$ on which the VAG discretization is used. Then, we define the subset of interfacial faces $\mathcal{F}^{hv} \subset \mathcal{F} \setminus \mathcal{F}_{ext}$ by

$$\mathcal{F}^{hv} = \{\sigma \in \mathcal{F} \setminus \mathcal{F}_{ext} \mid K \in \mathcal{M}^v, L \not\in \mathcal{M}^v \text{ or } L \in \mathcal{M}^v, K \not\in \mathcal{M}^v \text{ with } \mathcal{M}_\sigma = \{K, L\}\},$$

and the set of interface cells $\mathcal{M}^{hv}$ by

$$\mathcal{M}^{hv} = \{K \in \mathcal{M} \setminus \mathcal{M}^v \mid \mathcal{F}_K \cap \mathcal{F}^{hv} \neq \emptyset\}. \quad (4)$$

The subset of HFV cells on which the HFV discretization is used is finally defined by

$$\mathcal{M}^h = \mathcal{M} \setminus (\mathcal{M}^v \cup \mathcal{M}^{hv}),$$

such that $\mathcal{M}^v, \mathcal{M}^h, \mathcal{M}^{hv}$ defines a partition of the set of cells $\mathcal{M}$ (see Figure 1). We also define the following subsets of nodes and faces

$$\mathcal{V}^v = \bigcup_{K \in \mathcal{M}^v} \mathcal{V}_K, \quad \mathcal{V}^{hv} = \bigcup_{\sigma \in \mathcal{F}^{hv}} \mathcal{V}_\sigma, \quad \mathcal{F}^h = \left( \bigcup_{K \in \mathcal{M}^h \cup \mathcal{M}^{hv}} \mathcal{F}_K \right) \setminus \mathcal{F}^{hv},$$

and

$$\mathcal{V}_{ext}^v = \mathcal{V}_{ext} \cap \mathcal{V}^v, \quad \mathcal{F}_{ext}^h = \mathcal{F}_{ext} \cap \mathcal{F}^h.$$

For all $\sigma \in \mathcal{F}^h \cup \mathcal{F}^{hv}$, it is assumed in the following that the face $\sigma$ is planar and that $x_\sigma$ is the centre of gravity of $\sigma$. \textit{\ldots}
1.2 Combining the VAG and HFV discretizations using the gradient discretization framework

The junction between the VAG and HFV discretizations is obtained using the gradient discretization framework introduced in [15, 12, 10]. This framework is based on the definition of a vector space of discrete unknowns $X_D$, of a function reconstruction operator

$$
\Pi_D : X_D \rightarrow L^2(\Omega),
$$

and of a gradient reconstruction operator

$$
\nabla_D : X_D \rightarrow (L^2(\Omega))^d.
$$

The subspace of $X_D$ incorporating homogeneous Dirichlet boundary conditions is denoted by $X^0_D$. Then, the discretization of our model problem (2) is obtained by the following variational formulation: find $u_D \in X^0_D$ such that

$$
\int_{\Omega} \Lambda(x) \nabla_D u_D(x) \nabla_D v_D(x) dx = \int_{\Omega} f(x) \Pi_D v_D(x) dx
$$

for all $v_D \in X^0_D$. It admits a unique solution as soon as $\| \cdot \|_D = \| \nabla_D \cdot \|_{(L^2(\Omega))^d}$ defines a norm on $X^0_D$.

As exhibited in Figure 1, our construction is based on the following set of degrees of freedom (d.o.f.)

$$
dof_D = \{ K \in \mathcal{M} \} \cup \{ s \in \mathcal{V}^v \} \cup \{ \sigma \in \mathcal{F}^h \},
$$

the associated vector space $X_D$ of discrete unknowns

$$
X_D = \{ u_\nu \in \mathbb{R} \mid \nu \in dof_D \},
$$

and its subspace

$$
X^0_D = \{ u_D \in X_D \mid u_s = 0, u_\sigma = 0, s \in \mathcal{V}^v_{ext}, \sigma \in \mathcal{F}^h_{ext} \}.
$$

Let us also define the subsets of d.o.f. located at the boundary of a given cell $K \in \mathcal{M}$ as

$$
dof_K = \begin{cases} 
(F_K \setminus F^{hv}) \cup (\mathcal{V}_K \cap \mathcal{V}^{hv}) & \text{if } K \in \mathcal{M}^{hv}, \\
F_K & \text{if } K \in \mathcal{M}^h, \\
\mathcal{V}_K & \text{if } K \in \mathcal{M}^v.
\end{cases}
$$
The function reconstruction operator is based on an arbitrary partition \( \{D_K, D_{K,\nu}, \nu \in \text{dof}_K\} \) of each cell \( K \in \mathcal{M} \) and is defined by

\[
\Pi_D u_D(x) = \begin{cases} 
  u_K, & \text{for all } x \in D_K, \text{ for all } K \in \mathcal{M}, \\
  u_\nu, & \text{for all } x \in D_{K,\nu}, \text{ for all } K \in \mathcal{M}, \nu \in \text{dof}_K, 
\end{cases}
\]

(8)

with \( D_{K,\nu} = \emptyset \) for all \( \nu \in \mathcal{V}^w_{\text{ext}} \cup \mathcal{F}^h_{\text{ext}} \). The gradient reconstruction operator is defined cellwise by

\[
\nabla_D u_D(x) = \begin{cases} 
  \nabla^v_K u_D(x) & \text{for all } x \in K, K \in \mathcal{M}^v, \\
  \nabla^h_K u_D(x) & \text{for all } x \in K, K \in \mathcal{M}^h, \\
  \nabla^{hv}_K u_D(x) & \text{for all } x \in K, K \in \mathcal{M}^{hv}. 
\end{cases}
\]

(9)

It is based on the VAG gradient reconstruction operator \( \nabla^v_K \) for all VAG cells \( K \in \mathcal{M}^v \) and on the HFV gradient reconstruction operator \( \nabla^h_K \) for all HFV cells \( K \in \mathcal{M}^h \). On the interface cells \( K \in \mathcal{M}^{hv} \), the gradient reconstruction operator \( \nabla^{hv}_K \) must be built to guarantee that the gradient discretization \( (X_D, \nabla_D, \Pi_D) \) satisfies the coercivity, consistency and limit conformity properties of the gradient discretization framework, ensuring the well-posedness and convergence of the scheme (see [15, 12, 10] and subsection 1.3 below).

1.2.1 VAG gradient reconstruction operator

Following [17], a \( P_1 \) finite element discretization is built using the tetrahedral submesh \( \mathcal{T} \) of \( \mathcal{M} \) and a second order interpolation at the face centres \( \mathbf{x}_\sigma \),
\[ \sigma \in \mathcal{F} \setminus \mathcal{F}^h \text{ defined for } u_D \in X_D \text{ by} \]

\[ u_\sigma = \sum_{s \in V_\sigma} \beta_{\sigma,s} u_s. \]

For a given \( u_D \in X_D \), we define the function \( \Pi_T u_D \) on \( \bigcup_{K \in \mathcal{M}} K \) as the continuous piecewise affine function on each tetrahedron of \( T \) included in \( \bigcup_{K \in \mathcal{M}} K \) such that \( \Pi_T u_D(x_K) = u_K \), \( \Pi_T u_D(x_s) = u_s \), and \( \Pi_T u_D(x_\sigma) = \sum_{s \in V_\sigma} \beta_{\sigma,s} u_s \) for all \( K \in \mathcal{M}^v \), \( s \in V^v \) and \( \sigma \in \mathcal{F} \setminus \mathcal{F}^h \). The VAG gradient reconstruction operator is obtained from this finite element discretization by setting

\[ \nabla_v u_D(x) = \nabla \Pi_T u_D(x) \text{ for all } x \in K, K \in \mathcal{M}^v. \tag{10} \]

### 1.2.2 HFV gradient reconstruction operator

We follow the construction presented in [16]. As shown in [11] it can be generalized as the family of Hybrid Mimetic Methods covering in the same framework Mimetic Finite Difference, Hybrid Finite Volume and Mixed Finite Volume Methods. For \( K \in \mathcal{M} \), let us set \( U_K = (u_K, u_\sigma, \sigma \in \mathcal{F}_K) \in \mathbb{R}^{\#\mathcal{F}_K + 1} \) and define

\[ \nabla_K U_K = \frac{1}{|K|} \sum_{\sigma \in \mathcal{F}_K} |\sigma| (u_\sigma - u_K) n_{K,\sigma}, \]

where \( |K| \) is the volume of the cell \( K \), \( |\sigma| \) is the surface of the face \( \sigma \), and \( n_{K,\sigma} \) is the unit normal vector of the face \( \sigma \in \mathcal{F}_K \) oriented outward of the cell \( K \). Let us remark that \( \nabla_K U_K \) does not depend on \( u_K \) since \( \sum_{\sigma \in \mathcal{F}_K} |\sigma| n_{K,\sigma} = 0 \). Hence a stabilised gradient reconstruction is defined as follows:

\[ \nabla_{K,\sigma} U_K = \nabla_K U_K + \frac{1}{\sqrt{d} |K_\sigma|} R_{K,\sigma}(U_K) n_{K,\sigma}, \sigma \in \mathcal{F}_K, \]

with

\[ R_{K,\sigma}(U_K) = u_\sigma - u_K - \nabla_K U_K \cdot (x_\sigma - x_K), \]

where \( K_\sigma \) is the cone joining the face \( \sigma \) to the cell centre \( x_K \) and \( |K_\sigma| \) its \( d \)-dimensional measure. It leads to the definition of the HFV gradient reconstruction operator for \( u_D \in X_D \) as

\[ \nabla^h_{K} u_D(x) = \nabla_{K,\sigma} U_K \text{ for all } x \in K_\sigma, K \in \mathcal{M}^h, \sigma \in \mathcal{F}_K. \tag{11} \]

Note that the weight \( \frac{1}{\sqrt{d}} \) is chosen in order to recover the gradient reconstruction corresponding to the two point flux approximation in the case of a superadmissible mesh (see Lemma 2.1 of [16]).
1.2.3 First gradient reconstruction operator in the interface cells

Our first construction is based on a second order interpolation of the face unknown \( u_\sigma \) at the centre of gravity \( x_\sigma \) for each face \( \sigma \in \mathcal{F} \) defined by

\[
u_\sigma = \frac{1}{|\sigma|} \int_\sigma \Pi_T u_D(x) d\sigma(x).
\]

Since \( x_\sigma \) is the centre of gravity of the face \( \sigma \), it results that

\[
u_\sigma = \sum_{s \in V_\sigma} \beta_{\sigma,s} u_s.
\]

Then we set for \( u_D \in X_D \),

\[
U_K = \left(u_K, u_\sigma = \frac{1}{|\sigma|} \int_\sigma \Pi_T u_D(x) d\sigma(x), \sigma \in \mathcal{F}_K \cap \mathcal{F}^{hv}, u_{\sigma_1}, \sigma \in \mathcal{F}_K \setminus \mathcal{F}^{hv}\right),
\]

and

\[
\nabla^{hv}_K u_D(x) = \nabla_{K,\sigma} U_K \text{ for all } x \in K_{\sigma}, K \in \mathcal{M}^{hv}, \sigma \in \mathcal{F}_K.
\] (12)

1.2.4 Second gradient reconstruction operator in the interface cells

The second construction combines the previous interpolation at the faces \( \sigma \in \mathcal{F}^{hv} \) with a stabilisation of the cell gradient. As previously, for \( u_D \in X_D \), let us set

\[
U_K = \left(u_K, u_\sigma = \frac{1}{|\sigma|} \int_\sigma \Pi_T u_D(x) d\sigma(x), \sigma \in \mathcal{F}_K \cap \mathcal{F}^{hv}, u_{\sigma_1}, \sigma \in \mathcal{F}_K \setminus \mathcal{F}^{hv}\right).
\]

Then we rewrite the constant gradient \( \nabla_K U_K \) as

\[
\nabla_K U_K = \sum_{\nu \in \text{dof}_K} (u_\nu - u_K) b_{K,\nu},
\]

with

\[
\left\{
\begin{array}{l}
b_{K,\sigma} = \frac{|\sigma|}{|K|} n_{K,\sigma} \text{ for } \sigma \in \mathcal{F}_K \setminus \mathcal{F}^{hv}, \\
b_{K,s} = \sum_{\{\sigma \in \mathcal{F}_K \cap \mathcal{F}^{hv} \mid s \in V_\sigma\}} \beta_{\sigma,s} \frac{|\sigma|}{|K|} n_{K,\sigma} \text{ for } s \in V_K \cap V^{hv}.
\end{array}
\right.
\]

This gradient does not actually depend on \( u_K \) and must be stabilised using the residual

\[
R_{K,\nu}(u_D) = u_\nu - u_K - \nabla_K U_K \cdot (x_\nu - x_K),
\]
and, for each $\nu \in \text{dof}_K$, the new gradient

$$\nabla_{K,\nu} u_D = \nabla_K U_K + \gamma_{K,\nu} R_{K,\nu}(u_D) b_{K,\nu}.$$  

It leads to define the stabilised gradient

$$\nabla^h_{K} u_D(x) = \nabla_{K,\nu} u_D \text{ for all } x \in \omega_{K,\nu}, K \in \mathcal{M}^h, \nu \in \text{dof}_K. \quad (13)$$

where the weights $(\gamma_{K,\nu})_{\nu \in \text{dof}_K}$ and the partition $(\omega_{K,\nu})_{\nu \in \text{dof}_K}$ of the cell $K \in \mathcal{M}^h$ are such that

$$\begin{cases}
\omega_{K,\sigma} = K_\sigma \text{ for } \sigma \in \mathcal{F}_K \setminus \mathcal{F}^h, \\
|\omega_{K,s}| = \frac{\sum_{\sigma \in \mathcal{F}_K \cap \mathcal{F}^h} |K_\sigma|}{\#(\mathcal{V}_K \cap \mathcal{V}^h)} \text{ for } s \in \mathcal{V}_K \cap \mathcal{V}^h,
\end{cases}$$

and

$$\begin{cases}
\gamma_{K,\sigma} = \frac{1}{\sqrt{d} |K_\sigma|} \text{ for } \sigma \in \mathcal{F}_K \setminus \mathcal{F}^h, \\
\gamma_{K,s} = \frac{1}{\sqrt{d} |\omega_{K,s}|} \text{ for } s \in \mathcal{V}_K \cap \mathcal{V}^h,
\end{cases}$$

such that $\gamma_{K,\nu} |\omega_{K,\nu}| = \frac{1}{\sqrt{d} |K|}$ for all $\nu \in \text{dof}_K$. Note that, as soon as the diffusion tensor $\Lambda(x)$ is cellwise constant, only the $d$-dimensional measures of the sets $\omega_{K,\nu}$, $\nu \in \text{dof}_K$ are used.

**Remark 1.1** This second gradient reconstruction (13) based on interpolation and stabilisation can be applied as a standalone discretization in all cells provided that a partition of the faces $\sigma \in \mathcal{F}$ between those with a face unknown $u_\sigma$ and those with node unknowns $u_s, s \in \mathcal{V}_\sigma$ is given. The situation is different for the first gradient reconstruction (12) based only on interpolation which leads to a stable discretization thanks to the neighboring VAG cells (see Subsection 1.3). For example, if all faces are with node unknowns, it is clear that the first construction, if applied to all cells, will lead to an unstable discretization while the second construction reduces to the VAG discretization presented in [15] which differs from the VAG gradient reconstruction defined by (10).

### 1.2.5 Conservative formulation

From the cellwise definition of the gradient reconstruction, one can define the cell transmissibility symmetric positive matrices $T_K \in \mathbb{R}^{\text{dof}_K \times \text{dof}_K}$, $K \in \mathcal{M}$ such that
\[ \int_{\Omega} \mathbf{A}(x) \nabla_D u_D(x) \nabla_D v_D(x) \, dx = \sum_{K \in \mathcal{M}} \sum_{\nu \in \text{dof}_K} \sum_{\nu' \in \text{dof}_K} T^\nu_{K,\nu'} (u_{\nu'} - u_K)(v_{\nu'} - v_K), \]

with
\[ T^\nu_{K,\nu'} = \int_K \mathbf{A}(x) \nabla_D u_D^{(\nu)}(x) \nabla_D v_D^{(\nu)}(x) \, dx, \]

where \( w^{(\nu)}_\mu = \delta^{\nu}_\mu \) for all \((\nu, \mu) \in \text{dof}_D \times \text{dof}_D\). Let us define the following fluxes connecting each cell \( K \in \mathcal{M} \) to its boundary d.o.f. \( \nu \in \text{dof}_K \)

\[ F_{K,\nu}(u_D) = \sum_{\nu' \in \text{dof}_K} T^\nu_{K,\nu'} (u_K - u_{\nu'}). \quad (14) \]

Then, the gradient scheme (4) can be formulated as a set of discrete conservation equations as follows: find \( u_D \in X^0_D \) such that

\[
\begin{cases}
\sum_{\nu \in \text{dof}_K} F_{K,\nu}(u_D) = \int_{D_K} f(x) \, dx \text{ for all } K \in \mathcal{M}, \\
\sum_{K \in \mathcal{M} | \nu \in \text{dof}_K} -F_{K,\nu}(u_D) = \sum_{K \in \mathcal{M} | \nu \in \text{dof}_K} \int_{D_{K,\nu}} f(x) \, dx \\
\quad \quad \quad \text{for all } \nu \in (\mathcal{F}^h \cup \mathcal{V}^v) \setminus (\mathcal{F}^h_{ext} \cup \mathcal{V}^v_{ext}).
\end{cases} \quad (15)
\]

Each cell unknown \( u_K \) can be eliminated from the first equation in (15) which depends only on \( u_K \) and \( u_{\nu'} \), \( \nu \in \text{dof}_K \). It leads to a Schur complement linear system without any fill-in depending only on the face and node unknowns \( u_{\nu} \) for \( \nu \in \mathcal{F}^h \cup \mathcal{V}^v \).

**Remark 1.2** For the first construction, given \( T^K_h \in \mathbb{R}^{\mathcal{F}_K \times \mathcal{F}_K} \), the HFV transmissibility matrix of the cell \( K \in \mathcal{M}^{hv} \), then the transmissibility matrix \( T_K \) can be easily computed by

\[ T_K = (A_K)^t T^K_h A_K, \quad (16) \]

where \( A_K \in \mathbb{R}^{\mathcal{F}_K \times \text{dof}_K} \) is such that \((A_K)_{\sigma,\nu} = \delta^{\nu}_\sigma \) for all \( \sigma \in \mathcal{F}_K \cap \mathcal{F}^h \), \( \nu \in \text{dof}_K \), \((A_K)_{\sigma,s} = \beta_{\sigma,s} \) for all \( \sigma \in \mathcal{F}_K \cap \mathcal{F}^{hv} \), \( s \in \mathcal{V}_s \), and \((A_K)_{\sigma,\nu'} = 0 \) for all \( \sigma \in \mathcal{F}_K \cap \mathcal{F}^{hv} \), \( \nu' \in \text{dof}_K \setminus \mathcal{V}_s \).

**Remark 1.3** The cell transmissibility matrix \( T_K \) is Symmetric Positive Definite (SPD) for all \( K \in \mathcal{M}^v \cup \mathcal{M}^h \), but \( T_K \) is SPD for \( K \in \mathcal{M}^{hv} \) for the second construction only. From (16), it is clear that \( T_K \) is symmetric positive but not definite for the first construction for \( K \in \mathcal{M}^{hv} \).
Remark 1.4 In the special case for which a given cell \( K \in \mathcal{M}^{hv} \) satisfies the superadmissibility property \( \sigma \perp x_K \mathbf{x}_{\sigma} \) for all \( \sigma \in \mathcal{F}_K \), and say for \( \mathbf{A} \) isotropic and cellwise constant, the HFV discretization transmissibility matrix \( T^h_K \) is diagonal leading to two point fluxes \( F_{K,\sigma} \) (see Lemma 2.1 of [16]). From (16), it can be checked that this two point flux property is preserved by the first construction for all faces \( \sigma \in \mathcal{F}_K \cap \mathcal{F}^h \) while it is not a priori the case for the second construction. This is one of the major advantage of the first approach when coupling the VAG and TPFA discretizations.

1.3 Mathematical analysis in the gradient discretization framework

1.3.1 Gradient discretization framework

Let us recall the coercivity, consistency, and limit conformity properties for sequences of gradient discretizations introduced in [15, 12, 10].

Coercivity: Let \( C_D > 0 \) be defined by

\[
C_D = \max_{v_D \in X^0_D \setminus \{0\}} \frac{||\Pi_D v_D||_{L^2(\Omega)}}{||v_D||_D}. 
\] (17)

Then, a sequence of gradient discretizations \( (D^l)_{l \in \mathbb{N}} \) is said to be coercive if there exist \( C_P > 0 \) such that \( C_D^l \leq C_P \) for all \( l \in \mathbb{N} \).

Consistency: For all \( u \in H_0^1(\Omega) \) and \( v_D \in X^0_D \) let us define

\[
S_D(u, v_D) = ||\nabla_D v_D - \nabla u||_{L^2(\Omega)} + ||\Pi_D v_D - u||_{L^2(\Omega)} 
\] (18)

and

\[
S_D(u) = \min_{v_D \in X^0_D \setminus \{0\}} S_D(u, v_D). 
\] (19)

Then, a sequence of gradient discretizations \( (D^l)_{l \in \mathbb{N}} \) is said to be consistent if for all \( u \in H_0^1(\Omega) \) one has \( \lim_{l \to +\infty} S_{D^l}(u) = 0 \).

Limit Conformity: For all \( q \in H_{\text{div}}(\Omega) \) and \( v_D \in X^0_D \), let us define

\[
W_D(q, v_D) = \int_{\Omega} ((\Pi_D v_D) \text{div} q + \nabla_D v_D \cdot q) dx, 
\] (20)

and

\[
W_D(q) = \max_{v_D \in X^0_D \setminus \{0\}} \frac{|W_D(q, v_D)|}{||v_D||_D}. 
\] (21)
Then, a sequence of gradient discretizations \((D_l)_{l \in \mathbb{N}}\) is said to be limit conforming if for all \(q \in H_{\text{div}}(\Omega)\) one has \(\lim_{l \to +\infty} W_D(q) = 0\).

The following proposition is proved in [15, 12, 10].

**Proposition 1.1** Let \(D = \left(X_0^D, \nabla_D, \Pi_D\right)\) be a gradient discretization such that \(\|\cdot\|_D\) is a norm on \(X_0^D\), then the gradient scheme (4) has a unique solution \(u_D \in X_0^D\) which satisfies the a priori estimate

\[
\|u_D\|_D \leq \frac{C_D}{k} \|f\|_{L^2(\Omega)}.
\]

Let \(u \in H_0^1(\Omega)\) be the solution of (2) and let us set \(q = -\Lambda \nabla u \in H_{\text{div}}(\Omega)\). Then, one has the following error estimates:

\[
\begin{align*}
\|\nabla u - \nabla_D u_D\|_{L^2(\Omega)} &\leq (k^2 + k^2) S_D(u) + \frac{1}{k} W_D(q), \\
\|\Pi_D u_D - u\|_{L^2(\Omega)} &\leq \frac{1}{k} \left((C_D + k^2) S_D(u) + C_D W_D(q)\right).
\end{align*}
\]

### 1.3.2 Proof of the coercivity, consistency and limit conformity properties for both constructions

**Proposition 1.2** Let us consider the gradient discretization \(D = \left(X_0^D, \nabla_D, \Pi_D\right)\) defined by (7), (8), (9) with the gradient reconstructions given either by (10)-(11)-(12) or by (10)-(11)-(13). Then, there exists \(C_D\) depending only on \(\theta_T\) such that

\[
\|\Pi_D v_D\|_{L^2(\Omega)} \leq C_D \|v_D\|_D, \text{ for all } v_D \in X_0^D,
\]

and the following consistency estimate

\[
S_D(\varphi) \leq C_{\varphi} h_T, \text{ for all } \varphi \in C^2(\overline{\Omega}) \cap H_0^1(\Omega),
\]

holds with \(C_{\varphi}\) depending only on \(\theta_T\) and \(\varphi\). Furthermore, the following limit conformity estimate

\[
W_D(\varphi) \leq C_{\varphi} h_T, \text{ for all } \varphi \in (C^1(\overline{\Omega}))^d,
\]

holds with \(C_{\varphi}\) depending only on \(\theta_T\) and \(\varphi\).

**Proof for the first gradient reconstruction**: the consistency estimate (23) is a classical result already established in the case of the VAG discretization (see [7] Lemmas 3.7 and 3.4) and of the HFV discretization (see
Lemma 4.3). The extension to our case results from the exactness of the cell gradients on affine functions as well as from the definition of $\theta_T$ (3). Let us now prove the coercivity (22). Let us set for all $u_D \in X_D$, $\Pi_M u_D(x) = u_K$ for all $x \in K$ and $K \in \mathcal{M}$. It results from the discrete Sobolev embeddings proved in [16] Lemma 5.3, that there exists $C_1$ depending only on $\theta_T$ such that for all $u_D \in X_D^0$

$$\|\Pi_M u_D\|_{L^2(\Omega)}^2 \leq C_1 \sum_{K \in \mathcal{M}} \sum_{\sigma \in \mathcal{F}_K} \frac{\sigma}{d_{K,\sigma}} (u_\sigma - u_K)^2,$$

(25)

with $u_\sigma = \sum_{s \in V_{\sigma}} \beta_{\sigma,s} u_s$ for all $\sigma \in \mathcal{F} \setminus \mathcal{F}^h$ and $d_{K,\sigma} = n_{K,\sigma} \cdot (x_\sigma - x_K)$. For all $K \in \mathcal{M}^v$, it results from the convex combination assumption on the weights $\beta_{\sigma,s}$, $s \in V_\sigma$, the definition of $\theta_T$ (3), and from Lemma 3.2 of [7] that there exists $C_2$ depending only on $\theta_T$ such that

$$\sum_{\sigma \in \mathcal{F}_K} |\sigma| d_{K,\sigma} (u_\sigma - u_K)^2 \leq C_2 \|\nabla^v K u_D\|_{L^2(K)^d}^2.$$

(26)

For all $K \in \mathcal{M}^h \cup \mathcal{M}^{hv}$, it also results from the definition of $\theta_T$ (3), and from Lemma 4.1 of [16] that there exists $C_3$ depending only on $\theta_T$ such that

$$\sum_{\sigma \in \mathcal{F}_K} |\sigma| d_{K,\sigma} (u_\sigma - u_K)^2 \leq C_3 \|\nabla D u_D\|_{L^2(K)^d}^2.$$

(27)

Combining (25)-(26)-(27), it results that the coercivity holds for the cellwise constant reconstruction in the sense that there exists $C_4$ depending only on $\theta_T$ such that for all $u_D \in X_D^0$

$$\|\Pi_M u_D\|_{L^2(\Omega)} \leq C_4 \|\nabla D u_D\|_{L^2(\Omega)^d}.$$

(28)

To conclude the proof of the coercivity property, let us now prove that there exists $C_5$ depending only on $\theta_T$ such that for all $u_D \in X_D$

$$\|\Pi_M u_D - \Pi_D u_D\|_{L^2(\Omega)} \leq C_5 h_T \|\nabla D u_D\|_{L^2(\Omega)^d}.$$

(29)

It results from (27) and Lemma 3.4 of [7] that there exists a constant $C_6$ depending only on $\theta_T$ such that for all $u_D \in X_D$ and for all $K \in \mathcal{M}^v \cup \mathcal{M}^h$, one has

$$\|\Pi_M u_D - \Pi_D u_D\|_{L^2(K)}^2 \leq C_6 (h_K)^2 \|\nabla D u_D\|_{L^2(K)^d}^2,$$

(30)

where $h_K$ is the diameter of the cell $K$. On the interface cells $K \in \mathcal{M}^{hv}$, from (27), there exists a constant $C_7$ depending only on $\theta_T$ such that for all $u_D \in X_D$

$$\sum_{\sigma \in \mathcal{F}_K \setminus \mathcal{F}^{hv}} |K| |u_\sigma - u_K|^2 \leq C_7 (h_K)^2 \|\nabla^{hv} K u_D\|_{L^2(K)^d}^2.$$

(31)
For all $\sigma \in \mathcal{F}^h$, $\mathcal{M}_\sigma = \{K, L\}$, $K \in \mathcal{M}^h$, using that $L \in \mathcal{M}^v$ and Lemma 3.2 of [7], there exists a constant $C_8$ depending only on $\theta_T$ such that for all $u_D \in X_D$

$$
\sum_{s \in V_s} |K| |u_s - u_L|^2 \leq C_8 (h_L)^2 \|\nabla^v L u_D\|_{(L^2(L))^d}^2.
$$

It results that, for $\sigma \in \mathcal{F}^h$, $\mathcal{M}_\sigma = \{K, L\}$, $K \in \mathcal{M}^h$, there exists a constant $C_9$ depending only on $\theta_T$ such that for all $u_D \in X_D$

$$
\sum_{s \in V_s} |K| |u_s - u_K|^2 \leq C_9 \left( (h_L)^2 \|\nabla^v L u_D\|_{(L^2(L))^d}^2 + (h_K)^2 \|\nabla^h L u_D\|_{(L^2(K))^d}^2 \right).
$$

It is clear from (32) that the control of the contribution of the node $s \in V_s$ to $\|\Pi_M u_D - \Pi_D u_D\|_{L^2(K)}^2$ is obtained thanks to the neighboring VAG cell $L$.

Gathering (30)-(31)-(32) concludes the proof of (29) and hence of the coercivity (22).

Let us first prove the limit conformity estimate (24) for the gradient discretization $\left( X_D^0, \nabla_D, \Pi_D \right)$ using the function reconstruction $\Pi_D$ defined by $\Pi_D u_D(x) = \Pi_T u_D(x)$ for all $x \in K$, $K \in \mathcal{M}^v$ and $\Pi_D u_D(x) = \Pi_M u_D(x)$ for all $x \in K$, $K \in \mathcal{M}^h \cup \mathcal{M}^h$. Using that $\nabla^v L u_D = \nabla^h L u_D = \Pi_M u_D$ for all $K \in \mathcal{M}^v$, one has

$$
T^v = \sum_{K \in \mathcal{M}^v} \int_K \left( (\Pi_D u_D) \text{div} \varphi + \nabla_D u_D \cdot \varphi \right) dx
= \sum_{\sigma \in \mathcal{F}^h, \mathcal{M}_\sigma = \{K, L\}, K \in \mathcal{M}^v} \int_\sigma (\Pi_T u_D) \varphi \cdot n_K d\sigma(x).
$$

Let us set $u_s = \sum_{s \in V_s} \beta_{s, s} u_s$ for all $\sigma \in \mathcal{F} \setminus \mathcal{F}^h$ and $\varphi_s = \frac{1}{|\sigma|} \int_\sigma \varphi(x) d\sigma(x)$, $\varphi_K = \frac{1}{|K|} \int_K \varphi(x) dx$. We define

$$
T^h = \sum_{K \in \cup \mathcal{M}^h \cup \mathcal{M}^h} \int_K \left( (\Pi_D u_D) \text{div} \varphi + \nabla_D u_D \cdot \varphi \right) dx = T^h_1 + T^h_{21} + T^h_{22},
$$

with

$$
T^h_1 = \sum_{K \in \cup \mathcal{M}^h \cup \mathcal{M}^h} \int_K (\Pi_D u_D) \text{div} \varphi dx = \sum_{K \in \cup \mathcal{M}^h \cup \mathcal{M}^h} \sum_{\sigma \in \mathcal{F}_K} |\sigma| u_K \varphi_{\sigma} \cdot n_{K, \sigma},
$$

$$
T^h_{21} = \sum_{K \in \cup \mathcal{M}^h \cup \mathcal{M}^h} \sum_{\sigma \in \mathcal{F}_K} |\sigma| (u_s - u_K) \varphi_K \cdot n_{K, \sigma},
$$

$$
T^h_{22} = \sum_{K \in \cup \mathcal{M}^h \cup \mathcal{M}^h} \sum_{\sigma \in \mathcal{F}_K} \frac{1}{\sqrt{d}} |\sigma| R_{K, \sigma}(u_D) n_{K, \sigma} \cdot \frac{1}{|K|} \int_{K, \sigma} \varphi(x) dx.
$$
Since $\sum_{\sigma \in F_K} |\sigma| R_{K,\sigma}(u_D) n_{K,\sigma} = 0$, one has

$$T_{22}^h = \sum_{K \in M^h \cup M^{hv}} \sum_{\sigma \in F_K} \frac{1}{|K|} |\sigma| R_{K,\sigma}(u_D) n_{K,\sigma} \cdot \frac{1}{|K|} \int_{K,\sigma} (\varphi(x) - \varphi_K) d\mathbf{x},$$

and, from [16], it exists $C$ depending only on $\theta_T$ and $\varphi$ such that

$$|T_{22}^h| \leq C h_T \left( \sum_{K \in M^h \cup M^{hv}} \|\nabla_D u_D\|_{L^2(K)}^2 \right)^{\frac{1}{2}}.$$

Since

$$\sum_{K \in M^h \cup M^{hv}} \sum_{\sigma \in F_K} |\sigma| u_\sigma \varphi_\sigma \cdot n_{K,\sigma} = \sum_{\sigma \in F^{hv}} |\sigma| u_\sigma \varphi_\sigma \cdot n_{K,\sigma},$$

one has

$$T_1^h = \sum_{K \in M^h \cup M^{hv}} \sum_{\sigma \in F_K} |\sigma| (u_K - u_\sigma) \varphi_\sigma \cdot n_{K,\sigma} + \sum_{\sigma \in F^{hv}} |\sigma| u_\sigma \varphi_\sigma \cdot n_{K,\sigma}.$$

Combining the previous identities and using that $|\sigma| u_\sigma = \int_{\sigma} \Pi_T u_D(x) d\sigma(x)$ for all $\sigma \in F^{hv}$, we obtain that

$$T^h + T_1^h + T_{21}^h = T^{hv} + T_3^h,$$

with

$$T_3^h = \sum_{K \in M^h \cup M^{hv}} \sum_{\sigma \in F_K} |\sigma| (u_\sigma - u_K) (\varphi_K - \varphi_\sigma) \cdot n_{K,\sigma},$$

$$T^{hv} = \sum_{\sigma \in F^{hv}} \int_{\sigma} (\Pi_T u_D(x) - u_\sigma) (\varphi(x) - \varphi_\sigma) \cdot n_{K,\sigma} d\sigma(x).$$

We deduce that there exists $C$ depending only on $\theta_T$ and $\varphi$ such that

$$|T_3^h| \leq C h_T \left( \sum_{K \in M^h \cup M^{hv}} \|\nabla_D u_D\|_{L^2(K)}^2 \right)^{\frac{1}{2}}.$$

Since for $\sigma \in F^{hv}$ with $\mathcal{M}_\sigma = \{K, L\}$, $K \in \mathcal{M}^v$, there exists a constant $C$ depending only on $\theta_T$ such that

$$\|\Pi_T u_D(x) - u_\sigma\|_{L^2(\sigma)} \leq C h_K^{\frac{1}{2}} \|\nabla_{Kv} u_D\|_{(L^2(K))},$$

18
we deduce that there exists a constant $C$ depending only on $\theta_T$ and $\varphi$ such that whatever the subset $\mathcal{M}^v$ of VAG cells one has the estimate

$$|T_t h^v| \leq C h_T \left( \sum_{\sigma \in F_h^v} \|\nabla^v u_D\|_{L^2(K_c)^d}^2 \right)^{\frac{1}{2}}.$$

Note that a better estimate of order $h^3 T^2$ is obtained for $|T_t h^v|$ if the subset of VAG cells is such that the surface of the interface $\sum_{\sigma \in F_h^v} |\sigma|$ remains bounded independently of the mesh.

This concludes the proof of the limit conformity estimate (24) for the gradient discretization $(X^0_D, \nabla_D, \Pi_D)$. The extension of this estimate to $D = (X^0_D, \nabla_D, \Pi_D)$ results from the estimate

$$\|\Pi_D u_D - \Pi_D u_D\|_{L^2(\Omega)} \leq C h_T \|u_D\|_D,$$

for all $u_D \in X^0_D$ which is obtained in a similar way than the estimate (29) on $\|\Pi_M u_D - \Pi_D u_D\|_{L^2(\Omega)}$ established in the above proof of the coercivity.

**Proof for the second gradient reconstruction**: as stated in remark 1.1, the second gradient reconstruction (13) can be used in combination with $X^0_D$ and $\Pi_D$ as a standalone gradient discretization. The proof of the coercivity, consistency and limit conformity for this gradient discretization is similar to the one presented in Lemma 3.1 of [15] using that $\sum_{\nu \in \text{dof}_K} (x_\nu - x_K) b^T_{K,\nu} = I$ and that $\sum_{\nu \in \text{dof}_K} R_{K,\nu}(u_D) b_{K,\nu} = 0$. The limit conformity when combining this gradient discretization with the VAG gradient reconstruction (10) must be checked but this analysis is similar to the one performed above using that $|\sigma| u_\sigma = \int_\sigma (\Pi_T u_D) d\sigma(x)$ for all $\sigma \in F_h^v$.

**Proposition 1.3** Let $(D^l)_{l \in \mathbb{N}}$ be a sequence of gradient discretizations $D^l = (X^0_D, \nabla_D, \Pi_D)$ defined by (7), (8), (9) with the gradient reconstructions given either by (10)-(11)-(12) or by (10)-(11)-(13) and such that there exists $\theta$ with $\theta_{T^l} \leq \theta$ for all $l \in \mathbb{N}$ and such that $\lim_{l \to +\infty} h_{T^l} = 0$. Then, the sequence $(D^l)_{l \in \mathbb{N}}$ is coercive, consistent and limit conforming. Therefore the gradient scheme is convergent. Furthermore, it satisfies a first order error estimate on smooth solutions.

**Proof**: the coercivity of the sequence of gradient discretizations results from Proposition 1.2 and from the shape regularity assumption. The consistency of the sequence of gradient discretizations results from Proposition 1.2, from
\lim_{l \to +\infty} h_{\mathcal{T}^l} = 0 \text{ and from the density of } C^2(\Omega) \cap H_0^1(\Omega) \text{ in } H_0^1(\Omega). \text{ The limit conformity property of the sequence of gradient discretizations results from Proposition 1.2, the density of } (C^1(\Omega))^d \text{ in } H_{\text{div}}(\Omega) \text{ and from the coercivity property.}

1.4 Numerical tests for second order diffusion problems

In the following subsections, the VAG scheme on the full domain (vag), the HFV scheme on the full domain (hfv) and both combined VAG-HFV schemes using stabilisation (vag-hfv stab) or not (vag-hfv) are compared on various families of meshes. All test cases consider the exact solution

\[ u(x, y, z) = e^{\cos(x+y+z)}, \]

with Dirichlet boundary conditions at \( \partial \Omega \). If not specified differently, the diffusion tensor \( \Lambda \) is the identity matrix.

1.4.1 Hexahedral meshes

Let us consider the family of uniform Cartesian grids of the domain \( \Omega = (0, 1)^3 \) of size \( N \times N \times N \) with \( N = 8, 16, 32, 64 \). The family of hexahedral meshes is obtained by random perturbation of the Cartesian grids inside the subdomain \( \Omega^v = (0.25, 0.75)^3 \) as exhibited in Figure 2 for \( N = 8 \).

Figure 2: Hexahedral mesh obtained for \( N = 8 \) and composed of cubic cells in the HFV subdomain \( \Omega \setminus \Omega^v \) and of randomly perturbated cubic cells in the VAG subdomain \( \Omega^v = (0.25, 0.75)^3 \).
A convergence of order two is observed as expected in Figure 3 on the potential and of order one on the gradient for the VAG and both VAG-HFV schemes. This is not the case for the HFV scheme for which the gradient clearly does not converge due to the non-planar faces in the VAG region. The combined VAG-HFV schemes solve this issue by using the consistent VAG scheme in the non-planar face region. Both VAG-HFV schemes are remarkably more accurate than the VAG scheme on the potential. The VAG-HFV stabilised scheme is also more accurate than the VAG scheme on the gradient with both norms. The unstabilised version is doing slightly worse than the VAG scheme on the $L^\infty$ gradient norm.

1.4.2 Hybrid meshes with hexahedra and pyramids

Let us consider the family of uniform Cartesian grids of the domain $\Omega = (0, 1)^3$ of size $N \times N \times N$ with $N = 8, 16, 32, 64$. Then our family of hybrid meshes is obtained by cutting in 6 pyramids each cubic cell contained in the VAG subdomain $\Omega^v = (0.25, 0.75)^3$ as exhibited in Figure 4 for $N = 8$. 

Figure 3: Convergence in $L^2$ norm (left) and in $L^\infty$ norm (right) of the potential (above) and of the gradient (below) on the family of hexahedral meshes and for the VAG, HFV, VAG-HFV and the stabilised VAG-HFV schemes.
Figure 4: Hybrid mesh obtained for $N = 8$ and composed of cubes in the HFV subdomain $\Omega \setminus \Omega^v$ and of pyramids in the VAG subdomain $\Omega^v = (0.25, 0.75)^3$.

Figure 5: Convergence in $L^2$ norm (left) and in $L^\infty$ norm (right) of the potential (above) and of the gradient (below) on the family of hybrid meshes and for the VAG, HFV, VAG-HFV and the stabilised VAG-HFV schemes.

A convergence of order two is observed as expected in Figure 5 on the potential and of order one on the gradient for all schemes. The VAG scheme is more accurate than the HFV scheme on the gradient while it is the contrary on the potential. The convergence of both combined VAG-HFV schemes matches with the convergence of the HFV scheme on the potential and the
VAG-HFV schemes provide the best convergence of the gradient in $L^2$ norm. In $L^\infty$ norm the convergences of the gradient for the VAG-HFV schemes are rather in between the VAG and HFV convergences.

1.4.3 **Anisotropic test case**

We consider in this subsection the previous test case with the following homogeneous anisotropic diffusion tensor

$$\Lambda = \begin{pmatrix} 3 & -1 & -1 \\ -1 & 3 & -1 \\ -1 & -1 & 3 \end{pmatrix}.$$  

Figure 6: Convergence in $L^2$ norm (left) and in $L^\infty$ norm (right) of the potential (above) and of the gradient (below) on the family of hybrid meshes (hexahedral and pyramidal cells) with anisotropic permeability and for the VAG, HFV, VAG-HFV and the stabilised VAG-HFV schemes.

As exhibited in Figure 6, the order of convergence are again the expected ones for all schemes. The VAG scheme is more accurate than the HFV scheme on the gradient while it is the contrary on the potential. The convergences of both combined VAG-HFV schemes are roughly in between those of the VAG and HFV schemes.
1.4.4 Red black test case

Let us consider the family of uniform Cartesian grids of the domain $\Omega = (0,1)^3$ of size $N \times N \times N$ with $N = 8, 16, 32, 64$. The cells are ordered in red black fashion and the VAG cells (resp. the HFV cells) correspond to the red cells (resp. black cells) as exhibited in Figure 7. Note that all the HFV cells are interface cells for this test case i.e. $\mathcal{M}^b = \emptyset$.

Figure 7: Uniform Cartesian mesh for $N = 8$ with the VAG cells in red and the HFV cells in blue.

A super convergence of order two of the gradient is observed in Figure 8 for the VAG and HFV schemes on this family of uniform Cartesian meshes. This super convergence property is lost as expected for the combined VAG-HFV schemes for which the usual order one convergence of the gradient in $L^\infty$ norm is clearly recovered. We also remark that the HFV scheme provides a better accuracy than the VAG scheme for this family of meshes and consequently that the convergence of the potential for the combined VAG-HFV schemes is close to the one of the VAG scheme.
Figure 8: Convergence in $L^2$ norm (left) and in $L^\infty$ norm (right) of the potential (above) and of the gradient (below) on the family of Cartesian meshes and for the VAG, HFV, VAG-HFV and the stabilised VAG-HFV schemes.

2 Combined VAG-HFV discretization of two-phase Darcy flows

The extension of the VAG-HFV discretization to two-phase Darcy flows combines ideas presented in [18] for the VAG discretization of multi-phase Darcy flow models and in [3] for the HFV discretization of two-phase Darcy flows. It is based on the discrete fluxes $F_{K,\nu}$, $K \in \mathcal{M}$, $\nu \in \text{dof}_K$ defined in (14) and connecting each cell $K$ to its nodes $s \in \mathcal{V}_K \cap \mathcal{V}^v$ and faces $\sigma \in \mathcal{F}_K \cap \mathcal{F}^h$. Porous volumes are assigned as usual to all cells $K \in \mathcal{M}$ but also, following [18], to each node $s \in \mathcal{V}^v \setminus \mathcal{V}_D$ (excluding the Dirichlet nodes $\mathcal{V}_D$). Then, discrete conservation equations are derived for all $K \in \mathcal{M}$ and $s \in \mathcal{V}^v \setminus \mathcal{V}_D$ using the porous volumes, the discrete fluxes $F_{K,\nu}$ and an upwind approximation of the mobilities. The faces $\sigma \in \mathcal{F}^h$ are considered as interfaces on which, following [3], the flux continuity equations are written for each phase assuming the continuity of the phase mobility. This is a natural generalisation to the HFV discretization of the harmonic transmissibility formula which is classically considered for Two-Point Flux Approximations [4, 22].
2.1 Two-phase Darcy flow model

Let us consider the following two-phase Darcy flow model

\[
\begin{align*}
\phi(x) \partial_t S^\alpha + \text{div}(q^\alpha) &= 0, \quad \alpha \in \mathcal{P}, \\
\sum_{\alpha \in \mathcal{P}} S^\alpha &= 1,
\end{align*}
\]

where \(\phi(x)\) is the porous-medium porosity, \(\mathcal{P} = \{g, l\}\) denotes the set of the non-wetting phase (denoted by \(g\) to fix ideas) and the wetting phase (denoted by \(l\) to fix ideas) and \(S^\alpha, \alpha \in \mathcal{P}\) is the phase saturation. The flow rates \(q^\alpha\) are defined by the following generalized Darcy laws for \(\alpha \in \mathcal{P}\):

\[
q^\alpha = -\frac{k^\alpha(x, S^\alpha)}{\mu^\alpha} \Lambda(x) \left( \nabla P^\alpha - \rho^\alpha g \right),
\]

where \(\rho^\alpha\) is the phase mass density, \(\mu^\alpha\) is the phase dynamic viscosity, \(g\) is the gravitational acceleration, \(\Lambda(x)\) is the absolute permeability tensor, \(k^\alpha(x, S^\alpha)\) is the phase relative permeability and \(P^\alpha\) is the phase pressure. The model is closed by the following capillary pressure relation

\[
P^g - P^l = P_c(x, S^g),
\]

where \(P_c(x, S^g)\) is the capillary function.

Let us consider a partition \(\partial \Omega_D \cup \partial \Omega_N\) of the boundary \(\partial \Omega\). On \(\partial \Omega_D\), we consider a Dirichlet boundary condition with prescribed pressures \(P^\alpha\) and saturations \(S^\alpha\), \(\alpha \in \mathcal{P}\). On \(\partial \Omega_N\), homogeneous Neumann boundary conditions are imposed with \(q^\alpha \cdot n = 0\) for \(\alpha \in \mathcal{P}\).

2.2 Combined VAG-HFV discretization

The mesh is assumed to be conforming with the boundary condition in the sense that there exists a subset \(\mathcal{F}_D \subset \mathcal{F}_{\text{ext}}\) such that \(\bigcup_{\sigma \in \mathcal{F}_D} \overline{\sigma} = \overline{\partial \Omega_D}\). Let us define the set of Dirichlet boundary HFV faces by

\[
\mathcal{F}_D^h = \mathcal{F}_D \cap \mathcal{F}^h,
\]

and the set of Dirichlet boundary VAG nodes by

\[
\mathcal{V}_D^v = \mathcal{V}^v \cap (\bigcup_{\sigma \in \mathcal{F}_D} \mathcal{V}_\sigma).
\]
The Neumann boundary HFV faces are defined by
\[ \mathcal{F}_N^h = (\mathcal{F}_{ext} \setminus \mathcal{F}_D) \cap \mathcal{F}^h. \]

A rocktype \( r_t \) is assigned to each cell \( K \in \mathcal{M} \) and each rocktype \( r_t \) corresponds to given capillary and phase relative permeability functions denoted by \( P_{c,rt}(S^g) \) and \( k_{\alpha,rt}(S^\alpha) \). The porosity and absolute permeability tensor are also assumed cellwise constant and denoted by \( \phi_K \) and \( \Lambda_K \) for all \( K \in \mathcal{M} \).

Let us define the set of neighboring cells of a node \( s \) as \( \mathcal{M}_s = \{ K \in \mathcal{M} | s \in V_K \} \). For the VAG discretization, a single rocktype \( r_t \) is assigned to each node \( s \in V \cap V_D \). It is chosen as the most permeable rocktype among all rocktypes \( (r_K)_{K \in \mathcal{M}_s \cap \mathcal{M}_v} \). Then, the porous volume is distributed to the VAG nodes as follows: given a parameter \( \omega \in (0, 1) \), we set for all \( K \in \mathcal{M}_v, s \in V \cap V_K \)
\[ \alpha_{K,s} = \begin{cases} 0 & \text{if } r_t \neq r_t \text{ or } s \in V_D, \\ \frac{\#V_k \cap V_D}{\#\{s \in V_k \cap V_D | r_t = r_t \}} & \text{if } r_t = r_t \text{ and } s \notin V_D, \end{cases} \]
thus the porous volumes are
\[ \varphi_s = \sum_{K \in \mathcal{M}_s \cap \mathcal{M}_v} \alpha_{K,s} \phi_K | K |, \]
for \( s \in V \),
\[ \varphi_K = \left(1 - \sum_{s \in V_K} \alpha_{K,s}\right) \phi_K | K |, \]
for \( K \in \mathcal{M}_v \), and
\[ \varphi_K = \phi_K | K |, \]
for \( K \in \mathcal{M}_h \cup \mathcal{M}_hv \). Note that \( \omega \) is chosen small enough such that \( 1 - \sum_{s \in V_K} \alpha_{K,s} > 0 \) (see Figure 9). The complementary rock volume for \( \nu \in \mathcal{M} \cup (V \cap V_D^v) \) is denoted by \( \bar{\varphi}_\nu \). For HFV Dirichlet boundary faces \( \sigma \in \mathcal{F}_h \), let us also set \( r_t = r_t \) with \( \mathcal{M}_s = \{ K \} \).

The set of unknowns and dirichlet data, exhibited in Figure 10, is defined by
\[ U_D = \{(P^g, P^l, S^g, S^l), \nu \in \mathcal{M} \cup V \cup F_D^h \} \cup \{(P^g, P^l), \sigma \in \mathcal{F}_h \setminus \mathcal{F}_D^h \}, \]
and the subsets of phase pressure unknowns by
\[ P_D^g = \{P^g, \nu \in \mathcal{M} \cup V \cup \mathcal{F}_h \}. \]
Figure 9: Example of a 2D mesh with the distribution of the volumes $\alpha_{K,s}|K|$ at each node $s \in V_K$ of the cell $K \in M^e$ in the case of a single rock type.

Figure 10: 2D mesh with examples of discrete unknowns in the set $U_D$ for the two-phase flow model.

for $\alpha \in \mathcal{P}$.

Using the combined VAG-HFV discretization, let us define the discrete Darcy fluxes for all $K \in M$ and $\nu \in \text{dof}_K$ by

$$F_{K,\nu}^\alpha(P_D^\alpha) = F_{K,\nu}(P_D^\alpha) - \rho^\alpha F_{K,\nu}(G_D),$$

with $G_D \in X_D$ such that for all $\nu \in \text{dof}_D$, $G_\nu = x_\nu \cdot g$, where $g$ is the gravity acceleration. The discrete generalized Darcy fluxes for all $K \in M$
and $\nu \in \text{dof}_K$ are deduced using an upwind approximation of the mobilities as follows:

$$V_{K,\nu}^n(U_D) = \begin{cases} 
\frac{k_{\nu}(S^n_{K})}{\mu}(F^n_{K,\nu}(P^n_{D}))^+, & \text{if } \nu \in \mathcal{V}^u \cup \mathcal{F}^h, \\
\frac{k_{\nu}(S^n_{K})}{\mu}(F^n_{K,\nu}(P^n_{D}))^-, & \text{if } \nu \in \mathcal{F}^h \setminus (\mathcal{F}^h \cup \mathcal{F}_N), \mathcal{M}_\nu = \{K, L\}, \\
0 & \text{if } \nu \in \mathcal{F}^h_N.
\end{cases}$$

The time integration is based on a fully implicit Euler scheme to avoid severe restrictions on the time steps. For $N_{tf} \in \mathbb{N}^*$, let us consider the time discretization $t^0 = 0 < t^1 < \cdots < t^{n-1} < t^n \cdots < t^{N_{tf}} = t_f$ of the time interval $(0, t_f)$. We denote the time steps by $\Delta t^n = t^n - t^{n-1}$ for all $n = 1, \cdots, N_{tf}$. It leads to the following set of equations at each time step $n = 1, \cdots, N_{tf}$ accounting for the cell conservation equations

$$\varphi_K \frac{S^n_{K} - S^{n-1}_{K}}{\Delta t^n} + \sum_{\nu \in \text{dof}_K} V_{K,\nu}^n(U_D^n) = 0, \quad K \in \mathcal{M}, \quad \alpha \in \mathcal{P}, \quad (37)$$

the VAG node conservation equations

$$\varphi_s \frac{S^n_{s} - S^{n-1}_{s}}{\Delta t^n} - \sum_{K \in \mathcal{M}_s \setminus \mathcal{M}^h} V_{K,s}^n(U_D^n) = 0, \quad s \in \mathcal{V}^v \setminus \mathcal{V}_D^v, \quad \alpha \in \mathcal{P}, \quad (38)$$

coupled with the flux continuity equations or Neumann boundary condition at HFV faces

$$\sum_{K \in \mathcal{M}^s} F^n_{K,\sigma}(P^n_D) = 0, \quad \sigma \in \mathcal{F}^h \setminus \mathcal{F}_D^h, \quad \alpha \in \mathcal{P}, \quad (39)$$

the Dirichlet boundary conditions at Dirichlet nodes and faces

$$P^n_{\nu \nu} = P^n_{D,\nu}, \quad S^n_{\nu} = S^n_{D,\nu}, \quad \nu \in \mathcal{V}_D^u \cup \mathcal{F}_D^h, \quad \alpha \in \mathcal{P}, \quad (40)$$

and with the closure laws

$$S^n_{\nu} + S^n_{L} = 1, \quad P^n_{\nu} - P^n_{L} = P_{\text{ext},\nu}(S^n_{\nu}), \quad \nu \in \mathcal{M} \cup \mathcal{V} \setminus \mathcal{V}_D^v. \quad (41)$$

### 2.3 Numerical experiments on a one dimensional solution

This test case considers the domain $\Omega = (0, 1)^3$ with homogeneous isotropic permeability $\Lambda = 1$ and porosity $\phi = 1$. The gravitational acceleration $g$
is set to zero, the relative permeabilities to $k_\alpha^\nu(S^\alpha) = (S^\alpha)^2$, $\alpha = g, l$, the dynamic viscosities to $\mu^g = 5$ and $\mu^l = 1$, and the capillary pressure to $P_c(S^g) = -0.1 \log(1 - S^g)$. Dirichlet boundary conditions are set at $x = 0$ with imposed non-wetting phase pressure $P^g = 2$ and saturation $S^g = 0.9$, as well as at $x = 1$ with $P^l = 0$ and $S^g = 0$. Homogeneous Neumann conditions are considered at the remaining boundaries. The saturation is set to $S^g = 0$ at initial time $t = 0$ and the final simulation time is fixed to $t_f = 1$.

In the following subsections, the VAG scheme on the full domain (vag), the HFV scheme on the full domain (hfv) and both combined VAG-HFV schemes using stabilisation (vag-hfv stab) or not (vag-hfv) are compared on three families of meshes. The error is computed both for the saturation and for the non-wetting phase pressure based on a numerical reference solution obtained on a one dimensional uniform grid with 1000 cells and time steps. A space time discrete $L^1$ norm computed from all cell and time step values is used for simplicity.

For all test cases, a uniform time stepping is used with 200 time steps on $(0, t_f)$. The system of equations (37)-(38)-(39)-(40) is solved at each time step by using a Newton-Raphson algorithm w.r.t. the set of primary unknowns

$$U_P^D = \{(P^g_\nu, S^g_\nu), \nu \in \mathcal{M} \cup \mathcal{V}^{n-1} \setminus \mathcal{V}_D^D\} \cup \{(P^g_\sigma, P^l_\sigma), \sigma \in \mathcal{F}^{h} \setminus \mathcal{F}_D^h\},$$

(42)

taking into account the elimination of the Dirichlet boundary conditions (40) and of the secondary unknowns $\{(P^l_\nu, S^l_\nu), \nu \in \mathcal{M} \cup \mathcal{V}^{n-1} \setminus \mathcal{V}_D^D\}$ together with the closure laws (41).

The Jacobian matrix is computed analytically, then the VAG cell primary unknowns and conservation equations for $K \in \mathcal{M}^n$ are eliminated without any fill-in by Schur complement. As mentioned in Remark 1.4, in the case of superadmissibility of the cells $K \in \mathcal{M}^h \cup \mathcal{M}^{hv}$ such as for Cartesian cells with isotropic permeability tensor, the HFV scheme reduces to a TPFA scheme and the face unknowns $\{(P^g_\sigma, P^l_\sigma), \sigma \in \mathcal{F}^{h} \setminus \mathcal{F}_D^h\}$ are eliminated from the flux continuity equations (39). When using the stabilised version of the combined VAG-HFV scheme, note that the TPFA fluxes are not preserved at the faces of the interface cells. Consequently these face unknowns will not be eliminated for the stabilised VAG-HFV scheme. The reduced linear systems obtained at each Newton iteration are solved using the GMRes iterative solver combined with a CPR-AMG preconditioner [20, 24].

The numerical behavior of the four schemes is reported for the three families of meshes on the finest mesh with $N_{red}$ the number of degree of
freedom of the reduced linear systems with two primary unknowns per d.o.f., $NZ_{red}$ the number of non-zero 2 by 2 entries in the reduced linear systems, $N_{newton}$ the average number of Newton iterations per time step and $N_{gmres}$ the average number of GMRes iterations per Newton step. The CPU times are in seconds on 3.1 Ghz Intel Core i7 processor and 16Go RAM.

2.3.1 Hexahedral meshes

Let us consider the family of uniform Cartesian grids of the domain $\Omega = (0,1)^3$ of size $N \times N \times N$ with $N = 4, 8, 16, 32$. The family of hexahedral meshes is obtained by random perturbation of the Cartesian grids inside the VAG subdomain $\Omega_v = (0.25, 0.75)^3$ as exhibited in Figure 2 for $N = 8$.

Figure 11 exhibits, for the four schemes, the convergence of the error. All schemes exhibit the same order of convergence both for the saturation (lower but close to 1) and for the pressure (roughly 1). The VAG scheme is more accurate on this type of mesh since it uses more d.o.f. than the HFV scheme for the transport of the saturation accounting for the leading error term due to the first order upwind discretization of the mobilities. The combined VAG-HFV schemes both exhibit roughly the same convergence as the HFV scheme since the HFV domain is much larger than the VAG domain in this test case.

Table 1 exhibits the numerical behavior of the four schemes on the finest mesh $N = 32$ with 4096 hexahedra in the VAG subdomain and 28672 cubes in the HFV subdomain. All schemes have roughly the same number of Newton iterations and hence their numerical behavior differs by the sparsity of the
reduced linear systems and efficiency of the CPR-AMG preconditioner. The HFV scheme reduces to a TPFA scheme in the HFV region representing most of the domain which explains the better CPU time observed with the HFV scheme compared with the VAG scheme in this test case. The VAG-HFV scheme without stabilisation leads to the sparsest reduced system and to the lowest CPU time. The stabilisation increases the number of non-zero elements of the reduced linear systems since the face unknowns located at the interface cells are not eliminated. The CPR-AMG preconditioner is also less efficient leading to a CPU time that is twice larger than the unstabilised VAG-HFV scheme.

<table>
<thead>
<tr>
<th>Scheme</th>
<th>( N_{\text{red}} )</th>
<th>( N_{Z_{\text{red}}} )</th>
<th>( N_{\text{newton}} )</th>
<th>( N_{\text{gmres}} )</th>
<th>CPU(s)</th>
</tr>
</thead>
<tbody>
<tr>
<td>hfv</td>
<td>45824</td>
<td>411392</td>
<td>3.06</td>
<td>7.4</td>
<td>670</td>
</tr>
<tr>
<td>vag</td>
<td>35937</td>
<td>877215</td>
<td>3.05</td>
<td>7.4</td>
<td>1060</td>
</tr>
<tr>
<td>vag-hfv</td>
<td>33585</td>
<td>322961</td>
<td>3.0</td>
<td>6.9</td>
<td>553</td>
</tr>
<tr>
<td>vag-hfv stab</td>
<td>38385</td>
<td>427985</td>
<td>3.06</td>
<td>9.3</td>
<td>1048</td>
</tr>
</tbody>
</table>

Table 1: Numerical behavior of the VAG, HFV and VAG-HFV schemes for the two-phase Darcy flow on the finest Hexahedral mesh obtained for \( N = 32 \).

2.3.2 Hybrid meshes with hexahedral and pyramids

Let us consider the family of uniform Cartesian grids of the domain \( \Omega = (0,1)^3 \) of size \( N \times N \times N \) with \( N = 8, 16, 32 \). Then our family of hybrid meshes is obtained by cutting in 6 pyramids each cubic cell contained in the VAG subdomain \( \Omega^v = (0.5,1) \times (0,1)^2 \) as exhibited in Figure 12 for \( N = 8 \).

![Figure 12: Hybrid mesh obtained for \( N = 8 \) and composed of cubes in the HFV subdomain \( \Omega \setminus \Omega^v \) and of pyramids in the VAG subdomain \( \Omega^v = (0.5,1) \times (0,1)^2 \).](image)

As exhibited in Figure 13, the convergence of the error behaves like in the previous test case.
Figure 13: Convergence in space time discrete $L^1$ norm of the saturation and the non-wetting pressure on the family of hybrid meshes and for the VAG, HFV, VAG-HFV and the stabilised VAG-HFV schemes.

The following Table 2 exhibits the numerical behavior of the four schemes on the finest mesh $N = 32$ with 16384 cubes in the HFV subdomain and 98304 pyramids in the VAG subdomain. The HFV scheme is roughly four times more costly than the three other schemes due the much larger number of faces in the VAG region compared with the number of nodes.

<table>
<thead>
<tr>
<th>Scheme</th>
<th>$N_{red}$</th>
<th>$NZ_{red}$</th>
<th>$N_{newton}$</th>
<th>$N_{gmres}$</th>
<th>CPU(s)</th>
</tr>
</thead>
<tbody>
<tr>
<td>hfv</td>
<td>361472</td>
<td>5447552</td>
<td>3.02</td>
<td>15.0</td>
<td>6260</td>
</tr>
<tr>
<td>vag</td>
<td>52321</td>
<td>1024671</td>
<td>3.04</td>
<td>7.5</td>
<td>1507</td>
</tr>
<tr>
<td>vag-hfv</td>
<td>51281</td>
<td>709552</td>
<td>3.05</td>
<td>7.3</td>
<td>1525</td>
</tr>
<tr>
<td>vag-hfv stab</td>
<td>54417</td>
<td>778480</td>
<td>3.03</td>
<td>9.5</td>
<td>1360</td>
</tr>
</tbody>
</table>

Table 2: Numerical behavior of the VAG, HFV and VAG-HFV schemes for the two-phase Darcy flow on the finest hybrid mesh obtained for $N = 32$.

2.3.3 Red black test case

Let us consider the family of uniform Cartesian grids of the domain $\Omega = (0, 1)^3$ of size $N \times N \times N$ with $N = 4, 8, 16, 32$. The cells are ordered in red black fashion and the VAG cells (resp. the HFV cells) correspond to the red cells (resp. black cells) as exhibited in Figure 7.

The VAG and VAG-HFV schemes have roughly the same structure in the sense that the face unknowns are only located at the boundary for the VAG-HFV schemes. Note however, as can be noticed in Table 3, that the HFV cells are not eliminated for the VAG-HFV schemes while they are eliminated for the VAG scheme. Let us also remark that the HFV scheme reduces here
to a TPFA scheme on the full domain. From Figure 14, we can check as expected that the convergence of the errors for the VAG and for both VAG-HFV schemes are very close while the HFV scheme is less accurate due to its twice lower number of unknowns used for the transport of the saturation. As for the previous test cases, the orders of convergence are the same for all schemes.

![Figure 14: Convergence in space time discrete $L^1$ norm of the saturation and the non-wetting pressure on the family of Cartesian meshes with red black coloring and for the VAG, HFV, VAG-HFV and the stabilised VAG-HFV schemes.](image)

Table 3 exhibits the numerical behavior of the four schemes on the finest mesh $N = 32$ with 16384 cubes both in the VAG and HFV regions. The HFV scheme is much cheaper since it reduces to a TPFA scheme on the full domain, while the three other schemes are rather close in CPU time with a significantly larger cost for the stabilised version of the VAG-HFV scheme.

<table>
<thead>
<tr>
<th>Scheme</th>
<th>$N_{red}$</th>
<th>$N_{Z_{red}}$</th>
<th>$N_{newton}$</th>
<th>$N_{gmres}$</th>
<th>CPU(s)</th>
</tr>
</thead>
<tbody>
<tr>
<td>hfv</td>
<td>32768</td>
<td>223232</td>
<td>2.92</td>
<td>5.3</td>
<td>398</td>
</tr>
<tr>
<td>vag</td>
<td>35937</td>
<td>877215</td>
<td>3.04</td>
<td>7.2</td>
<td>1020</td>
</tr>
<tr>
<td>vag-hfv</td>
<td>52317</td>
<td>1151623</td>
<td>3.06</td>
<td>6.4</td>
<td>927</td>
</tr>
<tr>
<td>vag-hfv stab</td>
<td>55389</td>
<td>1196415</td>
<td>3.06</td>
<td>7.0</td>
<td>1249</td>
</tr>
</tbody>
</table>

Table 3: Numerical behavior of the VAG, HFV and VAG-HFV schemes for the two-phase Darcy flow on the finest Cartesian mesh obtained for $N = 32$. 

34
3 Combined VAG-HFV discretization of non-isothermal compositional two-phase Darcy flows

We consider in this section the extension of the previous combined VAG-HFV discretization to the case of a non-isothermal compositional two-phase Darcy flow. This extension is based on the formulation of the model introduced in [5]. Its main advantages compared with the related Coats’ variable switch formulation [9] is to be based on a fixed set of unknowns using extended phase molar fractions and to express the thermodynamical equilibrium as complementary constraints for both phases \( \alpha \in \mathcal{P} \). Previous works have considered the VAG discretization of isothermal and of non-isothermal compositional two-phase Darcy flows in respectively [18] and [26]. The HFV discretization of isothermal two component two-phase Darcy flows is also derived in [3] and the related Mixed-Hybrid Finite Element discretization of three-phase Darcy flows in [2]. Our extension to the combined VAG-HFV discretization follows the methodology presented in the previous section for immiscible isothermal two-phase flows which takes advantage of the cell based definition of the fluxes shared by the VAG, the HFV and by the modified scheme at interface cells.

3.1 Non-isothermal compositional two-phase Darcy flow model

Let us consider a non-isothermal compositional liquid gas Darcy flow model where each phase \( \alpha \in \mathcal{P} \) is a mixture of an arbitrary number of components with typically the water component (denoted by \( w \)) which can vaporize in the gas phase and the air component (denoted by \( a \)) which can dissolve in the liquid phase. The set of components is denoted by \( \mathcal{C} \). The thermodynamic properties of each phase \( \alpha \in \mathcal{P} \) depend on its pressure \( P^\alpha \), the local equilibrium temperature of the system \( T \) and its molar fractions \( C^\alpha = (C^\alpha_i)_{i \in \mathcal{C}} \).

Our formulation of the model is based on the fixed set of unknowns defined by

\[
U = (P^g, P^l, T, S^g, S^l, C^g, C^l).
\]

Let us introduce the notations for the thermodynamic laws. The molar density is denoted by \( \zeta^\alpha(P^\alpha, T, C^\alpha) \) and the dynamic viscosity by \( \mu^\alpha(P^\alpha, T, C^\alpha) \) for each phase \( \alpha \in \mathcal{P} \). The mass density is defined by \( \rho^\alpha(P^\alpha, T, C^\alpha) = \sum_{i \in \mathcal{C}} C^\alpha_i m_i \zeta^\alpha \) where \( m_i \) is the molar mass of the component \( i \in \mathcal{C} \). Let us
denote by $e^{\alpha}(P^{\alpha}, T, C^{\alpha})$ the molar internal energy, by $h^{\alpha}(P^{\alpha}, T, C^{\alpha})$ the molar enthalpy of the phase $\alpha \in \mathcal{P}$, and by $E_r(T)$ the rock energy per unit rock volume. For shorter notations, let us introduce the fluid energy per unit pore volume defined by

$$E_f(U) = \sum_{\alpha \in \mathcal{P}} \zeta^\alpha S^\alpha e^\alpha,$$

and the number of moles of the component $i \in \mathcal{C}$ per unit pore volume denoted by

$$n_i(U) = \sum_{\alpha \in \mathcal{P}} \zeta^\alpha S^\alpha C^\alpha_i, \quad i \in \mathcal{C}.$$

In order to simplify the notations, each thermodynamic law can also be written in the following as a function of the full set of variables $U$ still keeping the same notation for the function.

Thermodynamic equilibrium between the gas and liquid phases is assumed for each component and governed by the phase fugacities denoted by

$$f^{\alpha}(P^{\alpha}, T, C^{\alpha}) = (f^\alpha_i(P^{\alpha}, T, C^{\alpha}))_{i \in \mathcal{C}}, \quad \alpha \in \mathcal{P}.$$

Note that, as opposed to the Coats’ variable switch formulation \cite{9, 8}, the molar fractions $C^{\alpha}$ of an absent phase $\alpha$ are extended by the ones at equilibrium with the present phase in the sense that the equality of the gas and liquid fugacities $f^g(P^g, T, C^g) = f^l(P^l, T, C^l)$ always holds. This allows to fix the set of unknowns independently of the present phases.

The total molar flow rate $q_i$ of the component $i \in \mathcal{C}$ and the energy flow rate $q_e$ are obtained from the generalized Darcy velocities introduced in (34) such that

$$\begin{cases}
q_i = \sum_{\alpha \in \mathcal{P}} C^\alpha_i \zeta^\alpha q^\alpha, \\
q_e = \sum_{\alpha \in \mathcal{P}} h^\alpha \zeta^\alpha q^\alpha - \lambda \nabla T,
\end{cases} \quad (43)$$

where $\lambda$ stands for the bulk thermal conductivity of the fluid and rock mixture. The molar diffusion is neglected for the sake of simplicity.

Let us write the system of equations accounting for the molar conservation of each component $i \in \mathcal{C}$ together with the energy conservation

$$\begin{cases}
\phi(x) \partial_t n_i + \text{div}(q_i) = 0, \quad i \in \mathcal{C}, \\
\phi(x) \partial_t E_f + (1 - \phi(x)) \partial_t E_r + \text{div}(q_e) = 0.
\end{cases} \quad (44)$$
It is complemented by the capillary relation between the two phase pressures and the pore volume balance

\[
\begin{align*}
P_c(x, S^g) &= P^g - P^l, \\
\sum_{\alpha \in \mathcal{P}} S^\alpha &= 1.
\end{align*}
\]

In the spirit of \[21\], the liquid gas thermodynamic equilibrium can be expressed as the following complementary constraints for each phase \(\alpha \in \mathcal{P}\) combined with the equality of the gas and liquid fugacities of each component

\[
\begin{align*}
\min(S^\alpha, 1 - \sum_{i \in \mathcal{C}} C_1^\alpha) &= 0, \quad \alpha \in \mathcal{P}, \\
f_0^\alpha(P^g, T, C^g) &= f_1^\alpha(P^l, T, C^l), \quad i \in \mathcal{C}.
\end{align*}
\]

To fix ideas, let us consider a Dirichlet boundary condition on \(\partial \Omega_D\) with prescribed phase pressures \(P^\alpha\), molar fractions \(C^\alpha\), saturation \(S^\alpha\), \(\alpha \in \mathcal{P}\) and temperature \(T\). On \(\partial \Omega_N\), homogeneous Neumann boundary conditions are imposed with \(q^\alpha \cdot n = 0\) for \(\alpha \in \mathcal{P}\) and \(q_e \cdot n = 0\).

### 3.2 Combined VAG-HFV discretization of non-isothermal compositional two-phase Darcy flows

The extension of the discrete set of unknowns (35) to the non-isothermal compositional two-phase flow model is defined by

\[
U_D = \{(P^g_\nu, P^l_\nu, T_\nu, S^g_\nu, S^l_\nu, C^g_\nu, C^l_\nu), \nu \in \mathcal{M} \cup \mathcal{V} \cup \mathcal{F}_D^h\} \cup \{(P^g_\sigma, P^l_\sigma, T_\sigma), \sigma \in \mathcal{F}^h \setminus \mathcal{F}_D^h\}.
\]

We also consider the subset of phase pressure unknowns \(P_D^\alpha\) defined in (36), the subset of temperature unknowns

\[
T_D = \{T_\nu, \nu \in \mathcal{M} \cup \mathcal{V} \cup \mathcal{F}_D^h\},
\]

and the subset of the physical unknowns at a given \(\nu \in \mathcal{M} \cup \mathcal{V} \cup \mathcal{F}_D^h\)

\[
U_\nu = (P^g_\nu, P^l_\nu, T_\nu, S^g_\nu, S^l_\nu, C^g_\nu, C^l_\nu).
\]

Let us define the discrete Darcy fluxes for all \(K \in \mathcal{M}\) and \(\nu \in \text{dof}_K\) by

\[
F_{K,\nu}^\alpha(U_D) = F_{K,\nu}(P_D^\alpha) - \rho_{K,\nu}^\alpha F_{K,\nu}(G_D),
\]

where the phase mass density is defined by

\[
\rho_{K,\nu}^\alpha = \begin{cases} 
\rho^\alpha(P_K^\alpha, T_K, C_K^\alpha) + \rho^\alpha(P_\nu^\alpha, T_\nu, C_\nu^\alpha) & \text{if } \nu \in \text{dof}_K \cap (\mathcal{V} \cup \mathcal{F}_D^h), \\
\rho^\alpha(P_K^\alpha, T_K, C_K^\alpha)^2 + \rho^\alpha(P_L^\alpha, T_L, C_L^\alpha)^2 & \text{if } \nu \in \text{dof}_K \cap (\mathcal{F}^h \setminus \mathcal{F}_D^h), \mathcal{M}_\nu = \{K, L\}, \\
\rho^\alpha(P_K^\alpha, T_K, C_K^\alpha)^2 & \text{if } \nu \in \text{dof}_K \cap \mathcal{F}_N^h,
\end{cases}
\]
Let us also introduce the discrete Fourier fluxes for all \(K \in \mathcal{M}\) and \(\nu \in \text{dof}_K\) by

\[
\lambda_K G_{K,\nu}(T_D),
\]

where the thermal conductivity \(\lambda_K\) is a cell average of the bulk thermal conductivity computed explicitly from the previous time step variables, and \(G_{K,\nu}\) is the flux function (14) obtained with the identity diffusion tensor in all cells.

The discretization of the mobilities is obtained using the phase based upwind approximation. For each Darcy flux, let us define the phase dependent upwind control volume \((K\nu)\) such that

\[
(K\nu) = \begin{cases} 
K & \text{if } F^a_{K,\nu}(U_D) \geq 0 \\
\nu & \text{if } F^a_{K,\nu}(U_D) < 0 \text{ and } \nu \in \mathcal{V}^\nu \cup \mathcal{F}^h_D \\
L & \text{if } F^a_{K,\nu}(U_D) < 0 \text{ and } \nu \in \mathcal{F}^h \setminus \mathcal{F}^c_{ext}, \mathcal{M}_\nu = \{K, L\}
\end{cases}
\]

for \(K \in \mathcal{M}, \nu \in \text{dof}_K\).

Let us introduce the upwind approximation of the phase molar fluxes

\[
V^a_{K,\nu}(U_D) = \begin{cases} 
\zeta^a(U_{(K\nu)}^\alpha) \frac{k_{r,rt}(K\nu)}{\mu^a(U_{(K\nu)}^\alpha)} (S^a_{(K\nu)}^\alpha) F^a_{K,\nu}(U_D), & \text{if } \nu \in \mathcal{V}^\nu \cup \mathcal{F}^h \setminus \mathcal{F}^h_N, \\
0 & \text{if } \nu \in \mathcal{F}^h_N.
\end{cases}
\]

The discrete generalised compositional Darcy and flowing enthalpy fluxes write respectively

\[
V^a_{i,K,\nu}(U_D) = C^a_{i,(K\nu)} V^a_{K,\nu}(U_D), \quad K \in \mathcal{M}, \quad \nu \in \text{dof}_K, \quad i \in \mathcal{C},
\]

and

\[
V^a_{e,K,\nu}(U_D) = h^a(U_{(K\nu)}^\alpha) V^a_{K,\nu}(U_D), \quad K \in \mathcal{M}, \quad \nu \in \text{dof}_K.
\]

It leads to the following set of equations at each time step \(n = 1, \cdots, N_{tf}\) accounting for the cell conservation equations

\[
\begin{cases} 
\varphi_K \frac{n_i(U^n_K) - n_i(U^{n-1}_K)}{\Delta t^n} + \sum_{\alpha \in \mathcal{P}} \sum_{\nu \in \text{dof}_K} V^a_{i,K,\nu}(U^n_D) = 0, & i \in \mathcal{C}, \\
\varphi_K \frac{E_f(U^n_K) - E_f(U^{n-1}_K)}{\Delta t^n} + \varphi_K \frac{E_r(U^n_K) - E_r(U^{n-1}_K)}{\Delta t^n} + \sum_{\alpha \in \mathcal{P}} \sum_{\nu \in \text{dof}_K} V^a_{e,K,\nu}(U^n_D) + \sum_{\nu \in \text{dof}_K} \lambda^{-1}_{K,\nu} G_{K,\nu}(T^n_D) = 0,
\end{cases}
\] (46)
for $K \in \mathcal{M}$, the VAG node conservation equations

\[
\begin{align*}
\varphi_s \frac{n_i(U^n_s) - n_i(U^{n-1}_s)}{\Delta t^n} - \sum_{\alpha \in \mathcal{P}} \sum_{K \in \mathcal{M}_{s \setminus \mathcal{M}^\text{h}}} V_{i,K,s}(U^n_D) &= 0, \quad i \in \mathcal{C}, \\
\varphi_s E_f(U^n_s) - E_f(U^{n-1}_s) \Delta t^n + \varphi_s E_r(U^n_s) - E_r(U^{n-1}_s) \Delta t^n - \sum_{\alpha \in \mathcal{P}} \sum_{K \in \mathcal{M}_{s \setminus \mathcal{M}^\text{h}}} V_{e,K,s}(U^n_D) - \sum_{K \in \mathcal{M}_{s \setminus \mathcal{M}^\text{h}}} \lambda_{K,s}^{-1} G_{K,s}(T^n_D) &= 0,
\end{align*}
\]

for $s \in \mathcal{V}^v \setminus \mathcal{V}^D$, coupled with the Darcy and Fourier flux continuity equations and Neumann boundary conditions at HFV faces

\[
\sum_{K \in \mathcal{M}_{s \setminus \mathcal{M}^\text{h}}} F_{K,\sigma}^{\alpha}(P_{D,s}^{n-1}) = 0, \quad \alpha \in \mathcal{P}, \quad \sum_{K \in \mathcal{M}_{s \setminus \mathcal{M}^\text{h}}} \lambda_{K,s}^{-1} G_{K,\sigma}(T^n_D) = 0,
\]

for $\sigma \in \mathcal{F}_h \setminus \mathcal{F}^D$, the Dirichlet boundary conditions at Dirichlet nodes and faces

\[
P_{D,s}^{\alpha,n} = P_{D,s}^{\alpha}, \quad T_{D,s}^n = T_{D,s}, \quad S_{D,s}^{\alpha,n} = S_{D,s}^{\alpha}, \quad C_{D,s}^{\alpha,n} = C_{D,s}^{\alpha}, \quad \alpha \in \mathcal{P},
\]

and with the closure laws

\[
\begin{align*}
S_{D,s}^{\alpha,n} + S_{D,s}^{\beta,n} &= 1, \\
P_{D,s}^{\alpha,n} - P_{D,s}^{\beta,n} &= P_{crt,s}(S_{D,s}^{\alpha,n}), \\
\min(S_{D,s}^{\alpha,n}, 1 - \sum_{i \in \mathcal{C}} C_{D,s}^{\alpha,i,n}) &= 0, \quad \alpha \in \mathcal{P}, \\
f_i(P_{D,s}^{\alpha,n}, T_{D,s}^n, C_{D,s}^{\alpha,n}) &= f_i(P_{D,s}^{\alpha,n}, T_{D,s}^n, C_{D,s}^{\alpha,n}), \quad i \in \mathcal{C},
\end{align*}
\]

for $\nu \in \mathcal{M} \cup \mathcal{V}^v \setminus \mathcal{V}^D$.

The nonlinear system defined by the conservation equations (46)-(47), the flux continuity equations (48) and the local closure laws (50) is solved at each time step w.r.t. the set of unknowns $U_{D}^{n}$ (45) by a Newton-Raphson algorithm adapted to the complementary constraints (see [5] for details). The size of the linear system to be solved at each Newton iteration can be considerably reduced by elimination of the Dirichlet d.o.f. and by elimination for each d.o.f. $\nu \in \mathcal{M} \cup \mathcal{V}^v \setminus \mathcal{V}^D$ of the local closure laws (50) w.r.t. to a set of $\#\mathcal{C} + 4$ secondary unknowns $U_{D}^{S}$ chosen in such a way that the differential of the closure laws w.r.t. $U_{D}^{S}$ is non singular. A classical choice of the set of primary unknowns $U_{D}^{P} = U_{D} \setminus U_{D}^{S}$ is reported in Table 4. Furthermore, the
VAG cell unknowns $U_K$ and equations (46), $K \in \mathcal{M}^v$ can be eliminated from the linear system without any fill-in by Schur complement which considerably reduces the number of VAG d.o.f. in the case of simplicial meshes. Finally, in the case of superadmissibility of the cells $K \in \mathcal{M}^h \cup \mathcal{M}^{hv}$, as in Remark 1.4, the HFV scheme reduces to a TPFA scheme and the face unknowns $\{(P^g_\sigma, P^l_\sigma, T_\sigma), \sigma \in \mathcal{F}^h \setminus \mathcal{F}^h_D\}$ are eliminated from the Darcy and Fourier flux continuity equations (39) leading to the classical harmonic transmissibilities.

Table 4: Primary unknowns of the degree of freedom $\nu \in \mathcal{M} \cup \mathcal{V}^v \setminus \mathcal{V}^v_D$ depending on the active complementary constraints of the Newton-Raphson algorithm.

<table>
<thead>
<tr>
<th>Constraint</th>
<th>Unknowns</th>
</tr>
</thead>
<tbody>
<tr>
<td>$1 - \sum_{i \in C} C^g_{i,\nu} = 0$</td>
<td>$U^P_{\nu} = {P^g_{\nu}, S^g_{\nu}, (C^l_{i,\nu})_{i \in C \setminus {w}}}$</td>
</tr>
<tr>
<td>$1 - \sum_{i \in C} C^l_{i,\nu} = 0$</td>
<td>$U^P_{\nu} = {P^g_{\nu}, T_{\nu}, (C^l_{i,\nu})_{i \in C \setminus {w}}}$</td>
</tr>
<tr>
<td>$S^g_{\nu} = 0$</td>
<td>$U^P_{\nu} = {P^g_{\nu}, T_{\nu}, (C^l_{i,\nu})_{i \in C \setminus {w}}}$</td>
</tr>
<tr>
<td>$1 - \sum_{i \in C} C^g_{i,\nu} = 0$</td>
<td>$U^P_{\nu} = {P^g_{\nu}, T_{\nu}, (C^g_{i,\nu})_{i \in C \setminus {w}}}$</td>
</tr>
<tr>
<td>$S^l_{\nu} = 0$</td>
<td>$U^P_{\nu} = {P^g_{\nu}, T_{\nu}, (C^g_{i,\nu})_{i \in C \setminus {w}}}$</td>
</tr>
</tbody>
</table>

3.3 Two dimensional Bouillante geothermal test case

Geothermal energy is a carbon-free non-intermittent energy source which can represent an alternative to fossil energy both for power production and direct use, heat representing a large amount of the world final energy consumption. In countries with a favorable geological context, high temperature geothermal energy can even make a significant contribution to power production. Consequently, the world installed capacity is expected to double over the present decade [6]. Compositional multi-phase thermal Darcy flow models are essential tools to provide a quantitative assessment of deep geothermal resources, from exploration phases of geothermal operations with assessment of the geothermal potential, validation of conceptual hypothesis, well siting... to production phases to achieve an optimal and sustainable exploitation and prevent resource exhaustion.

High temperature geothermal fields are often located in active geological settings (e.g. plate boundaries, volcanic areas...) with complex natural...
structures and geometries such as fault networks with discontinuous properties and fractures that act as drain or barriers on the deep transfer of mass and energy, thus controlling the distribution of geothermal resources. The geological modelling of such systems and their discretization into conforming unstructured meshes are challenging tasks and often result in meshes that are hardly tractable for flow simulations. In such situation, hybrid meshes composed of different types of cells best suited to discretize the geology and geometry in different parts of the geothermal system represent a clear asset. Then, the scheme is adapted locally to the type of mesh/cells using the methodology developed in the previous sections.

In this section, we consider a simplified geological setting which corresponds to a 2D vertical cross-section of the Bouillante high temperature geothermal field (Guadeloupe, French West Indies). The vertical cross-section is assumed to be in the plane of major fault zone acting as a regional permeable drain. Our objective is to compare the results of the simulations on different meshes and schemes of the non-isothermal compositional liquid gas Darcy flow model. The following test cases focus on the coupling between the VAG scheme and the TPFA scheme assuming that the cells \( K \in \mathcal{M}^h \cup \mathcal{M}^{hv} \) satisfy the TPFA admissibility conditions. Only the unstabilised version of the combined VAG-TPFA scheme is considered in order to preserve the two-point fluxes at all faces \( \sigma \in \mathcal{F}^{hv} \).

We consider the above non-isothermal compositional two-phase Darcy flow model with the set of water and air components \( \mathcal{C} = \{a, w\} \). The thermodynamic laws used in this test case are the following. The gas phase is assumed to have a perfect gas molar density \( \zeta_g = \frac{P_g}{RT} \), \( R = 8.314 \text{ J.K}^{-1}.\text{mol}^{-1} \) and a constant gas dynamic viscosity fixed to \( \mu_g = 2 \cdot 10^{-5} \text{ Pa.s} \). The liquid molar enthalpy \( h_l^g \) and the gas molar enthalpies of each component \( h_{g,a}^g, h_{g,w}^g \) are taken from [25], from which the gas molar enthalpy is deduced assuming a perfect mixture

\[
h_g(P^g, T, C^g) = \sum_{i \in \mathcal{C}} C_i^g h_i^g(P^g, T).
\]

The liquid molar density and viscosity are also fixed to the constant values \( \zeta_l = \frac{1000}{0.0018} \text{ mol.m}^{-3} \) and \( \mu_l = 10^{-3} \text{ Pa.s} \) in order to avoid thermal convection instabilities which would prevent the comparison of the schemes on the different types of meshes. The mass density is defined by \( \rho^\alpha = \zeta^\alpha \sum_{i \in \mathcal{C}} m_i C_i^\alpha \) with the molar masses \( m_a = 0.029 \) and \( m_w = 0.018 \text{ Kg.mol}^{-1} \). The molar internal energy \( e^\alpha(T) \) of each phase \( \alpha \in \mathcal{P} \) is considered to be equal to its
enthalpy. The fugacities are defined by

\[
\begin{align*}
  f_i^g &= C_i^g P^g, & i &= a, w, \\
  f_a^l &= C_a^l H_a, \\
  f_w^l &= C_w^l P_{sat}(T) \exp \left( -\frac{P_{sat}(T) - P_i^l}{\xi^l R T} \right),
\end{align*}
\]

where the Henry constant of the air component is set to \( H_a = 10^{8} \, \text{Pa} \) and the vapour pressure \( P_{sat}(T) \) is given by the Clausius-Clapeyron equation

\[
P_{sat}(T) = 100 \exp \left( \frac{46.784 - 6435}{T} - 3.868 \log(T) \right).
\]

In this test case, the porous medium is homogeneous with porosity \( \phi(x) = 0.35 \) and isotropic permeability \( \Lambda(x) = K \times I \) with \( K = 1 \, \text{D} \). The relative permeabilities are defined by \( k_\alpha^r(S_\alpha) = (S_\alpha)^2 \) for each phase \( \alpha \in \mathcal{P} \) and the capillary pressure function is given by the Corey law

\[
P_c(S_g) = \begin{cases} 
  -b \ln(1 - S_g) & \text{if } 0 \leq S_g \leq S_1, \\
  -b \ln(1 - S_1) + \frac{b}{1 - S_1} (S_g - S_1) & \text{if } S_1 < S_g \leq 1,
\end{cases}
\]

regularized for \( S_g \in (S_1, 1] \) to allow for the disappearance of the liquid phase, with \( b = 2 \cdot 10^5 \, \text{Pa} \) and \( S_1 = 0.99 \). The rock energy per unit rock volume is fixed to \( E_r(T) = 2 \cdot 10^6 T \) in \( \text{J} \cdot \text{m}^{-3} \) and the bulk thermal conductivity of the fluid and rock mixture is fixed to \( \lambda = 3 \, \text{W} \cdot \text{m}^{-2} \cdot \text{K}^{-1} \). Figure 15 shows the 2D vertical cross-section of the Bouillante geothermal reservoir and the conditions applied at the domain boundary.

The initial and left side conditions are defined by a pure water liquid phase \( (S^l = 1, C_w^l = 1, C_a^l = 0) \) at hydrostatic pressure and by a linear temperature between the fixed top and bottom temperatures. The bottom boundary is impervious (zero Darcy fluxes) with a fixed temperature of 400 K except in the interval \( 8000 \, \text{m} \leq x \leq 10000 \, \text{m} \) where a pure water liquid input flux of \( -3 \cdot 10^{-2} \, \text{mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1} \) at 550 K is imposed. The right side of the domain is supposed thermally isolated (zero Fourier flux) and impervious (zero Darcy fluxes).

The upper boundary is composed of three parts corresponding to the seabed \( (z \leq 0 \, \text{m} \text{ and } 0 \leq x \leq 5000 \, \text{m}) \), a sunny plain zone \( (0 < z \leq 500 \, \text{m} \text{ and } 500 \, \text{m} < x \leq 8450 \, \text{m}) \) and a rainy mountain zone \( (z > 500 \, \text{m} \text{ and } 8450 \, \text{m} < x \leq 11000 \, \text{m}) \):

- the seabed boundary condition is defined by a pure water liquid phase \( (S^l = 1, C_w^l = 1) \) at hydrostatic pressure. The temperature is sea depth dependent. It is linear between the sea level \( z = 0 \, \text{m} \) at 300 K and \( z = -100 \, \text{m} \) at 278 K, then constant below \( z = -100 \, \text{m} \),
• the sunny plain zone is defined by the relative humidity fixed to 0.5, the temperature fixed to 300 K and the gas pressure fixed to $P_g = 1\, \text{atm}$, from which we deduce that only the gas phase is present with the molar fractions roughly equal to $C_g^a \approx 0.99$, $C_g^w \approx 10^{-2}$,

• the rainy mountain zone is characterized by a two-phase state at thermodynamic equilibrium which is defined by a fixed temperature, gas pressure and relative humidity corresponding to the following physical values:

\[
\begin{align*}
S_g &\approx 0.72, & S_l &\approx 0.28, \\
P_g & = 1\, \text{atm}, & P_l & \approx -153671\, \text{Pa}, \\
C_g^a & \approx 0.97, & C_g^w & \approx 0.03, \\
C_l^a & \approx 10^{-3}, & C_l^w & \approx 0.999, \\
T & = 300\, \text{ K}.
\end{align*}
\]

The simulations are run over the time interval $(0, t_f)$, $t_f = 650$ years, with an adaptive time stepping starting with an initial time step of 1 day and with a maximum time step of 150 days. Three meshes of roughly 18500 cells have been generated, a triangular mesh, a Voronoi mesh admissible both at inner and boundary faces and an hybrid mesh exhibited in Figure 16 combining Cartesian cells on the bottom subdomain $\Omega \setminus \Omega^v$ and triangular cells on the upper VAG subdomain $\Omega^v$ with $\Omega^v = \{ x \in \Omega \mid z > -1500 \, \text{m} \}$.

The numerical results on the various combinations of meshes and schemes
are compared to a reference solution obtained on a refined hybrid mesh with roughly 78000 cells including Cartesian cells on the TPFA subdomain \( \Omega \setminus \Omega_v \) and triangular cells on the VAG subdomain \( \Omega_v \).

![Coarse hybrid Cartesian-triangular mesh.](image)

**Figure 16:** Coarse hybrid Cartesian-triangular mesh.

![Reference temperature (in K) and gas saturation at final time (650 years) obtained with the refined Cartesian-Voronoi mesh combined with the VAG-TPFA scheme.](image)

**Figure 17:** Reference temperature (in K) and gas saturation at final time (650 years) obtained with the refined Cartesian-Voronoi mesh combined with the VAG-TPFA scheme.

![Temperature (in K) and gas saturation at final time (650 years) obtained with the VAG scheme on the triangular mesh.](image)

**Figure 18:** Temperature (in K) and gas saturation at final time (650 years) obtained with the VAG scheme on the triangular mesh.

Figures 17-20 show the temperature (on the left) and the gas saturation (on the right) at final time for the different combinations of meshes and schemes. All the numerical results are very similar and no visible artefact can be seen at the interface \( z = -1500 \text{ m} \) for the VAG-TPFA scheme.

However, a closer comparison with the reference solution focusing on the bottom part of the domain in the temperature plots exhibits that the Cartesian mesh combined with the TPFA scheme provides a more accurate solution. It can be explained by the quasi horizontal geometry of the flow lines.
Figure 19: Temperature (in K) and gas saturation at final time (650 years) obtained with the TPFA scheme on the Voronoi mesh.

Figure 20: Temperature (in K) and gas saturation at final time (650 years) obtained with the VAG-TPFA scheme on the Cartesian-triangular mesh.

close to the bottom boundary which is better captured by the Cartesian mesh coupled with the TPFA scheme (see Figure 20 compared with Figures 18, 19).

Figure 21: Ratio between the gas volume and the total pore volume as a function of time with log time scale for the various discretizations.

Figure 21 exhibits the ratio between the gas volume and the total pore volume as a function of time which is characteristic of the solution close to the top boundary. The graphic highlights two phenomena. First the desaturation of the vadose zone induced by the top Dirichlet boundary condition for $z > 0$. Then, around $t = 70000$ days, the plots exhibit the vaporization of the water component occurring when the high temperature front reaches the
low pressure zone close to the top boundary. The desaturated zone is thin compared to the height of the reservoir and strongly depends on the size of the top cells. This explains the small discrepancies observed between the plots obtained with the various schemes which have been checked to converge to the reference solution on refined meshes.

<table>
<thead>
<tr>
<th>scheme</th>
<th>mesh</th>
<th>$N_{\text{red}}$</th>
<th>$NZ_{\text{red}}$</th>
<th>$N_{tf}$</th>
<th>$N_{\text{chps}}$</th>
<th>$N_{\text{newton}}$</th>
<th>CPU</th>
</tr>
</thead>
<tbody>
<tr>
<td>VAG</td>
<td>triangular</td>
<td>9616</td>
<td>65822</td>
<td>1726</td>
<td>9</td>
<td>4.76</td>
<td>10178</td>
</tr>
<tr>
<td>TPFA</td>
<td>Voronoi</td>
<td>18828</td>
<td>128303</td>
<td>1709</td>
<td>6</td>
<td>4.12</td>
<td>15331</td>
</tr>
<tr>
<td>VAG-TPFA</td>
<td>Cart.-tri.</td>
<td>14702</td>
<td>82984</td>
<td>1933</td>
<td>25</td>
<td>3.95</td>
<td>10936</td>
</tr>
</tbody>
</table>

Table 5: Number of d.o.f. after elimination of the VAG cells and TPFA faces, number of 3 by 3 non-zero elements in the matrix after elimination of the VAG cells and TPFA faces, number of successful time steps, number of time step chops, average number of Newton-Raphson iterations per time step and CPU time (in s) obtained with the different meshes and schemes.

Table 5 compares the numerical behavior of the simulation with $N_{\text{red}}$ the number of degree of freedom of the reduced linear systems with 3 primary unknowns per d.o.f., $NZ_{\text{red}}$ the number of non-zero 3 by 3 entries in the reduced linear systems, $N_{tf}$ the number of successful time steps, $N_{\text{chps}}$ the number of time step chops and $N_{\text{newton}}$ the average number of Newton-Raphson iterations per successful time step. The CPU times are in seconds on 2.9 GHz Intel Core i5 processor and 8Go RAM. This table exhibits large differences in CPU time between the different meshes and schemes whereas the numbers of cells are comparable for all meshes. Thanks to the elimination of the VAG cell unknowns for all $K \in \mathcal{M}^e$, the number of non-zero entries in the Jacobian matrix is the smallest with the VAG scheme combined with the triangular mesh. It results that the VAG scheme combined with the triangular mesh leads to the fastest solution. On the other hand, as explained above, it also leads to a less accurate solution compared with the solution obtained using the TPFA scheme combined with a Cartesian mesh on the lower part of the reservoir. All together, the Cartesian-triangular mesh combined with the VAG-TPFA scheme provides the best compromise in terms of CPU time and accuracy for this geothermal test case.

**Conclusion**

A new methodology is introduced in this work to combine face based (HFV or TPFA) and nodal based (VAG) discretizations on hybrid meshes in order to adapt the numerical scheme to the different types of cells and medium
properties in different parts of the mesh. The stability and convergence of the combined VAG-HFV schemes is studied in the gradient discretization framework and is shown to hold on arbitrary partitions of the cells for the unstabilised version and on arbitrary partitions of the faces for the stabilised version. The framework preserves at the interface the discrete conservation properties of the VAG and HFV schemes with fluxes based on local to each cell transmissibility matrices of size the number of d.o.f. at the cell boundary. This discrete conservative form allows a natural extension of the VAG and HFV discretizations of two-phase Darcy flow models to the combined VAG-HFV schemes. Numerical results on different types of meshes show the accuracy and efficiency of the combined schemes which are compared to the standalone VAG and HFV (or TPFA) discretizations. The convergence of the schemes is first studied numerically for single-phase and two-phase Darcy flows using analytical solutions. Then, a non-isothermal compositional liquid gas Darcy flow test case representing a 2D vertical cross-section of the Bouillante geothermal reservoir is considered. For this test case, the combined VAG-TPFA scheme on an hybrid Cartesian triangular mesh is shown to provide the best compromise between accuracy and CPU time compared with the VAG scheme on a triangular mesh and the TPFA scheme on a Voronoi mesh.

References


