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XPS and AES studies of UHTC ZrB$_2$–SiC–Si$_3$N$_4$ treated with solar energy

E. Beche,$^a$* M. Balat-Pichelin,$^b$ V. Fland,$^c$ J. Esvan,$^d$ T. Duguet,$^d$ D. Sciti$^e$ and D. Alfano$^f$

The microstructure of ultra-high-temperature ceramics based on the ZrB$_2$–SiC composition and a sintering additive (Si$_3$N$_4$) was investigated using XPS and AES techniques. These ZrB$_2$–SiC–Si$_3$N$_4$ materials were treated in air plasma at high temperature ($T > 1750$ K) in the MESOX facility developed at the PROMES-CNRS laboratory (Moyen d’Essai Solaire d’Oxydation for the measurement of atomic oxygen recombination coefficients). The surfaces were characterized before and after the air plasma treatment. Surface modifications were observed and induced by the oxidation process. The elementary composition was determined using AES and XPS. Core level spectroscopy (XPS) was used to determine the atomic composition and the nature of the chemical bonds from the Zr 3d$_{3/2,5/2}$, Si 2p$_{1/2,3/2}$, O 1s and C 1s photoelectron peaks. The microstructural analyses revealed the presence of oxide layers: Silica and zirconia compounds were detected at temperatures near 1800 K, and a zirconia compound was mainly detected above 2200 K.

Keywords: XPS; AES; ultra-high-temperature ceramics; zirconium diboride; silicon carbide

Introduction

A ground test simulation in atmospheric re-entry conditions is necessary to characterize and select base materials for a thermal protection system (TPS). The thermophysical and microstructural properties are key parameters for the eligibility of ultra-high-temperature ceramic (UHTC) materials in hot structure manufacturing.

The base materials for future spaceplane-like, re-entry vehicles must resist temperatures approaching 2500 K and evaporation, erosion and oxidation in the harsh re-entry environment. These requirements are above the single-use temperature limit of current TPS materials (SiC-coated C–C composites).\cite{1,2}

Ceramic compounds based on metal borides, such as zirconium diboride (ZrB$_2$) and hafnium diboride (HfB$_2$), are defined as UHTCs because of their high melting temperatures, which are greater than 3300 K.\cite{3,4} Zrb$_2$ materials have a lower theoretical density (6.09 g/cm$^3$), which classifies them as the most promising candidates for TPSs. The presence of SiC fibers increases the mechanical properties (matrix stability) of the ZrB$_2$–SiC material. The value of the fracture toughness in ZrB$_2$ ceramics is approximately 3.8 MPa.m$^{1/2}$ and increases to approximately 5.3 MPa.m$^{1/2}$ in ZrB$_2$ ceramic + SiC fibers. Several authors\cite{5-8} have demonstrated that the incorporation of SiC provides significant enhancements to the oxidation resistance; a small amount of the formed borosilicate compound limits the oxygen diffusion. The incorporation of Si$_3$N$_4$ in the ZrB$_2$ matrix improves the sintering temperatures; the sintering temperature decreases from 2090 K (30 MPa, 20 min) to 1950 K (30 MPa, 10 min). During an oxidation process in air ($T = 1500$ K) of a ZrB$_2$–SiC composite, several authors\cite{9} reported that the thickness of the oxide layer decreases with an increasing amount of SiC from 0% to 50% (vol.) in the reference material.

Understanding the chemical environment of the surface and in the bulk is necessary to explain the surface properties and the phenomena regulating the surface oxidation of these UHTC materials. These materials are considered an attractive class of TPS ceramic compounds for aerospace applications such as sharp leading edges and the hot structures of slender-shaped re-entry vehicles. ZrB$_2$ UHTCs are processed using hot pressing. Complex-shaped components can then be obtained using either conventional diamond machining or electrical discharge machining (EDM), which is possible because of the electrical conductivity of the borides (10$^6$ S/cm). The surface finish can be better controlled using conventional machining. However, EDM is effective and can be used to machine UHTC pieces into complex-shaped components such as nose-cones or sharp leading edges.\cite{7}

In the last decade, the oxidation of ZrB$_2$–SiC UHTC materials (near 2000 K) using an XPS technique was studied in less than ten publications. No surface study using AES for oxidized ZrB$_2$–SiC UHTC materials was performed. The initial oxidation of ZrB$_2$ surfaces at high temperature (1600 K) was characterized by Aizawa et al.\cite{10} The authors present the AES spectra (Zr MNN, B KLL and O KLL) of a clean ZrB$_2$ and an exposed ZrB$_2$ surface under O$_2$ gas at 1600 K. Rayner et al.\cite{11} studied the evolution of the Zr compounds.

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Experimental section

Ceramic compounds were prepared using the following commercial powders: SiC chopped fibers (Hi Nicalon, COI Ceramics Inc., Magna, Utah, USA) and ZrB2 Grade B (H.C. Starck, Germany). For the sintering aids, Si3N4 Baysind (Bayer, Germany) were used. The following composition of sample A was produced (vol%): ZrB2 + 15% SiC + 5% Si3N4.

The UHTC compounds were obtained by hot pressing of powders and SiC fibers.[7] The powders and fiber mixtures were ball milled for 24 h. After solvent removal, the powder mixture was uniaxially pressed at 15 MPa to form 45-mm diameter green pellets. Before sintering, the pellets underwent a debonding cycle at 773 K to remove organic species. The pellets were subsequently hot pressed using a load of 40–50 MPa. Because the reinforcing fibers tend to react with the matrix and secondary phases during the high-temperature thermal treatment, the sintering temperature should be kept as low as possible.

The UHTC materials were heated in a MESOX solar reactor (6 kW). This apparatus is described in detail in previous papers.[7,12,13] Concentrated solar energy was used to heat the sample placed at the center of the microwave discharge (300 W); i.e. the air plasma conditions were kept constant, and only solar heating was transformed to increase the sample temperature for the measurement of the recombination coefficient.[13] The degree of oxygen dissociation was high (70–80%). The heating of the sample was independent from the plasma. The heating began at 1000 K and increased every 10 min by a step of 200 K until reaching the final temperatures (T = 1760 K, sample A1, and T = 2200 K, sample A2) for 1 h. Control of the temperatures was possible with an opening shutter. The temperature measurement was performed using a monochromatic (5 μm) optical pyrometer considering the normal spectral emissivity. Moreover, the pyrometer, the CaF2 window and the mirror were calibrated in our laboratory on a blackbody.

AES analysis was performed using a Thermoelectron MICROLAB 350 device (CIRIMAT-ENSIACET, France). The Auger electron emission spectra were recorded using electron gun (5 kV). The analyzed area was ~1 μm². The spectrometer energy calibration was made using the Si KLL2,3 (1615.8 ± 0.1 eV) and the Si LVV (92.9 ± 0.1 eV) Auger transition from a Si(100) wafer sample. AES spectra were recorded in direct N(E). The kinetic energy (KE) scale was established by referencing the C KVV value of adventitious carbon (284.8 eV).[16] The photoelectron peaks were calibrated in our laboratory on a blackbody.

The atomic compositions of the sputtered samples A, A1 and A2 were measured based on the O 1s, Zr 3d, B 1s, Si 2p, C 1s and N 1s core level photoelectrons peaks (Table 1). For sample A, the presence of residual oxide layers (sample A) and carbon species is explained by the finishing treatment; the electric discharge machining (EDM) leads to the presence of zirconia, silica and a high amount of carbon on the sample.

The assignment of the O 1s, Zr 3d, B 1s, Si 2p, C 1s and N 1s components from the XPS spectra collected for the UHTC compounds A, A1 and A2 is summarized in Table 2. For the heated samples A1 and A2, the atmospheric contamination components (C–C/C–H and/or C–O bonds) of the C 1s photoelectron peaks are not shown in Table 2.

The Zr 3d spectra collected for sample A (Fig. 1a) and samples A1 and A2 (Figs 1b and 1c) have five or two components, respectively. The ratio of the peak intensities, R = (I 3d5/2/I 3d3/2), was fixed at 1.50 ± 0.05. The spin–orbit energy difference between the 3d5/2 and the 3d3/2 components is approximately 2.38 ± 0.02 eV. The Zr 3d5/2 and Zr 3d3/2 peak positions located at 179.2, 181.6 ± 0.1 eV are attributed to the Zr–B bonds in a ZrB2 compound.[7,8,10,17]

The Zr 3d5/2 and Zr 3d3/2 peak positions located at approximately 182.6 and 185.1 ± 0.1 eV are characteristic of the O–Zr bonds in oxide compounds.[7,8,17] The Zr atoms are in Zr4+ environments (Zr4+ state). For the treated samples A1 and A2, no Zr–O bonds were detected.

The B 1s spectrum (Fig. 1a, sample A) located at 187.8 ± 0.1 eV was attributed to B–Zr bonds (ZrB2 compound).[7,8,10,17] No B element was detected for the tested samples A1 and A2.

<table>
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The aim of this work is to investigate the microstructure of reference and treated UHTC materials based on the ZrB2–SiC composition with a sintering additive (Si3N4) using XPS and AES. Qualitative and quantitative analysis was conducted using core level spectroscopy (XPS).

Results and discussion

The atomic compositions of the sputtered samples A, A1 and A2 were measured based on the O 1s, Zr 3d, B 1s, Si 2p, C 1s and N 1s core level photoelectrons peaks (Table 1). For sample A, the presence of residual oxide layers (sample A) and carbon species is explained by the finishing treatment; the electric discharge machining (EDM) leads to the presence of zirconia, silica and a high amount of carbon on the sample.

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The B 1s spectrum (Fig. 1a, sample A) located at 187.8 ± 0.1 eV was attributed to B–Zr bonds (ZrB2 compound).[7,8,10,17] No B element was detected for the tested samples A1 and A2.

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The three components (103.1, 101.7 and 100.5 ± 0.1 eV) of the Si 2p spectrum (sample A, Fig. 2a) were attributed to Si–O, Si–Na and Si–C bonds, respectively.[10,19–21] No Si–N and Si–Cbonds were detected on the surfaces of samples A1 and A2 (Figs 2b and 2c).

The O 1s spectra (Figs 3a–c) were curve fitted with two components. The component located at 530.4 ± 0.1 eV is attributed to O–Zr bonds.[7–17] These bonds are larger for sample A2 than those for sample A1. The shift between the O–Si and O–C component is less than 0.3 eV. Thus, in the peak-fitting process, only one component (532.4 ± 0.1 eV) was used to identify these two types of bonds (O–C and O–Si).[10,19] For samples A1 and A2 (Figs 3b and 3c), this component is mainly attributed to O–Si bonds (Table 2). However, for sample A (Fig. 3a), this component is mainly attributed to O–C bonds (Table 2).

The C–Si bonds (283.0 ± 0.1 eV) [4,5,9–11] were only detected on surface A (not shown).

The N 1s spectrum (A) was mainly curve fitted with one component (not shown). The main component located at 397.6 ± 0.1 eV was attributed to N–Si bonds [4][Si3N4 compound]. N–Si bonds were only detected from the N 1s photoelectron peaks of sample A.

Several points of a line scan (AES) were taken on the clean surface of sample A. Two types of field, pt1 and pt2, were identified (Fig. 4b).

The XPS results reveal the microstructure of a ZrB2–SiC–Si3N4 compound.

For sample A, the residual oxide layers and carbon species were not completely removed during the sputtering process. An induced surface roughness is revealed in SEM micrographs.

Several components (103.1, 101.7 and 100.5 ± 0.1 eV) of the Si 2p spectrum (sample A, Fig. 2a) were attributed to Si–O, Si–N and Si–C bonds, respectively.[10,19–21] No Si–N and Si–C bonds were detected on the surfaces of samples A1 and A2 (Figs 2b and 2c).

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The C–Si bonds (283.0 ± 0.1 eV) [4,5,9–11] were only detected on surface A (not shown).

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For sample A, the residual oxide layers and carbon species were not completely removed during the sputtering process. An induced surface roughness is revealed in SEM micrographs.

The XPS results reveal the microstructure of a ZrB2–SiC–Si3N4 compound.

For samples A1 and A2, the ZrB2, the SiC and the Si3N4 phases detected on the reference surface A were fully oxidized. These results indicate that two oxide phases, SiO2 and ZrO2, were formed in the heated initial surface. Higher temperatures were correlated with lower amounts of SiO2 and higher amounts of ZrO2: When the temperature increased to 1760 K, silica was embedded in zirconia for the same heating time. The presence of Zr–O–Si bonds in ZrSiO4 induced shifts of the Si 2p, Zr 3d and O 1s spectra: The components attributed to mixed Zr–O–Si bonds in ZrSiO4 compounds are detected at 101.8, 183 and 531.3 eV, respectively.[11] No (ZrO2) x(SiO2)1–x mixed alloys with Zr–O–Si bonds were observed from the Zr 3d, Si 2p and O 1s spectra.

Several points of a line scan (AES) were taken on the clean surface of sample A. Two types of field, pt1 and pt2, were identified (Fig. 4b).
The main Auger transitions, Zr M4,5N1N2,3, Zr M4,5N2,3N2,3 and Zr M4,5N2,3N4,5 (pt1, Fig. 4a), are located at 92.7, 117.7 and 147.5 ± 0.2 eV. The peak at 176.7 ± 0.2 eV is mainly assigned to the B KL2,3L2,3 transition (pt1, Fig. 4a) and a weak overlap of a Zr Auger transition (low kinetic energy (KE) side).

The Si L2,3VV and C KVV Auger transitions (pt2, Fig. 4a) are located at 86.5 and 266.0 ± 0.2 eV, respectively. These positions are characteristic of a SiC compound. Weak Zr MNN and B KL2,3L2,3 Auger transitions were also observed.

The spectra pt1 and pt2 (sample A) are characteristic of a ZrB2 ceramic and SiC fiber, respectively.

Several points of a line scan (AES) were taken on the clean surface of samples A2 and A1. For sample A2, one characteristic point, pt3, was identified (Fig. 5b). For sample A1, two characteristic points, pt4 and pt5, were identified (Fig. 5c).

Figure 5a presents the AES spectra collected from the clean surfaces of samples A2 and A1. The spectra (A2, pt3) were collected on the oxidized ZrB2 ceramic. The spectra (A1, pt5) were collected on an oxidized SiC fiber.

The position of the Zr MNN Auger transitions were all shifted to the low KE side (−5 eV) in comparison with the KE positions measured for sample A (pt1, Fig. 4). This result indicates the presence...
For sample A1, the oxidized SiC fibers located at the surface are partially covered by zirconia, which diffuses during the heat treatment. The oxidized SiC fibers (silica compound) are embedded in a zirconia layer.

No oxidized SiC fiber was observed on the surface of sample A2. The holes and valleys correspond to the initial position of the SiC fibers, which were burnt during the heat treatment (T = 2200 K).

Conclusions

XPS and AES analyses revealed significant results for the tested surfaces at various temperatures. For the non-tested sample, the surface layer was characteristic of SiC fibers embedded in ZrB$_2$ matrix.

The tested ZrB$_2$–SiC–Si$_3$N$_4$ materials were fully oxidized at 1760 and 2200 K. Higher temperatures were correlated with lower amounts of silica. At 1760 K, the surface layer was composed of a matrix of zirconia and oxidized fibers (silica compound). When the temperature increased to 2200 K, all the SiC fibers were burnt. The surface layer is a zirconia compound that contains holes and valleys corresponding to the initial SiC fibers.

This study highlights the extreme complexity of UHTC oxidation behavior. Knowledge about the chemical environment on the surface and in the bulk is necessary to explain the surface properties and phenomena regulating the surface oxidation of these UHTC materials.

Acknowledgements

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