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Technical note

Prediction of the sound field into high-rise building facades due to its balcony ceiling form

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Abstract

This study presents the acoustic performance off tall building facades closed to roadway due to one of balcony configurations, namely ceiling, with an inclined form in terms of traffic noise reduction. Three inclined angles are tested (5, 10, and 15°) with different balcony depths by using a Pyramid Tracing model developed by A. Farina. The results in terms of A-weighted sound pressure level reduction are expressed in free field into the balcony back wall. The protection level, defined as the difference in noise levels before and after inserting the proposed balcony form, has been used to assess the reduction offered by that configuration. A maximum reduction due to using these forms is obtained at higher floors and at balcony of 2 m depths and more. As a consequence of simulation results, it is found that the prediction of protection levels from 10th to 15th floor can be calculated from an empirical equation.

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Keywords: Environmental noise; Balcony; Pyramid Tracing; Traffic noise

1. Introduction

A balcony is an extension of an internal floor with access by means of windows or doors to an external environment. It provides view and weather protection and is a building familiar element. In particular, it can provide an acoustical protection by means of its elements forms.

Most of the previous studies investigated sound levels on balconies by using experimental models as the work of Mohsen, and Oldham [1], numerical models of Hothersall [2], and Li [3], and the field measurements analysed by May [4], Gilbert

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[5], and Li [3]. These studies carried out a study of traffic noise reduction in the context of treatment to the sound source, in the path between the sound source and the receiver, and at the reception point.

An alternative approach concerning the self-protecting buildings was discussed by Mohsen and Oldham by means of changing balcony depth [1]. Another architectural concept was presented by Hossam El-dien and Woloszyn [6,7], by using an inclined parapet to increase the shielding effect to protect the balcony back wall from the traffic noise nuisance in a free field.

In the present study, we aim to predict the effect of one of the balcony configurations, namely ceiling, on the traffic noise reduction into building facades.

Inclined ceilings with different angles are tested by a 3D numerical model of Pyramid tracing developed by Farina shown in Fig. 1 [8], and in free field conditions.

The results will be expressed in terms of sound pressure level reduction, in A-weighted scale, into the balcony back wall and for a high rise building.

2. Geometric parameters

Acoustic simulation programs (CITYMAP&DISIAPYR) are used to model the outdoor sound propagation environment within the balcony configurations and in

Fig. 1. Schematic representation of the pyramid tracing model (DISIPYR).

three dimensions. This algorithm allows the simulation of outdoor sound propagation with a complex urban form and the evaluation of sound passing through sound insulating panels, taking into account the edge diffraction over the boundaries and the scattering of sound from the edges of finite surfaces, and the surface diffusion coefficient [9].

As shown in Fig. 2, the simulation has been carried out with the following variables:

1. The horizontal projection depth ($W = 1, 2$, and 3 m).
2. The balcony's ceiling inclined angle ($\varnothing = 5, 10$, and 15°).

And we have fixed the following parameters:

1. Sound source (infinite).
2. Distance to road (8.00 m).
3. Front wall height (1.00 m).
4. Balcony's length (5.00 m).
5. Number of floors (17 floors).

3. Prediction methodology

In three dimensions, the model is equivalent to an infinite coherent line source parallel to the building facade. All the surfaces in the model are initially defined as specular surfaces (concrete with absorption coefficient 0.07 at 1 KHz). The acoustic performance of the balcony ceiling with an inclined shape has been assessed by

Fig. 2. Geometric parameters.

Fig. 3. Schematic representation of the reception surface and its image before and after changing balcony ceiling form.

means of a numerical simulation. Three inclined angles have been tested (5, 10, and 15°).

The basic concept of inclining the balcony ceiling is to decrease the power of reflection and diffuse energy components by changing the direction of reflected rays away from the openings located at the balcony back wall as shown in Fig. 3. In the case of the inclined ceiling, we can notice that the protected surface over the balcony back wall increases by comparison of the protected surface gained from the classical form as a consequence of ceiling reflected area.

Firstly, the sound pressure reference level (SPL_{ref}), was calculated over the balcony back wall with an inclined angle θ equal to 0° through 3000 reception points over the back wall.

The protection level is defined as the difference in noise level at an assessment point with and without changing ceiling inclined angle, and is calculated according to the following equation:

$$L_p = SPL_{ref} - SPL_{\theta} \quad \text{dB(A)}$$

where SPL_{ref} is the reference level and SPL_{θ} is the sound pressure level calculated for a given ceiling angle at the same point.

4. Simulation results

4.1. Balcony with 1 m depth

In this part of investigation, the acoustic performance of inclined ceiling form and for a closed balcony with 1 m depth is simulated. Fig. 4 shows the average reduction of sound level obtained by three types of inclined ceiling forms. It was found that the protection gained at the lower levels is not noticeable as a result of the direct component effect. The effect of these forms can be observed from the fourth level, and

reaches to its maximum value at the 16th level (Fig. 4), where protection gain is 2 dB (A).

Generally, the performance of 10 and 15° angles are more effective than 5° angle, and the gain obtained is from 0.5 to 2 dB (A) in terms of sound level reduction.

Through studying each floor level, we can notice that the increase of protection values from 10th to 15th floor can be ordered (Fig. 5). It was found that the predicted protection values for these configurations can be calculated according to the following exponential equation:

$$L_p = ((2.40 + 0.2(n_i - n_o))\tan\theta + 0.20)e^{-1.85h/\tan\theta} \text{ dB(A)}, 15 \geq n_i \geq 10 \quad (1)$$

where n_i is floor number, $n_o = 10$, h is the height above the balcony floor, and θ is ceiling inclined angle.

Fig. 4. Average of protection offered by inclined ceilings of a balcony with 1 m depth.

Fig. 5. Balcony cross section shows the maximum effect of the inclined ceiling, for a balcony with 1 m depth, and with an angle equal to 5° (a), and the classical ceiling form (b) at the 16th floor.

4.2. Balcony with 2 m depth

By using the same method, the acoustic performance of inclined ceilings for a closed balcony with 2 m depth was tested. Figs. 6 and 7 shows the average of sound level reduction obtained for three angles for that configuration. The average reduction obtained at the lower levels is negligible by comparison of that obtained from 1 m balcony depth, while it increases at the higher floors. The reduction is negative

Fig. 6. Protection values provided at the centre of the balcony back wall with 1 m depth, numerical simulation (Dots), and empirical equation (Lines) at the 15th floors and for angles $\theta = 5, 10$, and 15° .

Fig. 7. Average of protection offered by inclined ceilings of a balcony with 2 m depth.

from the 1st to 5th floor while it increases from the 6th floor and reaches to its maximum value at the 13th floor (Fig. 8). Generally that form allows more benefits than that of 1 m balcony depth. Ten and 15° angles are more effective at lower levels, while 5° angle has a greater effect at higher levels. Furthermore, this configuration allows a protection level from 0.5 to 4 dB (A).

Similar to 1 m balcony depth, it is observed that protection values from the 10th floor to the 15th floor regularly increase except for the 13th floor (maximum value), and the 14th floor for the angle $\emptyset$ equal to 10°.

We found that protection predicted values for these floors and for these configurations can be calculated according to the following exponential equation:

Fig. 8. Balcony cross section shows the maximum effect of the inclined ceiling, for a balcony with 2 m depth, and with an angle equal to 5° (a), and the classical ceiling form (b) at the 13th floor, and at the reception surface.

Fig. 9. Protection values provided at the centre of the balcony back wall with 2 m depth, numerical simulation (Dots), and empirical equation (Lines) at the 15th floors and for angles $\emptyset = 5, 10$, and 15°.

$$L_p = ((0.25 + 0.1(n_i - n_o))\tan\theta + 0.40)e^{-1.85h/\tan\theta} \text{dB(A)}, \quad 15 \geq n_i \geq 10. \quad (2)$$

where n_i is floor number, $n_o = 10$, h is the height above the balcony floor, and θ is ceiling inclined angle (Fig. 9).

4.3. Balcony with 3 m depth

Acoustic performance of inclined ceilings for a closed balcony with 3 m depth provides more reduction at lower levels than that obtained from the previous configurations and also for higher levels. The average reduction obtained at the lower floors is more effective than the other two previous forms, and also for the higher floors. Reduction values are negative at the first two floors and begin to increase from the 3rd floor to reach its maximum value at the 11th floor (Figs. 10 and 11). In

Fig. 10. Average of protection offered by inclined ceilings of a balcony with 3 m depth.

Fig. 11. Balcony cross section shows the maximum effect of the inclined ceiling, for a balcony with 3 m depth, and with an angle equal to 5° (a), and the classical ceiling form (b) at the 11th floor.

Fig. 12. The protection values offered at the centre of the balcony back wall with 3 m depth, numerical simulation (Dots), and empirical equation (Lines) at the 15th floors and for angles $\Theta = 5^\circ$, 10° , and 15° .

general, the average protection gained from that configuration is from 0.5 to 6 dB (A).

In accordance with the previous forms, the protection values increase from the 10th floor to the 15th floor except for the 11th floor (maximum value) and the 12th floor. They can be calculated according to the following exponential equation:

$$L_p = ((-0.75 + 0.05(n_i - n_o))\tan\Theta + 0.60)e^{-1.85h/\tan\Theta} \text{dB(A)}, 15 \geq n_i \geq 10. \quad (3)$$

except for the 12th floor where it can be calculated using the following equation:

$$L_p = ((-1.75 + 0.05(n_i - n_o))\tan\Theta + 0.60)e^{-1.85h/\tan\Theta} \text{dB(A)}, n_i = 12.$$

where n_i is floor number, $n_o = 10$, h is the height above the balcony floor, and Θ is ceiling inclined angle (Fig. 12).

For these configurations, Eqs. (1), (2), and (3) lead to predict the protection level L_{pw} as a relation with the balcony depth can be calculated as the following relation:

$$L_{pw} = ((4.45 - 2.075w + 0.4^{-0.70w}(n_i - n_o))\tan\Theta + 0.40)e^{-1.85h/\tan\Theta} \text{dB(A)}$$

where w is balcony depth, n_i is floor number ($15 \geq n_i \geq 10$), $n_o = 10$, h is the height above the balcony floor, and Θ is ceiling inclined angle.

5. Conclusion

The Pyramid Tracing model was used to predict the performance of a balcony ceiling with inclined form. The average noise reduction provided by that configuration with reflective surface was about 0.5–6 db (A). This investigation showed that the inclined ceiling form can dominate the sound reflected from its bottom surface with changing the reflected ray direction away from a balcony back wall.

Reduction benefits are in direct proportion to both floor level and balcony depth. On the other hand, they are inversely proportional to the ceiling inclined angle at higher floors, and are directly proportional to the ceiling inclined angles at lower floors. Generally, the predicted results showed that a balcony ceiling form can be employed to protect weak points on the facades, for high rise buildings, against traffic noise propagation. In addition, results of this investigation will hopefully provide practical information to the architect who wishes to design facades which can be described as self protected with respect to the external acoustic environment. It will be seen that a slight modification of existing building envelope design can provide additional sound protection without compromising other environmental requirements. Further work will be undertaken to validate these results by means of experimental study.

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