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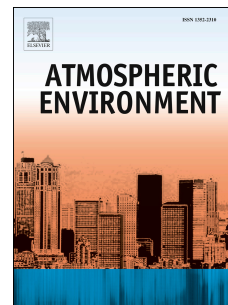
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Dilution effects on ultrafine particle emissions from Euro 5 and Euro 6 diesel and gasoline vehicles

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Abstract

Dilution and temperature used during sampling of vehicle exhaust can modify particle number concentration and size distribution. Two experiments were performed on a chassis dynamometer to assess exhaust dilution and temperature on particle number and particle size distribution for Euro 5 and Euro 6 vehicles. In the first experiment, the effects of dilution (ratio from 8 to 4000) and temperature (ranging from 50 °C to 150 °C) on particle quantification were investigated directly from tailpipe for a diesel and a gasoline Euro 5 vehicles. In the second experiment, particle emissions from Euro 6 diesel and gasoline vehicles directly sampled from the tailpipe were compared to the constant volume sampling (CVS) measurements under similar sampling conditions. Low primary dilutions (3–5) induced an increase in particle number concentration by a factor of 2 compared to high primary dilutions (12–20). Low dilution temperatures (50 °C) induced 1.4–3 times higher particle number concentration than high dilution temperatures (150 °C). For the Euro 6 gasoline vehicle with direct injection, constant volume sampling (CVS) particle number concentrations were higher than after the tailpipe by a factor of 6, 80 and 22 for Artemis urban, road and motorway, respectively. For the same vehicle, particle size distribution measured after the tailpipe was centred on 10 nm, and particles were smaller than the ones measured after CVS that was centred between 50 nm and 70 nm. The high particle concentration ($\approx 10^6$ #/cm³) and the growth of diameter, measured in the CVS, highlighted aerosol transformations, such as nucleation, condensation and coagulation occurring in the sampling system and this might have biased the particle measurements.

Keywords

Gasoline and diesel emissions; CVS; Tailpipe; Dilution; Temperature; Ultrafine particle; Nucleation; Condensation; Coagulation

Abbreviations

G-DI	Gasoline with Direct Injection	DPF	Diesel Particulate Filter
cat	Catalysed Filter	PMP	Particle Measurement Programme
CVS	Constant Volume Sampler	FPS	Fine Particle Sampler
NO _x	Nitrogen Oxides	NO ₂	Nitrogen Dioxide
NO	Nitric Oxide	PN	Particle Number
CPC	Condensation Particle Counter	ELPI	Electrical Low Pressure Impactor
SMPS	Scanning Mobility Particle Sizer	FMPS	Fast Mobility Particle Sizer Spectrometer
HEPA	high-efficiency particulate air		

40 1 Introduction

41 Vehicle exhaust emissions represent a major source of particle matter in urban environments.
42 On regional and global scales, atmospheric particles play an important role in human health and
43 climate change (Ning, 2010; Kulmala et al., 2000; Pope III, 2000). Particles emitted from diesel and
44 gasoline engines are ultrafine particles with size ranges of 20–130 nm and 20–60 nm, respectively
45 (Karjalainen et al., 2014; Morawska et al., 2008; Burtscher 2005; Jamriska et al., 2004). The ultrafine
46 particles represent only 0.1–10% of the total particulate mass, but it might represent more than 90% of
47 the total particle number (Giechaskiel et al., 2010; Kittelson, 1998). Particle emission depends on the
48 engine technology, fuel and aftertreatment devices. Liang et al. (2013) and Köhler (2013) showed that
49 the gasoline direct injection (G-DI) technology induced an increase in the particle number
50 concentration compared to the standard gasoline passenger cars. Moreover, the dilution process
51 (dilution ratio, dilution gas temperature and sampling residence time) has been established as a factor
52 influencing ultrafine particle formation (Manoukian et al., 2016; Wei et al., 2016; Ranjan et al., 2012;
53 Fujitani et al., 2012; Mamakos and Martini, 2011; Grieshop et al., 2009a; Vouitsis et al., 2008;
54 Rönkkö et al., 2006; Mathis et al. 2004). After the tailpipe, the exhaust undergoes high and fast
55 atmospheric dilution ratio that could reach up from 1000 to 4000 in 1–3 s (Fujitani et al., 2012; Zhang
56 and Wexler, 2004). The exhaust temperature (around 200 °C) decreases rapidly at ambient
57 temperature level within few seconds after emission due to the high dilution ratio. The rapid decrease
58 in temperature has significant implications in terms of thermodynamics of particles and semi-volatile
59 compounds (Kim et al., 2016; Huang et al., 2014; May et al., 2013; Wang and Zhang, 2012; Kozawa et
60 al., 2012; Mamakos and Martini, 2011; Casati et al., 2007; Morawska et al., 2008; Zhang et al., 2004)
61 leading to a drastic change in particle number concentration and size distribution (Huang et al., 2014;
62 Wang and Zhang, 2012; Uhrner et al., 2011; Grieshop 2009b). Although several recent studies have
63 focused on that issue, uncertainties still remain regarding the experimental determination of ultrafine
64 particle emissions from vehicle exhaust and the impact of dilution and temperature during their
65 sampling (Wei et al., 2016; Manoukian et al., 2016; Ranjan et al., 2012; Fujitani et al., 2012; Grieshop
66 et al., 2009a).

67 Particle number concentration is measured through a specific protocol, derived from the
68 Particle Measurement Program (PMP) through the full-flow Constant Volume Sampler (CVS). This
69 protocol requires the removal of the volatile phase by the dilution stage (150 °C) and a heated tube (at
70 300–400 °C). The PMP approach only regulates the non-volatile fraction of particles in order to
71 exclude the possible confounding of measurement data by low volatility hydrocarbons manifesting as
72 a nucleation mode present below 20 nm that highly depends on the sampling conditions (Giechaskiel
73 et al., 2008). In the atmosphere, the concentration of aerosols changes rapidly in the first seconds after
74 emission with condensation phenomenon and presence of SVOCs, which strongly depend on the
75 exhaust sampling (length of the sampling line, dilution factor, temperature, etc.) (Albriet et al., 2010).
76 Several studies showed that the ultrafine particle number concentration directly measured from the
77 tailpipe was significantly different than those from the CVS (Kim et al., 2016; Giechaskiel et al., 2010,
78 2007; Mathis et al., 2005). Giechaskiel et al. (2010) showed that deceleration (from 140 km/h to 120
79 km/h) induced a higher particle number concentration with higher mean diameter than acceleration
80 (from 90 km/h to 120 km/h) with a Euro 3 diesel vehicle without particulate filter. This observation is
81 in contrast with their previous work (Giechaskiel et al., 2007), which reported a lower particle number
82 concentration during deceleration than during acceleration. This contradiction can be explained by
83 differences in sampling systems. According to Giechaskiel et al. (2007), particles were sampled
84 directly from the tailpipe, while in Giechaskiel et al. (2010), particles were sampled from the CVS. As
85 mentioned by Giechaskiel et al. (2014), the CVS dilution tunnel has several disadvantages such as the
86 inability to control the dilution ratio and the dilution temperature, a long sampling path and a long

87 residence time. This dilution system favours nucleation, condensation and coagulation that could
88 induce the new particle formation or the modification of the particle size distribution.

89 Based on this evidence, the particle measurement directly from the tailpipe was considered as
90 a complementary sampling method to CVS in order to understand the sampling condition impacts on
91 particle number concentration. This work aimed to investigate the impacts of dilution and temperature
92 on particle emissions after a CVS tunnel system and directly from the tailpipe with Euro 5 and Euro 6
93 vehicles. Particle number and size distribution between the CVS and the tailpipe were compared under
94 similar dilution conditions to investigate the processes occurring in the dilution tunnel with the Euro 6
95 G-DI vehicle. Finally, we discussed the nucleation, condensation and coagulation phenomena
96 observed into the CVS dilution system.

97 2 Materials and methods

98 2.1 Vehicle characteristics

99 Four currently in-use vehicles were studied: a Euro 5 gasoline with direct injection system (G-
 100 DI), and Euro 5 diesel with catalysed particulate filter (DPF cat), a Euro 6 G-DI and a Euro 6 DPF cat.
 101 Technical characteristics of the tested vehicles are shown in Table 1. All the tested vehicles were
 102 private vehicles to be as representative as possible of the state of the current French fleet. All
 103 experiments were conducted using commercial fuel (sulphur content less than 10 ppm) pumped from
 104 the same petrol station to minimize variability of fuel composition and its impact on emissions.

105 Table 1. Technical characteristics of the tested vehicles.

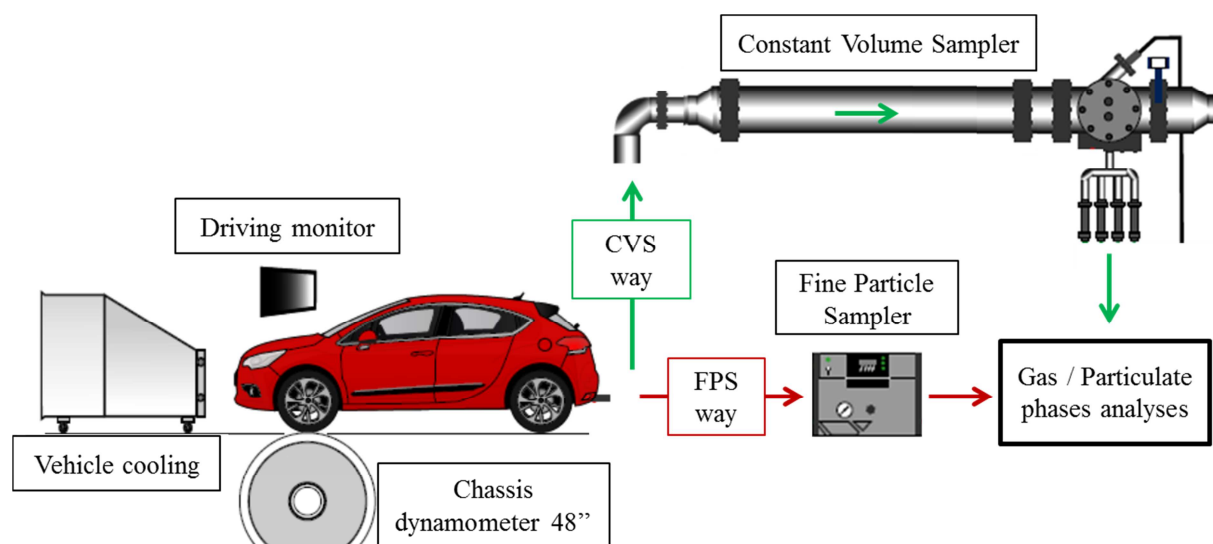
Vehicle	No. 1	No. 2	No. 3	No. 4
Size class	1.2	1.5	1.0	1.5
Technology	G-DI*	Diesel	G-DI*	Diesel
Standard	Euro5	Euro5	Euro 6	Euro 6
Empty weight (kg)	1320	1090	864	1087
Mileage (km)	25844	87073	2164	4700
Gearbox type	Manual (5)	Manual (5)	Manual (5)	Manual (5)
Registration date	27/02/2014	17/02/2012	11/12/2015	31/12/2015
Test date	31/03/2015	15/04/2015	29/03/2016	11/04/2016
Catalyst	Three-way	Oxidation	Three-way	Oxidation
Filter	No	Catalysed DPF [§]	No	Catalysed DPF [§]

106 * G-DI: Gasoline with direct injection system

107 [§] DPF: Diesel Particulate Filter

108 2.2 Experimental set-up

109 Emission measurements were performed on the chassis dynamometer at the Transports and
 110 Environment Laboratory (LTE) of the French Institute of Science and Technology for Transport,
 111 Development and Networks (IFSTTAR). The chassis dynamometer was composed of a 48-inch roller
 112 on which the drive wheels of the vehicle were placed. The dynamometer resisted to the vehicle rolling
 113 to simulate the road resistance, which was calculated based on road laws for each vehicle. The schema
 114 of the experimental setup is shown in Figure 1. Vehicle exhausts were sampled through two different
 115 ways: one directly at the tailpipe, diluted by the fine particle sampler (FPS) and the other through the
 116 CVS. Exhaust sampling from these two systems was diluted with filtered ambient air system.



117

118 Figure 1. Schema of the experimental setup; the green arrows represent the CVS way and the red
119 arrows represent the direct tailpipe way with FPS dilution.

120 2.2.1 Dilution systems

121 • Constant Volume Sampler (CVS)

122 Exhaust emissions measured using a CVS system were diluted with filtered ambient air (4 filters in
123 series including M6-F7-F9, M5, F7 EN-779-2012 filters, a HEPA H13 EN1822-2009 filter and a
124 cylindrical cartridge of charcoal scrubber). This filtered air allowed compensating the flow rate
125 variations related to the exhaust flow fluctuations and keeping a constant volume sampling. The
126 mixture air/exhaust went through the dilution tunnel, and then was monitored by different on-line gas
127 and particulate phase analysers.

128 • Fine Particle Sampler (FPS)

129 A Fine Particle Sampler (FPS 4000, Dekati Ltd) was used for direct tailpipe dilution. The exhaust
130 dilution was carried out in two stages: a primary dilution, close to the sampling point with controlled
131 temperature and a secondary dilution as ejector type diluter, located downstream of the primary
132 dilution and which adjusted the primary dilution to provide the total dilution. The FPS enabled the
133 control of several dilution parameters such as sampling flow, primary dilution, total dilution and
134 temperature.

135 2.2.2 Experimental protocol

136 Dilution and temperature effects were studied with two Euro 5 vehicles: gasoline (No. 1) and
137 diesel (No. 2). The vehicles were tested with two Artemis cycles (motorway and urban) (André, 2004)
138 and at 70 km/h steady speed. The particles were sampled from the tailpipe after the FPS dilution with
139 or without VKL diluters (depending on the total dilution tested). The FPS dilution temperatures were
140 set at 50°C, 100°C, and 150°C and the total dilution ratios were 30, 100, 400, 1000, 2000 and 4000 for
141 gasoline and 8, 12, 16, 30, 100, 400, 1000, 2000, 4000 for diesel. Each experimental condition was
142 repeated three times.

143 To compare the tailpipe emissions with the CVS measurements, the Euro 6 gasoline (No.3)
144 and the diesel (No.4) vehicles were tested with Artemis road, motorway and urban driving conditions.
145 The detailed driving cycles with repeated tests and sampling conditions were shown in Table 2. The
146 CVS operated at a total flow rate of 11 m³/min for the Artemis motorway cycle and 9 m³/min for the
147 other driving cycles. The average CVS dilution ratios ranged between 13 and 60 for the gasoline
148 vehicle and between 22 and 77 for the diesel vehicle, with a dilution temperature at 35 °C. At the

149 tailpipe the FPS primary dilution was set at 36°C to reproduce similar dilution and temperature
150 conditions as in the CVS.

151 Table 2. Detailed driving cycles with test number and sampling conditions for the FPS and the CVS
152 with Euro 6 G-DI (No.3) and Euro 6 diesel DPF cat (No.4) vehicles.

Vehicles	Euro 6 G-DI (No. 3)				Euro 6 diesel DPF cat (No. 4)			
	Repeated number	CVS dilution	Total tailpipe dilution	Primary dilution	Repeated number	CVS dilution	Total tailpipe dilution	Primary dilution
Road	9	33	35	22	9	51	54	25
Urban	10	60	59	25	10	77	88	27
Motorway	6	13	15	12	6	22	18	17

153 2.3 Analytical methods

154 2.3.1 Regulated compound analysis

155 Regulated compounds, such as carbon oxide (CO), carbon dioxide (CO₂), total hydrocarbons
156 (THC), nitric oxide (NO) and nitrogen oxides (NO_x) were monitored using a Horiba emission
157 measurement system (CO and CO₂ by non-dispersive infrared, THC by flame ionization detection, NO
158 and NO_x by chemiluminescence). The NO₂ concentration was determined by subtracting NO from
159 NO_x. Regulated compounds were monitored to ensure that vehicles had regular emission behaviours
160 with respect to their category and to detect any abnormalities that could introduce bias in the
161 measurements.

162 2.3.2 Particulate phase analysis

163 The particle number concentration and the size distribution were measured by a Fast Mobility
164 Particle Sizer Spectrometer (FMPS, model 3091 TSI). Particles went through a cyclone with a 1µm cut
165 off and an electrical diffusion charger. The particle number concentration from 5.6 nm to 560 nm is
166 determined by measuring the electrical current collected on a series of electrodes. Data were collected
167 every second at 8 L/min. The quantification limit depended on the particle size: for 5.6 nm the
168 maximum limit was 10⁷ #/cm³ and the minimum limit was 100 #/cm³. Particle size number distribution
169 was also characterised using an Electrical Low Pressure Impactor (ELPI, Dekati). The ELPI measured
170 the particle number distribution in the 7 nm to 4 µm range with 12 filter stages. The operating flow
171 rate of the ELPI was set at 10 L/min with a sampling period of 1s. The quantification limits ranged
172 from 250 to 7×10⁷ #/cm³ for particles with a diameter between 7 nm and 4 µm and from 0.1 to 2×10⁴
173 #/cm³ for particles with a diameter greater than 4 µm. A Condensation Particle Counter (CPC, model
174 3775 TSI) was used for total particle number concentration. The CPC contained a butanol
175 condensation chamber that enabled the detection of particles greater than 4 nm (particle size cut 50%).
176 The operating flow rate of CPC was set at 1.5 L/min. The experimental data were collected every
177 second with a concentration ranging from 0 to 10⁷ #/cm³.

178 The Particle Measurement Programme has been proposed as a regulatory approach for
179 measuring particle numbers for Euro 5 and Euro 6 vehicles, with a 50% cut-point size of 23 nm.
180 However, most particles emitted by the tested vehicles in our previous experiments were ultrafine
181 particles with diameters below 23 nm, especially during the Artemis motorway driving cycle and

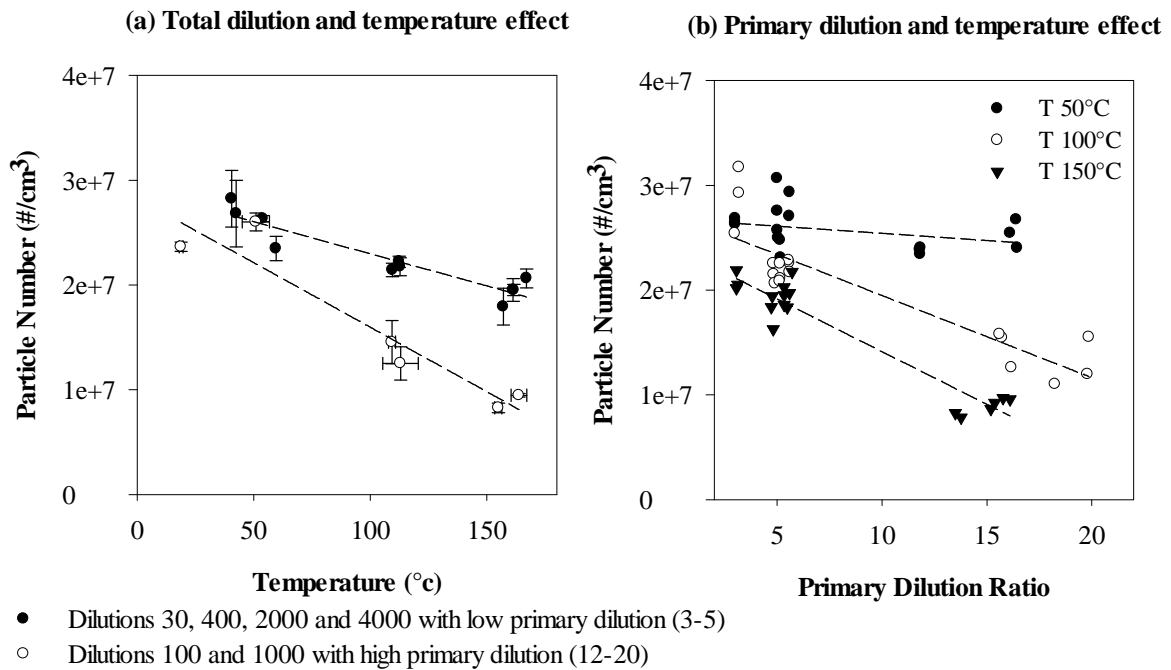
182 particulate filter regeneration (Louis et al., 2016). In order to have the most complete information on
183 total particle number emissions including particles smaller than 23 nm, and to compare it with direct
184 tailpipe emission, we did not fully follow the PMP protocol in this study. However the CVS tunnel
185 was conditioned according the latest regulatory requirement in Europe with heated air dilution at
186 35°C. Furthermore, by considering the volatile fraction of particles, the standard variations of particle
187 number concentration with six repeated tests, ranged from 7 to 11%.

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188 3 Results and discussion

189 3.1 Dilution and temperature effects

190 For the Euro 5 gasoline vehicle, the exhaust was sampled directly from the tailpipe at different
191 total dilution ratios through the FPS (at 30, 100, 400, 1000, 2000 and 4000). The total dilution ratios at
192 30, 400, 2000 and 4000 were obtained with low primary dilution ratios between 3 and 5, while the
193 total dilution at 100 and 1000 were obtained with high primary dilution ratios between 12 and 20.
194 Figure 2a showed the particle number concentration with the total dilution ratios between 30 and 4000
195 as function of the dilution temperature at 50, 100 and 150 °C during motorway driving condition. We
196 observed that the temperature played an important role on particle concentrations. According to
197 Beckers et al. (2009), low temperature (50 °C) induced 1.4 to 3 times more PN than high temperature
198 (150 °C) for all tested dilution ratios. The PN concentrations were classified into two groups: black
199 dots for total dilution of 30, 400, 2000 and 4000 characterized by a low primary dilution (3–5); white
200 empty dots for the total dilution at 100, 1000 with high primary dilution (12–20). These latter total
201 dilutions induced less particle emissions than dilution at 30, 400, 2000 and 4000 (Figure 2a). This can
202 be explained by the fact that dilution ratios 100 and 1000 were achieved using high primary dilution
203 ratio and it emphasised the key role of the primary dilution ratio. Figure 2b showed the particle
204 number emissions from a gasoline vehicle as function of the primary dilution (3–20) under motorway
205 driving condition with three primary dilution temperatures (50, 100 and 150°C). The particle number
206 concentration was corrected taking into account the dilution factors. At low primary dilution (3–5)
207 with the three tested dilution temperatures, PN concentrations were at $2\text{--}3 \times 10^7 \text{ \#/cm}^3$. For these
208 sampling conditions, PN concentration did not depend on the dilution gas temperature. At high
209 primary dilution conditions (12–20), PN concentration decreased with the increase in temperature. PN
210 emissions were about 2 times lower (at $1\text{--}1.5 \times 10^7 \text{ \#/cm}^3$) at 100°C and 150°C than at 50°C. For the
211 same temperature at 100 and 150 °C, the PN concentration decreased with the increase in the primary
212 dilution ratio. These results were in agreement with the ones reported by Casati et al. (2007) for Euro3
213 diesel passenger cars. Their results indicated that the low primary dilution and the low dilution
214 temperature of gas might promote the measurement bias. They recommended setting the sampling
215 system at a high primary dilution and high dilution temperature to minimise those bias. For the Euro 5
216 diesel vehicle, PN emissions were low due to the high filtration efficiency of the diesel particulate
217 filter (DPF). The particle number concentrations were lower than the detection limit of the instrument
218 for most of the dilution conditions and were not presented.



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Figure 2. Total dilution and temperature effects (a) and primary dilution and temperature effects (b) for the gasoline Euro 5 vehicle (No. 1) during the motorway driving conditions, at 50°C, 100°C and 150°C. The particle number emissions are corrected taking into account of the dilution factors. For the figure 2a, the black dots show total dilution ratios at 30, 400, 2000 and 4000 with low primary dilution (3–5) and the white dots show total dilution ratios at 100 and 1000 with high primary dilution (12–20).

3.2 Euro 6 G-DI particle characterisation tailpipe / CVS

PN emissions measured from the tailpipe have also been compared with CVS measurements for two Euro 5 vehicles under Artemis motorway cycle. Statistically significant differences in PN concentration have been observed between these two sampling systems. Particle size distribution was unimodal and centred at 20 nm after the tailpipe (FPS sampling system) and at more than 60 nm after the CVS. However, different analysers have been used for the PN quantification at the tailpipe (with an ELPI) and after the CVS (with a SMPS) due to experimental organisation and constraints. Therefore, in order to better understand the physical processes occurring in the sampling systems, with their impact on PN measurement, two Euro 6 gasoline and diesel vehicles have been tested. The PN concentrations have been followed by a FMPS after the tailpipe and after the CVS with Artemis Urban, Road and Motorway cycles. Primary dilution at 20 was chosen to the tailpipe dilution in order to minimise the PN concentration measurement bias.

3.2.1 Particle concentration comparison between tailpipe and CVS

Due to the high efficiency of the diesel particulate filter, PN emission from the Euro 6 diesel vehicle was lower than the analyser detection limit. Therefore, only gasoline emissions were presented and discussed here. Table 3 showed the average particle number concentrations for Euro 6 gasoline G-DI for the Artemis urban, road and motorway driving cycles. The concentrations reported were average values of several repeated cycles for each driving condition. The PN measurement after CVS and tailpipe were performed under similar total dilution and temperature conditions (Table 2). PN concentrations from CVS were higher than at tailpipe by a factor of 6, 80 and 22 for Artemis urban, road and motorway, respectively. Highest discrepancies were observed under Artemis road cycle. Unfortunately, we did not find an explication, since the tests were repeated 5 and 3 times after CVS and exhaust, respectively, which showed similar result.

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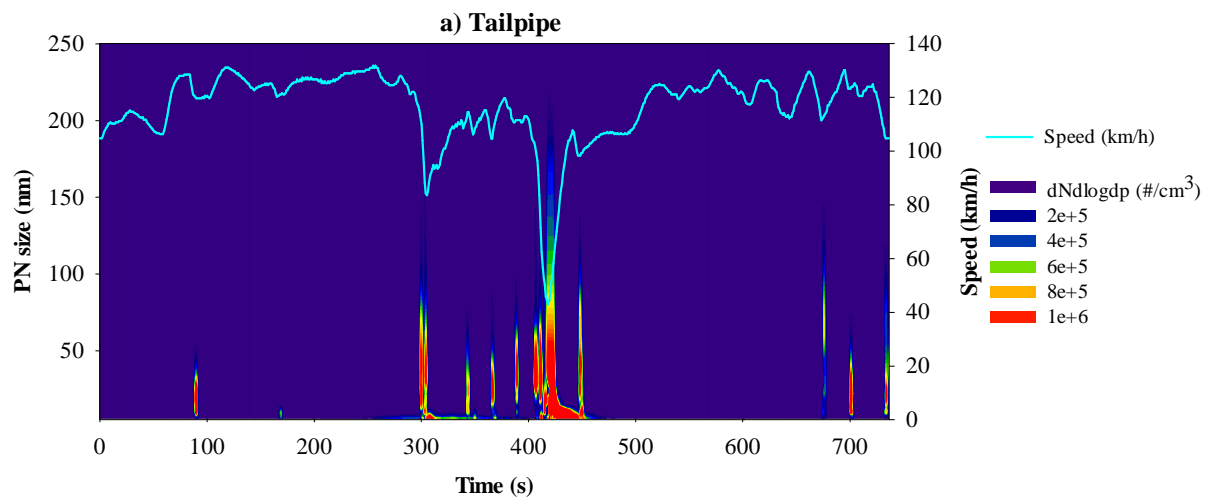
Table 3. Average particle number concentration for G-DI Euro 6 vehicle.

Particle concentration ($\#/cm^3$) G-DI Euro 6						
Driving cycle		Start	CVS	Tests Number	Exhaust	Tests Number
Artemis	urban	hot start	$(9 \pm 5) \times 10^4$	7	$(1.4 \pm 0.6) \times 10^4$	3
Artemis	road	hot start	$(2.3 \pm 0.4) \times 10^6$	5	$(3 \pm 2) \times 10^4$	3
Artemis	motorway	hot start	$(2.2 \pm 0.1) \times 10^7$	3	$(1.0 \pm 0.3) \times 10^6$	3

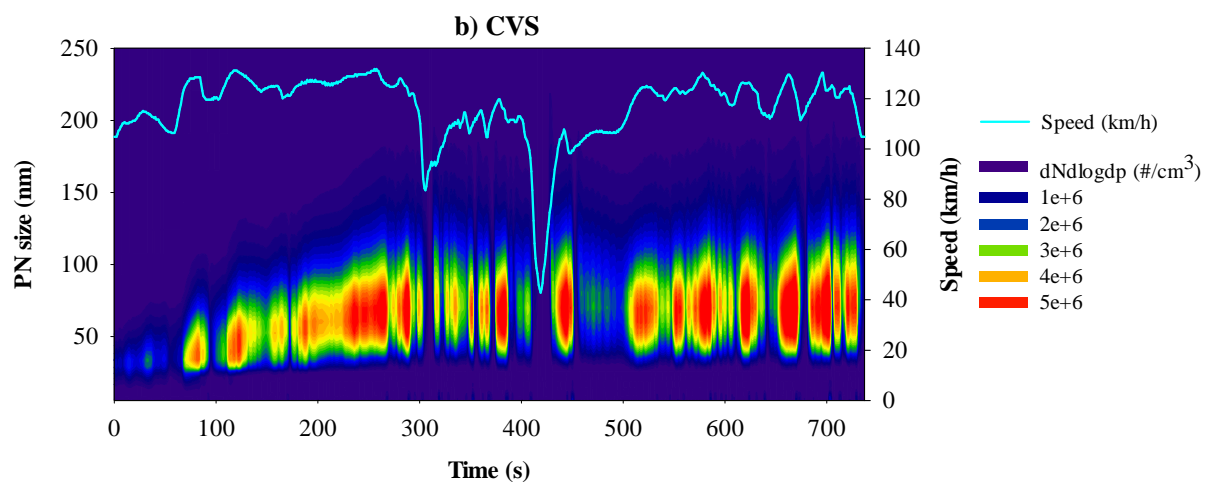
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3.2.2 Particle size distribution comparison between the tailpipe and the CVS

Figure 3 showed the particle number concentration and size distribution as a function of cycle time for the Euro 6 G-DI vehicle during an Artemis motorway driving cycle after the tailpipe (Figure 3a) and after the CVS (Figure 3b). At the tailpipe, particle emissions were characterised by narrow peaks of about 5s mainly during accelerations (Figure 3a), while after CVS particle emissions were characterised by larger emission peaks of about 30s and were observed for the whole cycle length (Figure 3b). Particle size distribution after tailpipe varied between 2 nm and 70 nm with a main mode at 10 nm. After the CVS the particle size distribution was centred at 50 nm and no particles below 30 nm were detected. This observation indicated that condensation and possibly coagulation happened. We observed an increase in PN after the CVS suggesting that also nucleation occurred in the CVS tunnel.



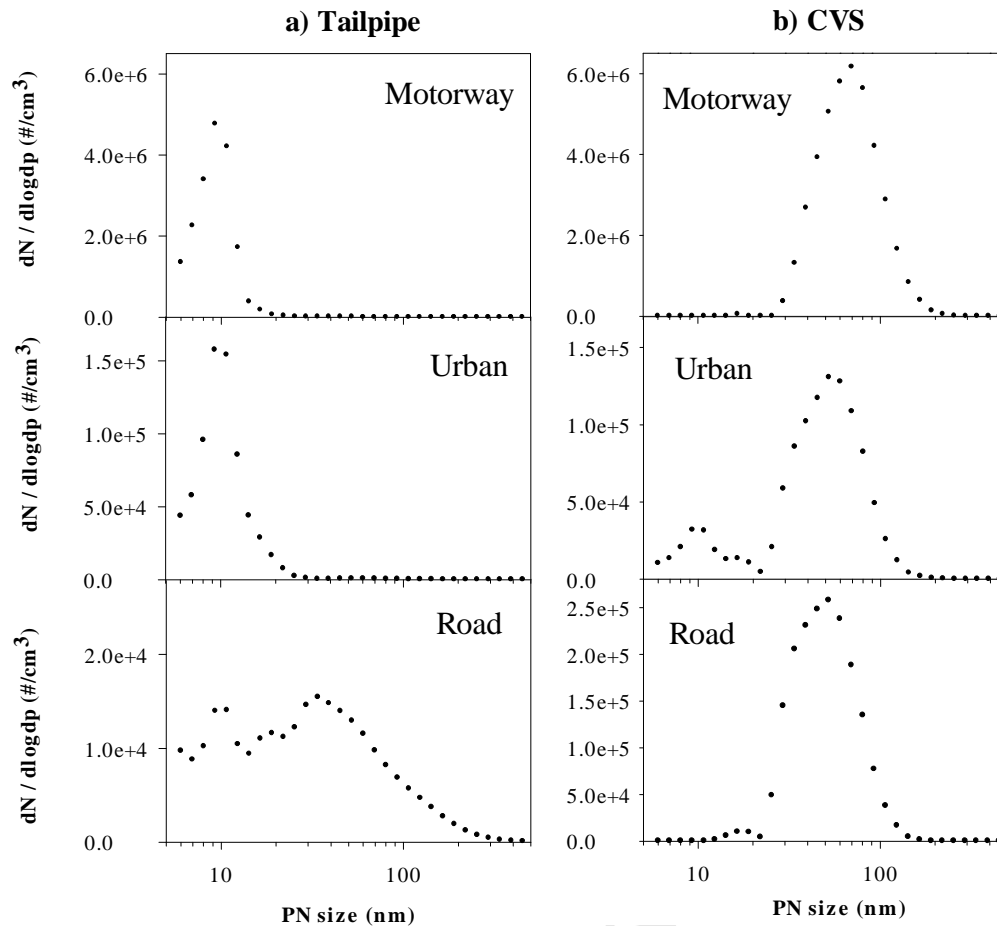
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263 Figure 3. Particle number concentration of the G-DI vehicle during an Artemis motorway driving
264 cycle, sampled: a) after the tailpipe and b) after the CVS. PN size distribution is described on the left
265 Y-axis. The light blue line represents the vehicle speed (km/h) on the right Y-axis.

266 Vehicle accelerations lead to distinct emission peaks. An average of emissions over the whole
267 cycle did not account for these disparities. In order to compare the CVS and exhaust particle size in an
268 acceleration phase (high emission), we choose the highest emission peak for each cycle. Comparisons
269 were made at 500s, 750s and 430s, respectively, for Artemis urban, road and motorway cycles. Figure
270 4 showed the PN size distribution for these three driving conditions after the tailpipe (Figure 4a) and
271 after the CVS (Figure 4b). For motorway, both tailpipe and CVS particle size distribution were
272 unimodal. However, the CVS measurement showed a higher PN concentration with the particle
273 diameter centred at 70 nm comparing to the tailpipe, for which the particle diameter was smaller and
274 centred at 10 nm. For urban, particle size distribution after the tailpipe was similar than the motorway
275 cycle, with a unimodal distribution centred at 10 nm. While after the CVS, the PN size distribution
276 was bimodal with a main mode at 50 nm and a second lower mode at 10 nm. For road, the tailpipe
277 particle size distribution was different than motorway and urban. It showed a bimodal distribution with
278 two main modes at 10 nm and 30 nm, and the CVS particle size distribution was unimodal and centred
279 at 50 nm. However, a similar increase in the particle diameter and concentration was observed in the
280 CVS as two other driving conditions. This observation could be explained by the nucleation,
281 condensation and coagulation phenomena as described by Seinfeld (2016). The increase in particle
282 number highlighted that nucleation process happened in the CVS. Moreover, different precursors in
283 vehicle exhaust, such as semi volatile compounds, sulfuric acid, ammonia, polycyclic aromatic
284 hydrocarbons (PAH), hopanes and steranes, could cause the nucleation and induce an increase in small
285 particle numbers (Louis et al., 2016; Benson et al., 2011; Casati et al., 2007; Virtanen et al., 2006;
286 Burtscher, 2005; Mathis et al., 2005; Zielinska et al., 2004; Bukowiecki et al., 2003). The nucleation
287 phenomenon has already been observed in other exhaust dilution studies by Vouitsis et al. (2009) and
288 Kittelson et al. (1998 and 2000). On the other hand, the particle growth from 10 nm to 50 nm
289 highlighted the condensation and coagulation phenomena that depended on the SVOCs and particle
290 concentration in the exhaust. The SVOCs condensed to the particle surface as function of the partition
291 coefficient between the gas and the particulate phase, which induced a rapid growth of the particles
292 (Zhang et al., 2004). The work of Albriet et al. (2010), with an aerosol computational fluid dynamics
293 model (CFD), confirmed that SVOCs condensation governed the growth of the nanoparticles in the
294 tailpipe plume of vehicles.



295

296 Figure 4. Euro 6 G-DI particle size distribution: a) after tailpipe and b) after CVS for Artemis
297 motorway (at 430s), urban (at 500s) and road (at 750s). Data were measured by a Fast Mobility
298 Particle Sizer Spectrometer (FMPS).

299 For urban, we also observed a particle mode at 10 nm after CVS that could be explained by the
300 lower PN concentration and flow rate in the CVS than motorway (9 m³/min for urban and 11 m³/min
301 for motorway). According to Albriet et al. (2010), turbulence remains a crucial parameter for particle
302 growth. The CVS sampling system turbulence was calculated by the Reynolds number given by
303 Kulkarni (2011). Reynolds number determines if the gas flow was laminar ($Re < 3 \times 10^3$) or turbulent
304 ($Re > 3 \times 10^3$).

305

$$Re = \frac{U \times d}{\nu}$$

306 U: velocity characteristic of the gas (m/s)

307 d: diameter of the pipe (m)

308 ν : kinematic gas viscosity ($\nu = \eta/\rho_g$)

309 For the CVS sampling system, the Reynolds numbers were 5×10^4 , 4×10^4 and 4×10^4 for the
310 motorway, urban and road cycles respectively that were greater than the limit value (3×10^3). The CVS
311 flow was thus a turbulent flow that promoted the phenomena of condensation and coagulation as well
312 as the temporal diffusion of the PN concentration peaks. This turbulence was proportional to the
313 average cycle speed. Low turbulence for the urban condition together with low PN concentration
314 induced low coagulation and condensation rates compared to motorway condition, which could
315 explain the bimodal PN distribution in the CVS.

316 Furthermore, high particle concentration and turbulent flow added to the Brownian motion
317 (random movement of a particle due to collisions with surrounding air particles) could induce
318 turbulent coagulation (Huang et al., 2014; Zhang et al., 2004). Table 4 (Appendix) shows an example
319 of particle coagulation time with different particle sizes and particle concentrations. The coagulation
320 coefficients used in this work were taken from Seinfeld (2016) assuming that the particles were
321 monodisperse taken into account the kinetic corrections and without turbulence. The coagulation half-
322 life time (τ_c) was determined with the following equation:

$$\tau_c = \frac{2}{K \times N_0}$$

323 K: coagulation coefficient for monodisperse aerosols;

324 N_0 : particle concentration

325 For particles having mobility diameter at 10 nm, the coagulation times were 3, 100 and 1000
326 minutes (Table 4, Appendix) for the concentration at $5.5 \times 10^6 \text{ \#/cm}^3$, $1.6 \times 10^5 \text{ \#/cm}^3$ and $1.4 \times 10^4 \text{ \#/cm}^3$,
327 respectively, which represented motorway, urban and road PN emissions (Figure 4). For the particles
328 with diameter at 40 nm, the coagulation times were higher than 1000 minutes for all conditions.
329 According to Albriet et al. (2010) and Grieshop et al. (2009a), coagulation by diffusion is a slow
330 process that takes more than five minutes to occur, which is greater than the CVS residence time (2–10
331 seconds). The turbulence of gas flow in the sampling system could reduce the coagulation time.
332 However, coagulation is known to have a little impact on particle growth in the first seconds after the
333 exhaust (Albriet et al., 2010). These results indicated that the CVS sampling system could induce
334 nucleation and condensation phenomena influencing the particle characteristic and quantification.
335 Particle sampling at the tailpipe could represent a complementary method to better quantify the
336 particle emissions.

337 **4 Conclusion**

338 To investigate the effects of the exhaust dilution on particle emissions, two types of
339 experiments were performed on a chassis dynamometer: 1) dilution and temperature effects on particle
340 emission were investigated with Euro 5 diesel and gasoline vehicles; 2) sampling condition impacts on
341 particle quantification were investigated with Euro 6 diesel and gasoline vehicles. The dilution and
342 temperature effects were studied directly from tailpipe with dilution ratios ranged from 8 to 4000 and
343 dilution temperatures from 50°C to 150°C. Low dilution temperature and low dilution ratios increased
344 the particle number concentration by a factor of 1.4–3. The results highlighted that the low primary
345 dilution ratios induced a significant influence on particle number concentration. At low primary
346 dilution (3–5), the particle emission was 2 times higher than at high primary dilution (12–20). To
347 minimise the bias, the FPS sampling system at tailpipe should be set at high primary dilution and high
348 dilution temperature.

349 In the second experiment, particle emissions from tailpipe were compared to those after the
350 CVS system under similar dilution conditions with two Euro 6 vehicles (gasoline G-DI and diesel
351 DPFcat). Due to the high efficiency of the diesel particulate filter, PN emissions from the Euro 6
352 diesel vehicle were near the detection limit. For Euro 6 G-DI vehicle, CVS PN concentrations were
353 higher than those at the tailpipe by a factor of 6, 80 and 22 for Artemis urban, road and motorway,
354 respectively. The main particle size mode after the tailpipe was centred on 10 nm while, particle size
355 after the CVS was centred at 70 nm for motorway and 50 nm for urban and road driving. The increase
356 in PN concentration and the growth of particle size in the CVS were induced by the nucleation and
357 condensation. These processes could be supported by different semi volatile particle precursors
358 observed in our previous studies and by the turbulent flow in the sampling tunnel (Reynolds numbers
359 = $4-5 \times 10^4$). The coagulation could happen in the CVS because of the high PN concentration and
360 turbulent flow, but it remained a negligible process for the short CVS residence time (2–10s). These
361 results indicated that the CVS sampling system could induce an over-estimation of PN. Particle
362 sampling at tailpipe could represent a complementary method to better quantify the particle emissions.

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516 **Appendix**

517 Table 4. CVS coagulation time for monodisperse particles as function of the PN size and
 518 concentration. The coagulation coefficient takes into account the kinetic corrections but not the
 519 turbulence.

Driving Cycle	PN size (nm)	PN concentration (#/cm ³)	Coagulation coefficient (cm ³ /s)	Coagulation time (s)
Motorway	4	1.3×10^6	1.3×10^{-9}	1.2×10^3
	10	5.5×10^6	1.9×10^{-9}	1.9×10^2
	20	1.5×10^6	2.4×10^{-9}	5.4×10^2
	40	4.8×10^3	2.3×10^{-9}	1.8×10^5
	100	1.6×10^3	1.5×10^{-9}	8.1×10^5
Urban	4	4.4×10^4	1.3×10^{-9}	3.5×10^4
	10	1.6×10^5	1.9×10^{-9}	6.7×10^3
	20	1.7×10^4	2.4×10^{-9}	5.0×10^4
	40	5.2×10^2	2.3×10^{-9}	1.7×10^6
	100	2.5×10^2	1.5×10^{-9}	5.5×10^6
Road	4	9.7×10^3	1.3×10^{-9}	1.6×10^5
	10	1.4×10^4	1.9×10^{-9}	7.5×10^4
	20	1.2×10^4	2.4×10^{-9}	7.2×10^4
	40	1.5×10^4	2.3×10^{-9}	5.9×10^4
	100	5.7×10^3	1.5×10^{-9}	2.4×10^5

520

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546		

Highlights

- Dilution and temperature effects on particle number emission
- Comparison between tailpipe and CVS for particle number emission
- Over-emission of particles from the CVS because of nucleation, condensation and coagulation
- Tailpipe measurement as a complementary method to the CVS for exhaust particle sampling