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Soft 3D acoustic metamaterial with negative index

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Introductory paragraph:

Many efforts have been devoted to the design and the achievement of negative-refractive-index metamaterials since the 2000s¹⁻⁸. One of the current challenges in that field is to extend beyond electromagnetism by realizing three-dimensional (3D) media with negative acoustic indices⁹. We report a new class of locally resonant ultrasonic metafluids consisting of a concentrated suspension of macroporous microbeads engineered using soft-matter techniques. The propagation of Gaussian pulses within these random distributions of “ultra-slow” Mie resonators is investigated through *in situ* ultrasonic experiments. The acoustic index is shown to be negative over broad frequency bandwidths, depending on the volume fraction of the microbeads as predicted by multiple-scattering calculations. These soft 3D acoustic metamaterials open the way for key applications such as sub-wavelength imaging and transformation acoustics, which require the production of acoustic devices with negative or zero-valued indices.

Main text:

Unlike periodic structures, *i.e.*, photonic crystals for light² or phononic crystals for sound³, in which negative refraction is a consequence of band-folding effects, the negative index of a metamaterial originates from low-frequency resonances of sub-wavelength particles. A negative refractive index in electromagnetism was first experimentally verified at microwave frequencies⁴; since then, other experimental demonstrations of negative-index metamaterials have been reported in the near-infrared domain^{5,6} and at optical wavelengths⁷. However, the metamaterial concept applies not only to electromagnetism⁸ but also to different fields such as acoustics⁹. Since the first experimental realization of “locally resonant sonic materials¹⁰”, negative-acoustic-index metamaterials have been achieved for only the audible domain through the use of two-dimensional solid structures consisting of periodic arrays of interspaced membranes and side holes¹¹ or arrays of Helmholtz and rod-spring resonators¹². Coiling up space has also proven to be an effective method of providing acoustic metamaterials with extreme constitutive parameters^{13,14}. Possible future applications such as perfect acoustic lenses, by analogy with John Pendry’s perfect electromagnetic lens¹⁵, call for three-dimensional negative-acoustic-index metamaterials, which have not yet been achieved¹⁶.

Unlike the mechanical engineering techniques that are usually used to machine 1D¹⁷ or 2D¹⁸ solid structures, soft-matter techniques are very promising for the fabrication of metamaterials because they should yield 3D locally-resonant metafluids, or so-called soft acoustic metamaterials¹⁹, which present the following advantages: i) macroscopic isotropy, unlike the most general class of acoustic metafluids with anisotropic inertia^{20,21}; ii) broad versatility, as microfluidics²² allows the up-scaled production of micro-resonators with controlled sizes, shapes

and compositions; iii) potential tunability, as soft inclusions can be either deformed or oriented under external stimuli²³; and iv) facile shaping and molding, as the host matrix is fluid.

A unique method of achieving 3D negative-acoustic-index metamaterials is to benefit from strong low-frequency Mie resonances (monopolar and dipolar) of “ultra-slow” inclusions²⁴. However, no dense homogeneous material possesses a sufficiently low sound speed to exhibit such a feature, not even the so-called “soft silicone rubbers²⁵”. By contrast, the use of *porous* soft silicone rubbers should be more promising because the sound speed in porous media is very low²⁶, with the latter depending on the ratio between the elastic moduli and mass density. Indeed, the large volume of air cavities present in porous materials causes them to be very soft (or highly compressible), thereby allowing these materials to exhibit very low elastic moduli while maintaining relatively high mass densities because of their solid skeletons. Particles composed of such “ultra-slow” materials ($v_l \approx 100$ m/s) randomly dispersed in water ($v_0 \approx 1500$ m/s) should exhibit an extremely large monopolar resonance, like air bubbles²⁷, thereby causing the suspension to exhibit a negative effective bulk modulus B . These fairly dense particles should also exhibit a strong dipolar resonance, producing a negative effective mass density ρ in an overlapping frequency region. If they are considered as perfect (non-dissipative) media, such “double-negative acoustic metamaterials” are expected to have negative acoustic indices²⁴.

Such a straightforward analysis in terms of negative constitutive parameters may be inappropriate for a dissipative medium with a negative refractive index²⁸. In both electromagnetism and acoustics, the refractive index n is complex-valued because it is defined as the ratio of the **complex-valued** wavenumber k ($= \omega/v + j\alpha$) in the metamaterial to that in a reference medium k_0 ($= \omega/v_0 + j\alpha_0$), where v denotes the phase velocity, α represents the attenuation coefficient, and ω is the angular frequency. For a non-dissipative reference medium

($\alpha_0 = 0$), the refractive index $n = v_0/v + j(\alpha v_0/\omega)$ is often referred to as its real part ($= v_0/v$). By convention, its imaginary part is taken to be positive ($\alpha > 0$), thus defining the forward direction along which the wave energy flows. Conventional dissipative media or positive-index materials support only forward wave motions ($v > 0$). Metamaterials, however, can sustain backward waves ($v < 0$) in the spectral vicinity of the particle resonances; such materials are referred to as negative-index materials¹.

In this study, we exploited strong low-frequency Mie resonances of sub-wavelength macroporous silicone rubber microbeads to achieve negative-index metamaterials in the ultrasonic domain. We produced particles with a mean radius $\langle a \rangle$ of 160 μm and a size dispersion of approximately 25% (Fig. 1a and b) by generating high-internal-phase emulsion droplets in a simple microfluidic device²⁹. These macroporous microbeads, with a porosity of approximately 40%, were then randomly dispersed in a water-based gel matrix, *i.e.*, a Bingham fluid³⁰ that behaves acoustically like water ($v_0 \approx 1500$ m/s), thus forming a concentrated suspension of “ultra-slow” particles with a volume fraction Φ_0 of approximately 20%. Because the macroporous microbeads are closed (Fig. 1c), they are stable over time (a few days), unlike air bubbles (a few minutes), which are very sensitive to numerous undesirable effects such as Oswald ripening or dissolution in the host matrix³¹.

To determine the acoustic refractive index n of the investigated macroporous-particle suspensions, we measured the angular phase shifts of Gaussian pulses propagating through varying thicknesses in direct-acoustical-contact measurements (Fig. 1e). Ultrasonic pulses, with central frequencies f_0 ranging from 50 kHz to 500 kHz, were emitted and detected using a pair of large broadband ultrasonic transducers (transmitter/receiver) with a diameter of 30 mm. Because the size of our macroporous particles is approximately 300 μm , *i.e.*, 10 times smaller than the

smallest incident wavelength used in our experiments (3 mm at 500 kHz for water), our microbeads can be considered to be sub-wavelength resonators, as sought for metamaterials¹. When the propagation distance z was varied from 1.0 mm to 1.5 mm, the transmitted temporal signals shifted on the time-delay axis, allowing us to directly infer the phase velocity v and the acoustic index $n (= v_0/v)$.

Indeed, such *in situ* acoustical measurements can avoid additional phase delays caused by the interfaces, as reported in electromagnetism⁶. Because the strong resonant scattering induces high attenuation in such a random medium, we detect only the ballistic coherent pulse³², which propagates from the transmitter to the receiver. Therefore, pulses reflected on the transducer surfaces are not propagated, thus avoiding spurious phase delays caused by interferences between the successive echoes (see the Supplementary Information).

For all operating frequencies f_0 , the amplitude of the transmitted pulses decreases when the propagation distance z is increased in such a passive medium, as illustrated at 140 kHz (Fig. 2a). However, the temporal shift of the pulse oscillations, which contains information regarding the phase velocity v , depends on the frequency f_0 . Note that in our conditions, *i.e.* by investigating “thin” samples, we are able to infer unambiguously the phase velocity because the measured phase delays ($\sim 0.1 \mu\text{s}$) are much smaller than the time period of the transmitted signals ($> 1 \mu\text{s}$). Since all the oscillations shift as a whole, we focus our attention on the center of the pulses, denoted by t_{phase} and for which the amplitude is zero, as depicted in Fig. 2b to d.

The forward shift of t_{phase} observed at 110 kHz (Fig. 2b) indicates a positive phase velocity (or positive acoustic index, Fig. 2e). By contrast, the backward shift of t_{phase} at 170 kHz (Fig. 2d) reveals a negative phase velocity (or negative acoustic index, Fig. 2g). For the intermediate

frequency $f_0 = 140$ kHz, the transmitted pulses are not shifted on the time-delay axis (Fig. 2c), indicating “infinite” phase velocities (or zero acoustic index, Fig. 2f).

Additionally, we obtained the phase-velocity and acoustic-index spectra over a broad frequency range [50–500 kHz] from the angular-phase measurements performed on the fast Fourier transforms (FFTs) of the temporal signals recorded for two different propagation distances ($z = 1.0$ mm and 1.5 mm). The phase velocity v and the acoustic index $n (= v_0/v)$ were observed to be negative between 140 kHz and 275 kHz (see the black curves in Fig. 3a and b).

The initial sample ($\Phi_0 \approx 20\%$) was then diluted to produce another sample with $\Phi_1 \approx 15\%$, which resulted in a clear reduction of the frequency width of the negative bands (red curves in Fig. 3a and b). When the volume fraction was drastically lowered ($\Phi_2 \approx 0.2\%$), the negative features disappeared (green curves in Fig. 3a and b), giving way to classical dispersion ($v > 0$), as previously observed in bubbly media³¹.

Finally, we compared our acoustical measurements to theoretical predictions produced through multiple-scattering modeling revealing fairly good qualitative agreement (Fig. 3a to d). To obtain the theoretical acoustic index n , we calculated the effective wavenumber k of our samples using the Waterman-Truell formula³³ (see the Supplementary Information), often used for concentrated random media ($\Phi \approx 10\%$). The values of the parameters for the porous silicone rubber that were used for the calculations (the velocity and attenuation coefficient for both longitudinal and shear waves) were measured independently on large monolithic cylindrical samples (30 mm in diameter and 3 mm in thickness) of the same material as the microbeads. The material parameters used for the calculations are $\rho_l = 600$ kg/m³, $v_L = 80$ m/s, $\alpha_L = 60$ Np/mm/MHz^{1.5} (for longitudinal waves), and $v_T = 40$ m/s, $\alpha_T = 200$ Np/mm/MHz^{1.5} (for shear waves) for the porous silicone rubber and $\rho_0 = 1000$ kg/m³, $v_0 = 1500$ m/s for the water-based gel matrix.

Through direct-pulse-propagation experiments on soft acoustic metamaterials, we confirmed that the phase velocity could be negative over a broad range of ultrasonic frequency bandwidths, thus demonstrating a three-dimensional negative-acoustic-index metamaterial. Our approach based on the use of soft-matter techniques means that these metafluids can be produced on a large scale, paving the way toward the production of acoustic devices with negative or zero-valued indices, as required for key applications such as sub-wavelength imaging and transformation acoustics.

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Contributions:

T.B., O.M.M., J.L., O.P. and C.A. designed the project. A.M. synthesized the macroporous soft silicone rubber microbeads with the help of K.Z. Formulation aspects were supervised by O.M.M. A.M. set up the microfluidics on the advice of J.L. T.B. and B.M. conducted the acoustical measurements and performed the calculations under the guidance of C.A. and O.P. for the theoretical aspects. T.B. wrote the paper in collaboration with C.A., O.P., J.L. and O.M.M.

Competing financial interests:

The authors declare that they have no competing financial interests.

Figure 1 Soft 3D acoustic metamaterials composed of “ultra-slow” Mie resonators.

a, Optical microscopy image of macroporous silicone rubber microbeads embedded in a water-based gel matrix. **b**, Corresponding histogram showing the microbead size distribution. The mean radius $\langle a \rangle$ is 160 μm , and the standard deviation σ of the distribution is 25%, as deduced from a Gaussian fit (solid line). The particle porosity is approximately 40%. **c** and **d**, SEM images of both the surface and core of a microbead. **e**, Photograph of the acoustical experimental setup for the *in situ* phase-velocity measurements. The propagation distance z between the pair of large broadband ultrasonic transducers (emitter/receiver) could be varied precisely because the receiver was mounted on a z -axis motorized linear stage.

Figure 2 Phase delays of the transmitted signals, as a function of propagation distance.

a, Examples of typical measured ballistic coherent pulses ($f_0 = 140$ kHz) transmitted through a concentrated suspension of macroporous silicone rubber microbeads ($\Phi_0 \approx 20\%$, $\langle a \rangle = 160$ μm , $\sigma = 25\%$) for five propagation distances z ($= 1.0, 1.1, 1.2, 1.3, 1.4$ and 1.5 mm). The time t_{phase} refers to the center of the pulses for which the amplitude is zero. **b-d**, Zoomed-in views of the oscillations around t_{phase} for $f_0 = 110, 140$ and 170 kHz. **e-g**, Values of the time t_{phase} as a function of the propagation distance z , yielding experimental values for the phase velocity v ($= \delta z / \delta t_{\text{phase}}$) and acoustic index n ($= v_0 / v$) from linear regressions for $f_0 = 110, 140$ and 170 kHz.

Figure 3 Comparisons between acoustical experiments and theoretical predictions.

a, Experimental phase velocities v extracted from fast Fourier transforms performed on ultrasonic Gaussian pulses with central frequencies f_0 ranging from 50 kHz to 500 kHz. **b**, Experimental acoustic indices $n (= v_0/v)$ deduced from the above phase-velocity spectra (**a**) given the knowledge of the phase velocity of the host matrix ($v_0 \approx 1500$ m/s). **c-d**, Predicted phase velocities and acoustic indices calculated in the framework of multiple scattering (see the Waterman-Truett formula given in the Supplementary Information). The volume fractions are approximately $\Phi_0 \approx 20\%$ (black lines), $\Phi_1 \approx 15\%$ (red lines) and $\Phi_2 \approx 0.2\%$ (green lines).