Needle-type GMR Sensor to Estimate the Magnetic Properties of Diluted Ferrofluid for Biomedicine Application

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Abstract:
This paper proposes a needle-type giant magnetoresistance (GMR) sensor for very low magnetic fluid weight density of ferrofluid estimation. The magnetic fluids or ferrofluids due to their biocompatibility are used for various applications in medicine such as cancer treatment, magnetic resonance imagining (MRI), cell separation and also to detect the bacteria. The high sensitivity of GMR sensor gives us to accurately measure the magnetic properties of ferrofluid in a weak magnetic field. The results were obtained by GMR sensor are compared by theoretical results and showing that the GMR sensor has a good ability for biofluid magnetic characterization.

Keywords:
Magnetic fluid, GMR sensor, demagnetizing factor, weight density, relative permeability, susceptibility.

1. Introduction
In several applications such as in medical care, environmental issues and chemicals analysis methods need to sense small amount of specific molecules. Using magnetic micro or nanoparticles to mark, detect, move or destroy living cells or molecules has recently gained a lot of interest [1]. Therefore, a large effort is lead toward developing compatible magnetic micro-nanoparticles as well as designing new high sensitivity magnetic sensors [2]. Giant magnetoresistance (GMR) sensors are particularly well suited for biomedical projects because they provide high sensitivity and detection capability at the micro [3] or nanoscale [4].
Ferrofluids or magnetic liquids involve extremely nanoparticle size of magnetic materials (iron, nickel or cobalt), they currently have a great importance in the mechanical or electronic military technology as well as in the various domains of medical applications such as magnetic resonance imaging (MRI) diagnostic, tissue repair, cellular therapy, magnetofection, cell separation, magnetic drug-targeting and hyperthermia treatment [5, 6].

The typical and most common bio-applications of magnetic fluid are described below:

- Magnetic cell separation is widely useful and very inexpensive method for separating different types of cells. The magnetic beads using in this method represent a mix of a polymer magnetic iron oxide in the range from 10 nm to 10 µm [7].
- Magnetic drug targeting is a transportation of drugs to target tissue place with aid and use of an external magnetic field toward a tumor [8].
- Magnetic resonance imaging (MRI) is a diagnostic and very informative method which is widely used in medicine to create a detailed picture of internal organs. It allows diagnosing soft tissue, brain, joints, bones and detecting focal lesions of central nervous system (CNS), liver lesions or tumors. Moreover,
MRI is a rather safe technique if compared with computerized tomography (CT) or X-ray. In MRI diagnostic the ferrofluid is sometimes injected into a vein (intravenous injection) in order to enhance the contrast of MRI imaging [9].

In hyperthermia treatment the tumor tissue targeting with magnetic nanoparticles, and placing under an AC magnetic field to heating the tumor tissue, where in the temperature of the body or body part reaches 42°C and more [10, 11].

Magnetic fluids are a unique system that combines the properties of paramagnetic materials and the ability to control thermal and optical characteristics of the magnetic field. Each particle of magnetic fluid is coated with a thin layer of protective membrane that prevents the adhesion of the particles. Ferrofluids do not exhibit ferromagnetic properties because it does not retain the remanent magnetization after that the external magnetic field has been shut off. In fact, liquids show features of “superparamagnetism” because of the lack of coupling between nanoparticles. Therefore, an external magnetic field orientates the magnetic moments of particles almost independently. The alignment of the magnetized particles along the magnetic field leads to a change in physical properties (magnetic, optical and rheological) of the system. In addition, under the influence of an external magnetic field, hydrostatic pressure in the liquid changes so that any non-magnetic body is pushed out of it whereas the magnetic particles moves towards the highest field strength liquid region. All this together allows controlling the behavior and physical properties of magnetic fluids and devices containing magnetic fluid.

The needle-type magnetoeresistance (GMR) sensors exist in different models depending on the number of sensing element and also their dimensions. Until now, they have been used for different investigations such as in printed circuit board (PCB) inspection checking [12], measurement of nerve pulse current [13] etc. The aim of the present research is to demonstrate the efficiency of a type of GMR sensor which has a good potential to estimate the magnetic fluid weight density (\(D_w\)) with low concentration as low as 2.5%.

2. Materials and method

2.1 Needle-Type GMR Sensor

The GMR sensor consists of two principal parts. The first one is a needle’s sensor and the second one is a Wheatstone bridge circuit.

The needle length is 17 mm with a cross section 300 µm×300 µm. It can be inserted into the cavity midpoint of ferrofluid. The needle of GMR sensor is made of hard materials such as Aluminum Titanium Carbide (AlTiC) and sintered materials of Aluminum Oxide (Al₂O₃) and Titanium Carbide (TiC).

The needle of this sensor has four GMR sensing elements with 75 µm×40 µm dimensions for each sensing element. The first sensing element is located at the tip and the rest of sensing elements are placed at the end of the needle. All sensing elements are connected in a Wheatstone bridge configuration. Figure 1 shows the GMR sensor architecture.
Figure 1. Schematic of the GMR needle type sensor and sensor’s Wheatstone bridge configuration. The Wheatstone bridge configuration of the GMR sensor permits to measure voltage variations induced by magnetic field with removing DC component of GMR polarization, and allows to measure magnetic flux density inside and outside of fluid filed container of magnetic liquid. The GMR sensor is connected to a DC power supply (±6 V) via an interface card. Interface card of the GMR sensor permits to limit the current. Furthermore, we should point out that for this type of the GMR sensor the maximum current being 5 mA.

As we mentioned previously, the GMR sensor has four sensing elements, the first sensing element at the top of sensor is in contact with the magnetic liquid in the container (inside magnetic flux density $B_1$) and the other sensing elements are embedded to sense magnetic flux density ($B_0$) at the outside of the ferrofluid’s cavity. The magnetic fluid weight density at fluid cavity can be calculated taking into account the difference between the outside and the inside magnetic flux density respectively $B_0$, and $B_1$.

Figure 2. Magnetic flux density distribution inside and outside of ellipsoidal cavity.
The magnetic flux distribution inside and outside of ellipsoidal cavity is presented in Figure 2. Considering the fluid cavity having μ_r > 1 placed under uniform magnetic flux density and assuming the outside relative permeability equals to 1. As expected, the magnetic flux density is more concentrated at the ellipsoidal cavity.

2.2 Theoretical derivation

When considering a large number of magnetic nanoparticles embedded in a magnetic liquid, it is possible to estimate the total relative permeability (μ_r) of the magnetic fluid using the following formula:

\[
μ_r = 1 + 4D_V \approx \frac{1 + 4D_W}{γ_f} \quad (D_w << 1)
\]  

Where D_V is magnetic fluid volume density, D_W is magnetic fluid weight density (mgFe/ml) and γ_f = 5.17, is the specific gravity of magnetic bead.

The relationship between changes of magnetic flux density δ and magnetic fluid weight density D_W can be described by the following expression:

\[
δ = \frac{(B_1 - B_0)}{B_0} = \frac{C_d (1 - N) D_W}{h_3 γ_f} \quad (D_w << 1)
\]  

Where B_0 is the outside magnetic flux density, B_1 is the magnetic flux density inside the cavity, C_d is a coefficient which is theoretically 4 and practically in range between 3-4. N is the demagnetizing factor, in spherical shaped cavities (aspect ratio S = height/diameter being equal to unity), and h_3 is space factor of cluster. The demagnetizing factor of a cavity depends on the aspect ratio of a cavity, for example, for the thin and long cavity the demagnetizing factor is zero (N=0, S=∞) [14].

The relationship of relative susceptibility (χ*) and the ratio of magnetic field by measurement of GMR sensor leads to the following expression:

\[
δ = \frac{(B_1 - B_0)}{B_0} = (1 - N) χ^* \quad (χ^* << 1)
\]  

The measured relationship between magnetic fluid volume density (D_V) and the magnetic fluid weight density (D_W) measured as a weight of ferrite per volume (mgFe/ml) are related by the following expression:

\[
D_W = \frac{γ_f D_V}{(1 - D_V) + γ_f D_V}
\]  

From equation (4) the magnetic fluid volume density (D_V) may be determined as:

\[
D_V = \frac{1}{1 + \left( \frac{1}{D_W} - 1 \right) γ_f}
\]  

2.3 Experimental Method and Setup

2.3.1 Preparation of Ferrofluids with Different Concentrations

To create the magnetic fluid by different weight density, pure magnetic fluid-D or fluid MAG-D was used. Fluid MAG-D is a specific magnetic resonance imaging (MRI) contrast that contains an aqueous dispersion of a large
number of superparamagnetic iron oxide nanoparticles \((\text{Fe}_3\text{O}_4 = \text{Fe}^{II}(\text{Fe}^{III})_2\text{O}_4)\) with hydrodynamic diameters of 100–200nm [15]. The magnetic fluid-D is produced by Chemicell Company and it can be injected as an intravenous injection (IV), to reduce the time dissemination and immediate imaging of the body’s organs. Moreover, it can be used in hyperthermia cancer therapy. The product information of the fluid MAG-D is shown in Table 1.

Table 1. The specification of the fluid MAG-D [15].

<table>
<thead>
<tr>
<th>Volume</th>
<th>1.5ml</th>
</tr>
</thead>
<tbody>
<tr>
<td>Size of particles</td>
<td>100nm</td>
</tr>
<tr>
<td>Number of Particles</td>
<td>1.8x10^{15}/g</td>
</tr>
<tr>
<td>Weight of Volume</td>
<td>25mg/ml</td>
</tr>
<tr>
<td>Density of each particle (Magnetite)</td>
<td>5.17g/cm³</td>
</tr>
<tr>
<td>Magnetic core</td>
<td>Magnetite (Fe₃O₄)</td>
</tr>
<tr>
<td>Color</td>
<td>Brown</td>
</tr>
<tr>
<td>Application</td>
<td>MRI-diagnostics, Cell separation, Magnetic Drug-Targeting</td>
</tr>
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</table>

Experiments were performed to prepare different magnetic fluids with several weight densities \(D_W\). In this experiment the fluid MAG-D by particles size 200 nm is diluted by distilled water to achieve several magnetic fluids with weight density at respectively 0.23%, 0.35%, 0.62%, 1.24% and 2.45% as shown in Figure 3. The weight density and volume density of pure fluid MAG-D and different concentration can be determined from the equations 4 and 5. Furthermore, to dilute the concentration is used the micro pipette to reduce the amount of mixing errors.

In our experiments, the magnetic fluid is inserted in a “cylindrical cavity” with ellipsoidal shape for the surface base. We assume that the magnetic nanoparticles are uniformly distributed in the fluid. Soft matter or solids can show ferromagnetic, paramagnetic, diamagnetic behaviors and in ferrofluids exhibit superparamagnetic behavior according to their magnetic susceptibility [5].

![Figure 3. Top-view cavities of five different weight densities of magnetic fluid.](image)

Next, the 450 μl of magnetic fluid were poured by micro pipette to cylindrical shape cavity (fabricated with Polydimethylsiloxane or PDMS) of dimensions 8x8 mm, after the five ferrofluids were placed respectively at the midpoint of the Helmholtz coil, where the magnetic field is more uniform.
2.3.2 Measurement Setup of GMR Sensor

The experimental setup is presented in Figure 4. Experiments were performed by needle-type GMR sensor to characterize the four samples (weight densities varying from 2.45%, 1.24%, 0.62%, 0.35 to 0.23%) of magnetic fluid. The sensor needle was precautionary placed inside the ferrofluid at the center of the container. After the measurement for each diluted ferrofluid, the needle of GMR sensor was cleaned by distilled water and soft sponge in order to reduce the percentage of testing errors.

Moreover, to provide protection of needle against any shock, we have used a specific displacement system. This system provides us possibility to control carefully the needle of the GMR sensor for two positions, injecting and cleaning. It is controlled by controller PCON-CG-42PI that allows us to backup 512 preset positions by a software. It is supported with 220V AC to 24V DC convertor via a protection relays.

The GMR sensor probe is connected to DC power source (±6 V) through an interface card. The interface card of the sensor permits to control and protect the GMR sensor to prevent excessive electrical current passing through the GMR sensor. The output signal is amplified approximately 1200 times (62 dB) by use of a circuit amplifier (Analog Devices AD 620). The preamplifier AD 620 is fed by another power supply (±9 V). The differential signal Vout-Vref of the whole sensor and its conditioning electronics was supplied to a multifunction HF2IS Impedance Spectroscope. Data of the GMR sensor (values of Vrms and phase) were collected by interface program of the HF2IS Impedance Spectroscope.

![Figure 4. Experimental and measurement setup.](image)

Helmholtz coil used in our experiment consists of two circular coils with 12 turns, each coil being of 0.52 meters diameter which is also the distance between coil to coil radiuses. It should be noted that the magnetic field range for measurement by GMR sensor is within tens of nT to few mT. The Helmholtz coil was amplified by a variable gain amplifier through two serial transformers. By using output signal generators of HF2IS Impedance Spectroscope, we can directly generate the supply system of Helmholtz coil without presenting waveform generator that leads to more system integration.

The experimental frequency of exciting field of the Helmholtz coil is 75 Hz, the input current of the coil is 180 mA, exciting field (H) is 147.77 (A/m) and magnetic flux density is 185.7 µT.
2.3.3 Measurement by Vibrating Sample Magnetometers (VSM)

Commercial vibrating sample magnetometer (VSM model 3374-140 GMW Associates) was used in order to measure macroscopically the in-field magnetization behavior of the ferrofluids. Several magnetic fluids were prepared from pure fluid MAG-D and placed into the VSM measurement setup (see Figure 5).

![Figure 5. VSM measurement setup where the container of ferrofluid is placed at the center of VSM](image)

Figure 5. VSM measurement setup where the container of ferrofluid is placed at the center of VSM

Figure 6 shows typical “magnetization versus magnetic field amplitude” loop obtained for a magnetic field applied perpendicularly to the length of the cylindrical cavity (Fig. 2 is as a top view of the cavity). No hysteresis neither remanent magnetization is observed in the measured loop, this loop is typical of paramagnetic or “superparamagnetic” materials. If each magnetic nanoparticle is considered as one magnetic moment, the completely random organization at zero field leads to zero magnetization. Thus under an external magnetic field, the magnetic moments tend to align and a non-null magnetization appears that reaches. As the magnetic fluid is diluted with distilled water, the overall magnetization at saturation decreases but the magnetization at saturation per magnetic fluid dose stays constant. This observation confirms that the magnetization originates from non-interacting particles.

![Figure 6. Magnetic hysteresis loop of pure fluid MAG-D and its different concentrations obtained by VSM device.](image)

3. Results

The experimental analysis obtained by GMR sensor was calculated for each ferrofluid’s concentration and also was compared with theoretical results according to equations (1, 3) for confirmation. The results of relationships
between relative permeability ($\mu_r$) and susceptibility ($\chi$) depending on weight density obtained by needle type GMR sensor and theoretical are presented in Figure 7 and Figure 8. We can also observe from the results that $\mu_r$ and $\chi$ are linear and proportional to $D_W$.

**Figure 7.** Experimental results of the relative permeability ($\mu_r$) as a function of different weight densities $D_w$ (%) and comparison with the theoretical results.

**Figure 8.** Comparison of the experimental and theoretical results of the susceptibility variations ($\chi$) as a function of the weight density $D_w$ (%).

The GMR needle probe was used to estimate the magnetic properties ($\mu_r$, $\chi$) of the magnetic fluid, by measuring the applied magnetic flux density outside ($B_0=185.7 \mu T$) and inside ($B_1$) of cavities.

**Figure 9.** Magnetic fluid density variations calculated for magnetic flux density ($\delta$) versus weight density ($D_w$) of ferrofluids.
According to the Equation (2), the experimental results were performed to estimate the magnetic flux density ($\delta$) by increasing weight density ($D_W$) with shape ratio of cavity ($S = 1$ and $N= 0.333$ for ellipsoidal shape), and the result obtained by the GMR sensor is presented in Figure 9.

4. Discussion of GMR Sensor’s Concept and its Performance

The characterization of the GMR sensor was determined by creating the uniform magnetic flux density for only one sensing GMR element. The sensor’s sensitivity is approximately equal to $8.5 \mu V/\mu T$. It permits to accurately estimate the magnetic properties of magnetic fluid at low concentration and to improve the measurement in very low magnetic field due to its high sensitivity and more easy portability compared to similar methods such as VSM or SQUID. Another interest is its ability to perform the time real and imaginary analysis in a sweep frequency range.

Magneticspectroscopy of ferrofluids plays an important role in a medicine as noted before. For example, in hyperthermia treatment the amount of required heat of ferrofluid inside a tumor depends on the ferrofluid’s weight density ($D_W$). After injection $D_W$ decreases because of the intra-tumor dilution of the ferrofluid. Thus it is important to check $D_W$ in order to reach a successful treatment. The GMR sensor opens interesting ways to develop biosensors for medical applications of magnetic fluids.

5. Conclusions

In this study a magnetic sensor technology based on giant magnetoresistance has been presented. It was demonstrated that the GMR sensor is useful and convenient for biomedical applications in order to characterize magnetic properties of low concentrated magnetic fluids in a weak magnetic field.

The experimental results achieved in this paper showed a proportional relationship between relative permeability, susceptibility and magnetic flux density (in the approximately range $0.02-0.0016$ for the susceptibility) as a function of weight density for small volume ($S=1$, $N=0.333$).

Moreover, for triangulation of validity and reliability of GMR sensor’s results we did the same analysis using as well the theoretical one. The results obtained by GMR sensor compared to those obtained by theoretical are close and both results confirm each other.
References


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