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Vidal-Gilbert

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# Desorption-induced shear failure of coal bed seams during gas depletion

D. N. Espinoza<sup>a,b</sup>, J. -M. Pereira<sup>a</sup>, M. Vandamme<sup>a</sup>, P. Dangla<sup>a</sup>, S. Vidal-Gilbert<sup>c</sup>

<sup>a</sup>*Université Paris-Est, Laboratoire Navier, (UMR 8205), ENPC, CNRS, IFSTTAR*

<sup>b</sup>*The University of Texas at Austin, Department of Petroleum and Geosystems Engineering*

<sup>c</sup>*Total S.A., Unconventional Gas Resources*

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## Abstract

The recovery of natural gas from coal bed seams is usually accompanied by a significant increase of permeability induced by coal matrix shrinkage and stress relaxation upon gas desorption. This advantageous increase in permeability may be impaired sometimes by mechanical failure of the reservoir rock and ensuing production of coal fines. Near-wellbore stress concentration and reduction of lateral stresses are known to promote shear failure during depletion in oil and gas reservoir formations. Yet, conventional analyses have shown limited success in predicting coal failure, since other chemo-physical mechanisms may be responsible in enhancing the conditions towards mechanical failure in the coal bed reservoir rock. We show a set of triaxial experiments involving gas desorption from coal cores under zero-lateral strain condition (radial stress measured and controlled) and constant total vertical stress meant to simulate the stress path during production far from the wellbore. CO<sub>2</sub> is used a surrogate fluid for CH<sub>4</sub>. The experimental data indicates that desorption can significantly help reduce lateral stress (and

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9 increasing deviatoric stress) until shear failure occurs. The results suggest  
10 that depletion-induced shear failure is much more likely to occur in coal  
11 seams than in conventional non-sorbing reservoir rocks. The adsorption-  
12 mechanical coupling turns out to be a key phenomenon in the process. Nu-  
13 merical simulations at the representative elementary volume scale adopting  
14 a double-porosity poromechanical model support the experimental findings  
15 and permit calculating a critical gas pressure for shear failure to happen.  
16 This emergent phenomenon is comparable to the outcome of other situations  
17 such as mineral dissolution or thermal contraction, where shrinkage relaxes  
18 lateral stress and acts as an intensifying driver for promoting shear failure  
19 within the reservoir rock. Coupled numerical simulation is needed to include  
20 near-wellbore effects and validate our findings with actual field observations.  
21 A thorough understanding of the coupled response of coal seams is necessary  
22 to enhance reservoir management and mitigate the effects of coal failure on  
23 fines production.  
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37 *Keywords:* fines production, CBM, adsorption, swelling, nanoporosity,  
38 faulting, chemo-mechanical coupling  
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## 42 43 **1. Introduction**

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2 Currently, natural gas accounts for roughly 20% of the World's energy  
supply (IEA, 2013). Coal bed methane constitutes an important domestic  
source of natural gas in several countries, namely Australia, USA, Canada  
and China (EIA, 2013). Moreover, production of coal bed methane is ex-  
pected to increase throughout the world in the near future as more reservoirs  
are discovered and new technology enables enhanced production.

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8 Various characteristics make coal beds a unique geomaterial, showing  
9 poromechanical properties notably different from other reservoir rocks. First,  
10 coal seams are naturally fractured reservoirs. Diagenetic processes lead to  
11 opening mode fractures predominantly oriented perpendicularly to the bed-  
12 ding plane, called cleats (Laubach et al., 1998). Cleats compose most of the  
13 macroporosity, where fluid flow occurs by advection (Mazumder et al., 2006;  
14 Pan and Connell, 2007). Second, the coal solid skeleton is constituted by a  
15 microporous disordered organic continuum, termed coal matrix. Micropores  
16 and mesopores sized in the order of  $10^{-9}$  to  $10^{-8}$  m compose the coal mi-  
17 croporosity. The coal matrix is capable of adsorbing various gases, including  
18 carbon dioxide  $\text{CO}_2$ , methane  $\text{CH}_4$ , and nitrogen  $\text{N}_2$ ; adsorption leads to  
19 coal matrix volumetric swelling in the order of a few percents (Reucroft and  
20 Sethuraman, 1987; Ceglarska-Stefanska and Czaplinski, 1993; Levine, 1996;  
21 Mazumder et al., 2006; Pan and Connell, 2007; Pini, 2009). Conversely,  
22 desorption leads to coal matrix shrinkage.

23 Bottom-hole depressurization induces gas production from fractures and  
24 desorption from the coal matrix during the production phase. Desorption-  
25 induced shrinkage has an important effect on coal seam permeability (Palmer  
26 and Mansoori, 1998; Pan and Connell, 2012). Shrinkage favors the opening  
27 of open-mode fractures with a concomitant increase in permeability. How-  
28 ever, large increases in permeability during depletion have sometimes been  
29 observed to be followed by a sudden drop of permeability (Figure 1), usually  
30 accompanied by the production of coal fines (Moore et al., 2011; Okotie and  
31 Moore, 2010). One cause of fines production (also responsible for sand pro-  
32 duction in conventional reservoir) is increased stress anisotropy and shearing

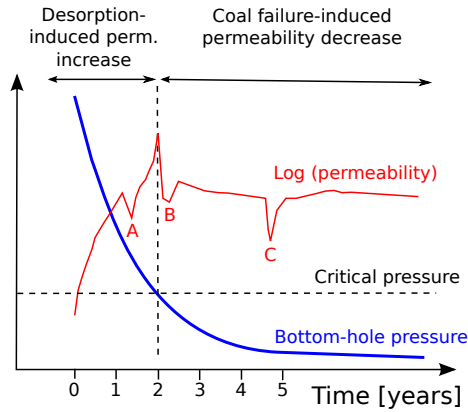


Figure 1: Schematic signature of reservoir response and coal failure during depletion as a function of time: bottom-hole pressure and permeability signals. Notice that sudden permeability reductions (indicated A, B and C) take place as bottom-hole pressure is reduced. The permeability drops are associated with coal failure events. The last permeability drop (C) is recovered after wellbore clean-up operations only. Adapted from field experimental data by Moore et al. (2011).

around uncased wells or perforations due to loss of radial support.

Reservoir depletion is known to induce changes in effective stresses in the reservoir rock far from the wellbore, that can sometimes lead to shear failure and fault reactivation within the reservoir. Depletion promotes zero-lateral strain loading condition in laterally extensive reservoirs (condition commonly known as uniaxial strain/compression in Petroleum Engineering and Structural Geology or oedometric condition in Geotechnical Engineering— Figure 2). The change in stresses upon depletion in conventional reservoirs is well predicted by poroelasticity, shear-failure (induced normal faulting), or a combination of both (Teufel et al., 1991; Segall and Fitzgerald, 1998; Gouly, 2003). Under zero-lateral strain condition, the ratio between the change of total lateral (horizontal) stress  $\Delta\sigma_h$  and the change of reservoir pressure  $\Delta p$

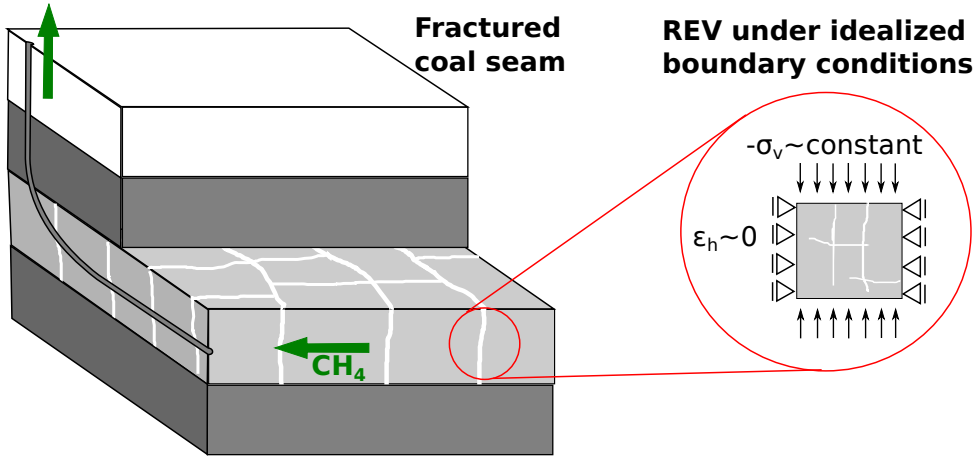


Figure 2: Schematic representation of a coal seam intercepted by a horizontal well and of a representative elementary volume (REV) far from near-wellbore effects. Laterally extensive coal seams follow zero-lateral strain compression far from the wellbore.

is equal to  $\Delta\sigma_h/\Delta p = 2/3$  for a poroelastic response with Poisson's ratio  $\nu = 0.25$  and Biot's coefficient  $\alpha = 1$  or for shear failure with friction coefficient  $\mu = 0.58$ . Recent experimental work shows a reduction of 9.4 MPa of lateral stress upon drawdown of  $\text{CH}_4$  gas pressure from 6.2 to 0.3 MPa while keeping zero-lateral (radial) strain condition in a cylindrical coal core (Mitra et al., 2012). This result indicates a ratio  $\Delta\sigma_h/\Delta p \sim 1.57$ . Theoretical  $\Delta\sigma_h/\Delta p$  values predicted by poroelasticity cannot be higher than 1 for any combination of Poisson's ratio and Biot's coefficient in conventional rocks (Zoback, 2013), which suggests that conventional poroelasticity cannot fully explain the behavior of coal seams.

Given the double porosity of coal seams (micro and macroporosity described previously) and the well known adsorption-induced swelling of the coal matrix, the change in lateral stress in coal seams upon depletion is expected to have some particularities with respect to conventional reservoirs.

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59 Recent work from the authors aims at predicting adsorption-induced strains  
10 and stresses in coal seams within a poromechanical framework including rig-  
11 orously adsorption phenomena (Brochard et al., 2012; Nikoosokhan et al.,  
12 2012, 2014; Espinoza et al., 2013, 2014). Our experimental and modeling re-  
13 sults indicate that adsorption can generate significant stresses in the order of  
14 tens of MPa at typical reservoir pressures. Hence, it should not be surprising  
15 that desorption at zero-lateral strain can significantly affect the reduction  
16 of lateral stress during depletion at a  $\Delta\sigma_h/\Delta p$  rate much greater than the  
17 one due solely to poroelastic effects in macropores predicted by conventional  
18 poroelasticity.  
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28 The objective of this study is to assess the reduction of lateral stresses in  
29 coal seams during depletion and gas desorption by replicating the depletion  
30 pressure-stress path in the laboratory using CO<sub>2</sub> as a surrogate fluid for  
31 CH<sub>4</sub>. We aim at understanding the underlying phenomena which lead to coal  
32 failure and production of coal fines at the scale of a representative elementary  
33 volume far from near-wellbore effects.  
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## 41 **2. Materials and Methods**

### 42 *2.1. Coal characterization and triaxial testing*

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46 We test coal originary from South Africa (Vitrinite reflectance 0.57% – sub-  
47 bituminous A/high volatile C bituminous by ASTM D 388). A set of cores  
48 38 mm diameter and 2:1 slenderness drilled perpendicularly to the bedding  
49 plane serve as experimental specimens. The bulk density of cores ranges  
50 from 1318 to 1356 kg/m<sup>3</sup>. The specimen Helium porosity varies from 11-to-  
51 13%. Core testing takes place in a triaxial cell connected to syringe pumps  
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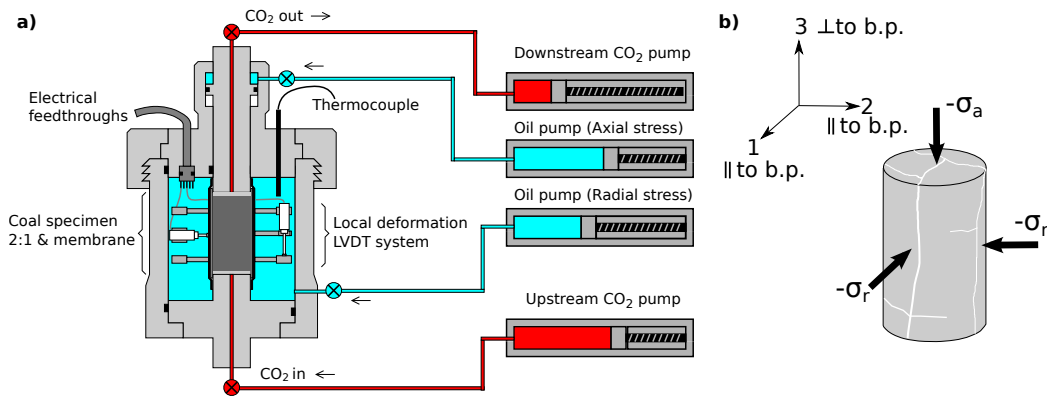


Figure 3: a) Experimental triaxial device; main characteristics include: maximum radial stress 40 MPa, maximum axial stress 60 MPa, measurement of local strains through LVDTs, temperature control and ability to handle pressurized pore-fluids. b) Orientation of the specimen respect to the bedding plane (b.p.).

to control stresses and pore-fluid pressure. The system is able to (1) measure specimen axial and radial deformations and (2) control independently axial and radial stresses to apply isotropic or anisotropic state of stresses (including zero-lateral strain condition). Figure 3 shows a schematic representation of the triaxial cell and its main features.

## 2.2. Determination of shear strength

We tested the shear strength of coal cores in dry conditions (without adsorbed gas) under unconfined and confined triaxial conditions. The triaxial cell imposes a deviatoric loading by applying a change in axial strain with time at a given constant confinement. The axial strain rate is fixed to a constant value equal to  $3 \cdot 10^{-4} \text{ min}^{-1}$ . Rigorously, the shear strength should be tested with sorbed gas, as sorption may reduce shear strength (See section 4.1 Fluid-specific effects).



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96 *2.3. Desorption test procedure*

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11 We aim at simulating in the laboratory the pressure-stress path of a  
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13 98 block of coal subjected to depressurization and depletion. Hence, the follow-  
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15 99 ing pressure-stress path is required: (1) recreation of in-situ initial state of  
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17 100 stresses and seam pressure (requires adsorbed gas in thermodynamical equi-  
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19 101 librium with gas in the cleats), (2) imposition of a pressure drawdown to  
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21 102 extract gas from the fractures and coal micropores, with simultaneous ad-  
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23 103 justment of lateral stresses to keep zero-lateral strain condition, while the  
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25 104 total vertical stress remains constant (constant overburden – see Figure 2).

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27 105 The experimental procedure to achieve the pressure-stress path described  
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29 106 above consists of the following steps:

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31 107 1. Increase confining stresses 1 to 2 MPa above the objective fluid injec-  
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33 108 tion pressure  $p_{ci}$  at which the core will be exposed. The resulting low  
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35 109 effective stress will facilitate quick advective gas flow through fractures  
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37 110 (since fracture permeability is highly sensitive to effective stress) and  
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39 111 reduce equilibration time in the next step.
- 40  
41 112 2. Inject CO<sub>2</sub> at constant confining stress, let the specimen swell and equi-  
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43 113 librate for  $\sim 7$  days. Swelling strains help us evaluate thermodynamical  
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45 114 equilibrium, such that when they reach steady-state values we consider  
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47 115 equilibrium has been attained.
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49 116 3. Increase effective stresses to the initial stress conditions representing  
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51 117 the current in-situ stresses in the formation. Let the specimen equi-  
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53 118 brate again for at least 1 day.
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55 119 4. Apply a drawdown pressure by imposing constant pressures at the two  
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57 120 loading caps  $p_{DS} < p_{US} < p_{ci}$  ( $p_{DS}$ : pressure downstream,  $p_{US}$ : pres-

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10 sure upstream).

11 5. The pressure drawdown induces axial and radial deformations. The  
12 radial deformation is canceled periodically (to keep variations smaller  
13 than  $\Delta\varepsilon_r < 3 \cdot 10^{-4}$ ) by reducing the total radial stress in order to  
14 maintain near zero-lateral strain condition. No action is taken on the  
15 axial direction, so that total axial stress remains constant.  
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21 All tests are performed under stress, pressure, and temperature relevant  
22 to in-situ coal bed conditions. Instead of  $\text{CH}_4$ , we utilize  $\text{CO}_2$  as the pore  
23 fluid. The applicability of our  $\text{CO}_2$  laboratory results to  $\text{CH}_4$  desorption are  
24 discussed in Section 4.1.  
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### 30 **3. Experimental results**

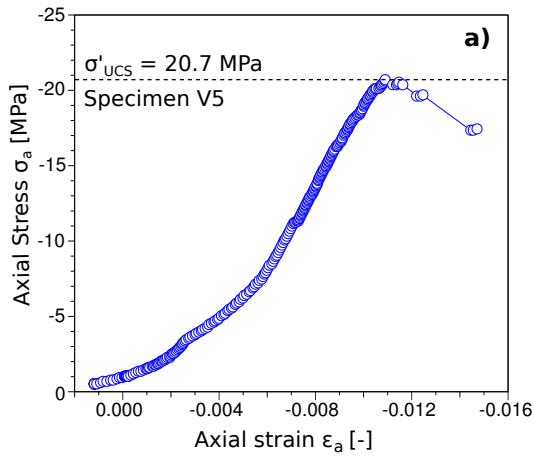
#### 31 *3.1. Dry testing – Shear failure envelope*

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33 Table 1 lists all shear strength experiments. Figure 4 shows an exam-  
34 ple of a coal core failed under simple compression. Specimens V4, V5, and  
35 V6 were tested under unconfined conditions while specimens V7 and V9  
36 were tested under confined triaxial conditions. Figure 5 shows the sum-  
37 mary of shear strength results with Mohr circles at failure. The shear  
38 strength increased non-linearly with added confining stress. The friction  
39 angle estimated from the orientation of shear fractures in failed specimens  
40 is  $\phi \sim 40^\circ$  to  $50^\circ$ . The best-fitting parameters for the Hoek-Brown criterion  
41  $\sigma'_1 = \sigma'_3 + \sigma'_{UCS} \sqrt{m\sigma'_3/\sigma'_{UCS} + s}$  in terms of Terzaghi's effective stress defined  
42 as  $\sigma' = -(\sigma + p_c)$  are  $s=1$ ,  $\sigma'_{UCS}=22.05$  MPa and  $m= 38.4$ . Pressure  $p_c$  is  
43 zero an all experiments listed in Table 1.  
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Table 1: List of shear strength experiments on dry specimens. (\*) Acquisition error – stress signal lost.

Specimen	Terzaghi's effective radial stress $\sigma'_r$ [MPa]	Terzaghi's effective axial stress $\sigma'_a$ [MPa]
V4	0.0	>17*
V5	0.0	20.7
V6	0.0	22.2
V7	3.0	55.0
V9	1.5	48.0



Coal failed under simple compression

Figure 4: Unconfined compression test: a) stress-strain curve, and b) picture of sheared coal as extruded out from the testing sleeve; fragments are ordered from left to right according to their size.

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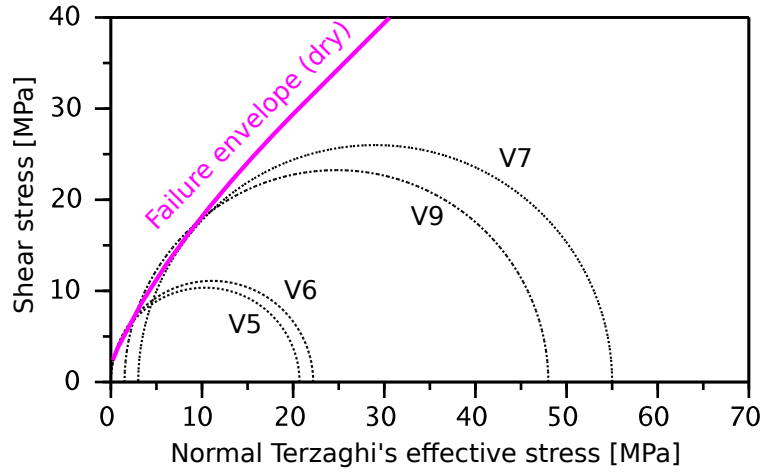


Figure 5: Summary of triaxial shear tests with Mohr circles at failure. The pink line represents the Hoek-Brown fitted shear failure envelope of dry specimens.

144 *3.2. CO<sub>2</sub> testing – Desorption-induced shear failure*

145 Table 2 lists the initial (subindex *i*) and final conditions (subindex *f*) of  
146 all desorption experiments performed. The experiments are carried out at  
147  $39 \pm 1^\circ\text{C}$ . Seven days of exposing the coal core to  $\text{CO}_2$  are quite likely enough  
148 to allow significant sorption, because in this time frame the measured swelling  
149 strains reached steady state values in the order of 2 to 3% attributable only to  
150 adsorption. Figure 6 shows the experimental time history of specimen V2b  
151 upon desorption. Depressurization starts at 0.112 days, moment at which  
152 the pressure of the loading cap downstream is regulated to  $p_{DS} = 1$  MPa.  
153 Five minutes later, the pressure at the loading cap upstream is regulated to  
154  $p_{US} = 1.5$  MPa. Notice that at this time the fluid pressure in the cleats is  
155 likely to be higher than the pressure regulated at loading caps. 15 minutes  
156 after having regulated the pressure at the loading cap upstream, the pressure  
157 at the loading cap downstream is regulated one more time to  $p_{DS} = 0.5$  MPa.

Table 2: List of CO<sub>2</sub> zero-lateral strain desorption experiments: initial and final pressure-stress conditions.

Specimen	Initial conditions			Final conditions		
	$p_{ci}$ [MPa]	$\sigma_{ri}$ [MPa]	$\sigma_{ai}$ [MPa]	$p_{cf}$ [MPa]	$\sigma_{rf}$ [MPa]	Failure [Y/N]
V2a	10.0	-21.0	-22.0	1.0	-2.0	N
V3a	5.0	-6.0	-10.0	0.5	-0.6	N
V2b	10.0	-15.0	-30.0	1.5-0.5	-2.0	Y
V3b	10.0	-15.0	-30.0	1.0	-3.0	Y

This experiment shows that the result of depressurization and desorption at zero-lateral strain is a reduction of 13 MPa of radial stress. Failure (at constant total vertical stress) manifests itself through the measured variables as a rapid homogenization of the pressures upstream and downstream (shear fractures form) and a rapid change of strains in axial (contraction) and radial (expansion) directions. The radial strain is not controllable anymore after the onset of failure.

Figure 7 shows the experimental data from Figure 6 plotted independently of time. Figure 7-a shows the change of strain as a function of total radial stress. Radial strain  $\varepsilon_r$  remains nearly constant till the onset of failure. Figure 7-b shows the change of total stresses as a function of the mean CO<sub>2</sub> pressure upstream and downstream. Figure 7-c shows the effective stress path of the apex of the Mohr circle. Recall that  $p_c$  is not homogeneous through the specimen and its average value is unknown shortly after depressurization. Terzaghi's effective stress is computed with an average value of CO<sub>2</sub> pressure:  $\sigma'_r = -[\sigma_r + (p_{US} + p_{DS})/2]$  and  $\sigma'_a = -[\sigma_a + (p_{US} + p_{DS})/2]$ . The increase

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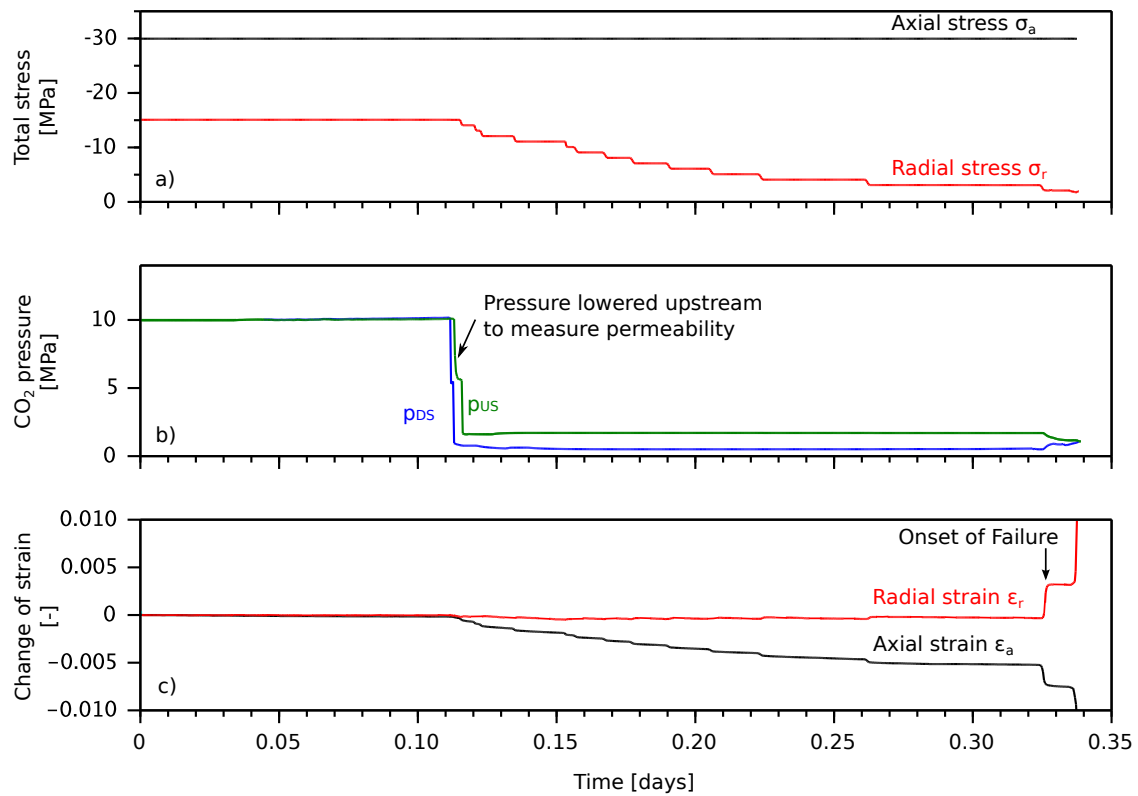


Figure 6: Time history of experiment V2b: a) total stresses, b) fluid pressure measured at upstream and downstream loading caps (a pressure gradient is applied to measure permeability), and c) change of strain respect to equilibrium initial conditions.

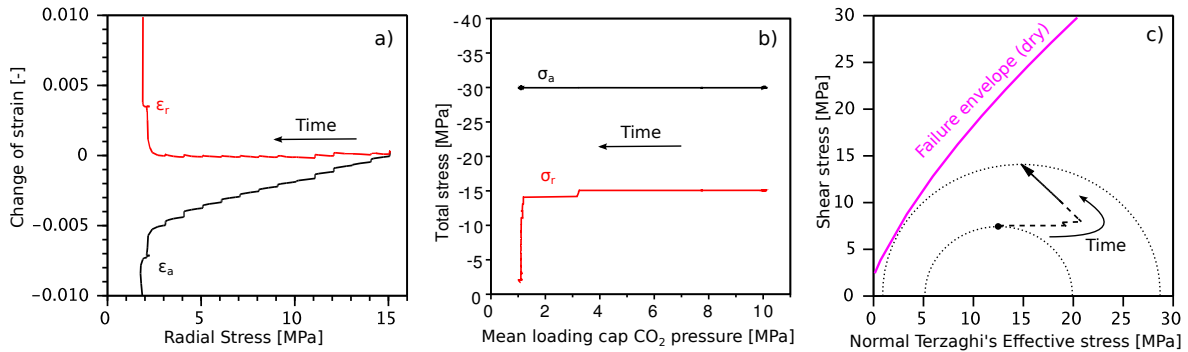


Figure 7: Experimental data from experiment V2b: a) deformation as a function of radial stress, b) path of total stresses as a function of the mean CO<sub>2</sub> pressure upstream and downstream  $(p_{US} + p_{DS})/2$ , and c) path of the apex of the Terzaghi's effective stress Mohr circle (the pressure in the cleats  $p_c$  is not well approximated by the average loading cap pressures right after depressurization – plotted as dashed lines).

in deviatoric stress is clearly manifested by an increase in the radius of the Mohr circle. Specimen V2b fails upon desorption at a state of stress which nearly touches the failure envelope fitted for coal cores from the same seam without CO<sub>2</sub>.

Figure 8 shows post-testing X-ray computed tomography images of specimen V2b. The images confirm pervasive shear failure all over the specimen. Many fractures seem to be initiated at pre-existing fractures and continue through lamination layers.

Experiment V3b showed a response to desorption similar to that of specimen V2b. Shear failure occurred by gradual but steady increase in axial strain, much less abruptly than in experiment V2b. Experiments V2a and V3a experienced desorption-induced reduction of lateral stress but did not achieve shear failure. Notice that experiment V3a reaches nearly zero Terzaghi's effective radial stress. At this point, the radial confining pressure (ra-

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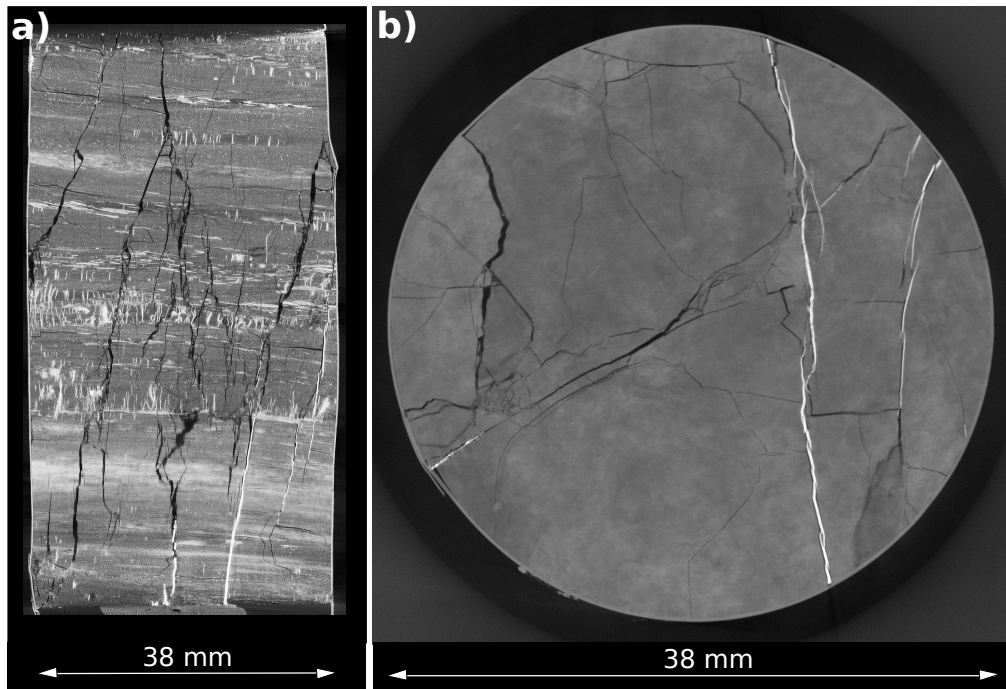


Figure 8: Coal specimen V2b after desorption-induced shear failure imaged by X-ray computed tomography at Laboratoire Navier ([navier.enpc.fr/Microtomographe](http://navier.enpc.fr/Microtomographe)): a) vertical cross section and b) horizontal cross section. Intense white regions represent calcite-filled fractures. Diffuse white regions indicate higher clay-content lamination layers. Dark black stands for voids and empty fractures. Resolution: 25  $\mu\text{m}$ . Note: the specimen is still contained by confining membrane at the time of X-ray imaging.



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10 188 dial stress) cannot be reduced to compensate shrinkage because otherwise  
11 189 the pore-fluid would escape into the confining fluid. Thus, zero-lateral strain  
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13 190 condition cannot be held anymore after this point and the specimen contin-  
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15 191 ues to desorb shrinking in all directions. Similarly, shear failure does not  
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17 192 indicate the end of desorption. Cores from experiments V2b and V3b likely  
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19 193 continued to desorb and shrink after shear failure.  
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## 22 194 **4. Discussion**

### 23 24 25 195 *4.1. Fluid-specific effects and scale effects*

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27 196 The underlying physical mechanisms and geomechanical consequences are  
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29 197 expected to be qualitatively similar with CH<sub>4</sub> and CO<sub>2</sub>. Nonetheless, two  
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31 198 points must be considered to project our experimental results to CBM ap-  
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33 199 plications.

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35 200 First, CO<sub>2</sub> adsorption-induced strains are nearly two to three times as  
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37 201 high as the ones induced by CH<sub>4</sub> adsorption at the same bulk fluid pressure  
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39 202 (Chikatamarla et al., 2009; Pini, 2009; Pan and Connell, 2011). Independent  
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41 203 gravimetric sorption measurements on crushed coal from the same formation  
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43 204 as the one tested here show that the maximum excess sorption of CO<sub>2</sub> is  
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45 205 1.4 mmol/g, about twice as high as the maximum excess sorption of CH<sub>4</sub>  
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47 206 (experiments performed by BGC-Analytik UG). Hence, our laboratory ex-  
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49 207 perimental results present a scenario considerably more likely to induce shear  
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51 208 failure by desorption as it would be the case using CH<sub>4</sub>.

52 209 Second, various studies indicate changes in geomechanical parameters  
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54 210 with CO<sub>2</sub> sorption, including reduction of Young's modulus (Masoudian  
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56 211 et al., 2013, 2014; Hol et al., 2014), reduction of unconfined compression  
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212 strength (Czaplinski and Holda, 1982), enhanced creep (Hagin and Zoback,  
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213 2010) and microfracturing (Hol et al., 2012) when coal is exposed to CO<sub>2</sub>  
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214 sorption. Although CO<sub>2</sub> may affect the coal matrix in ways that CH<sub>4</sub> may  
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215 not, our results show little affect of CO<sub>2</sub> sorption on the shear strength of  
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216 coal cores with natural fractures compared to dry coal. Similarly to coal  
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217 cores, the shear strength of the coal seam will be dominated by pre-existing  
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218 planes of weakness.

#### 219 *4.2. Failure mechanism*

220 Let us evaluate the state of stresses of a representative elementary vol-  
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222 ume (REV) of a coal seam through its effective stress Mohr circle. Terzaghi's  
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224 effective stress (defined as  $\sigma' = -(\sigma + p_c)$ ) is used since in this section we  
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226 at evaluating failure rather than deformation (Boutéca and Guéguen, 1999).  
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228 Figure 9 shows a series of steps that illustrate the proposed failure mecha-  
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230 nism. These steps are summarized as follows:

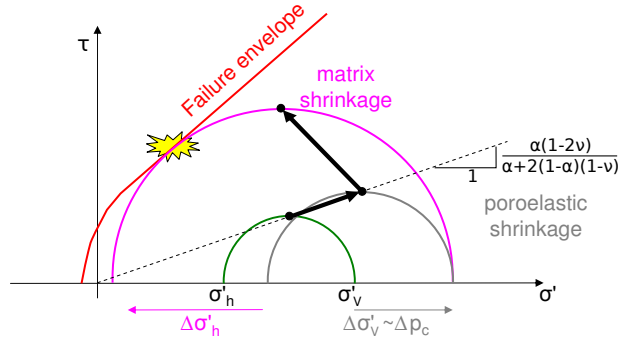
- 231 1. Assume the original conditions correspond to a normal faulting regime  
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233 such that the absolute value of total vertical stress  $\sigma_V$  is higher than  
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235 the maximum  $\sigma_{Hmax}$  and minimum horizontal stresses  $\sigma_{hmin}$  ( $|\sigma_V| >$   
236  
237  $|\sigma_{Hmax}| > |\sigma_{hmin}|$ ) and that the effective stress anisotropy ratio  $\sigma'_V/\sigma'_h$   
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239 is below the critical value for promoting shear failure (where horizontal  
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241 stresses are assumed to be the same  $\sigma_h = \sigma_{Hmax} = \sigma_{hmin}$  for the sake  
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243 of simplicity).
- 244 2. Under zero-lateral strain condition, a fluid pressure reduction in the  
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246 fractures increases effective stresses  $\sigma'_V$  and  $\sigma'_h$ . According to linear  
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248 isotropic poroelasticity, the increases in Terzaghi's effective stress are

$\Delta\sigma'_V = -\Delta p_c$  and  $\Delta\sigma'_h = [(1 - 2\nu)(1 - \nu)^{-1}\alpha - 1]\Delta p_c$ , with  $\alpha$  the Biot coefficient,  $\nu$  the Poisson's ratio, and  $\Delta p_c < 0$  the reservoir change in pressure due to depletion. Thus, the shear stress  $(\sigma'_V - \sigma'_h)/2$  increases by  $-\alpha(1 - 2\nu)[2(1 - \nu)]^{-1}\Delta p_c$  and the average stress  $(\sigma'_V + \sigma'_h)/2$  increases by  $\{\alpha(1 - 2\nu)[2(1 - \nu)]^{-1} - 1\}\Delta p_c$  upon reservoir depletion.

3. Desorption induces coal matrix shrinkage, which, given the zero-lateral strain condition, upscales as a reduction of compressive effective lateral stress  $\Delta\sigma'_h$ . If desorption takes place at constant gas pressure in the fractures, i.e., desorbed gas is quickly drained compared with desorption times, then the effective vertical stress remains constant, so that, only the lateral effective stress changes.
4. The lateral stress reduction induced by desorption increases stress anisotropy until a situation in which coal shear failure may occur, depending on the coal shear strength and initial pressure-stress conditions.

Our experiments (see Figure 7-c) show that the above proposed mechanism is quite likely to explain the stress path observed experimentally and the stress path that a coal seam in the field would go through upon depletion. Step 2 (poroelastic shrinkage) could not be measured in the laboratory because the CO<sub>2</sub> pressures upstream and downstream are regulated early to facilitate rapid desorption and set with a pressure gradient of about 1 MPa. The upper bound for fracture-induced poroelastic increase in maximum shear stress is  $-\alpha(1 - 2\nu)[2(1 - \nu)]^{-1}\Delta p_c$ . Consider  $\nu = 0.3$  and  $\alpha = 1$ , the change in shear stress of specimen V2b upon depressurization of the cleat system ( $\Delta p_c = 9$  MPa) should be at most  $\sim 2.6$  MPa. Figure 7-c shows an increase of maximum shear stress of about 14 MPa, about five times higher than the

Stress path of coal seam REV far from the near-wellbore effects



- 1 – Original normal faulting conditions  $\sigma'_v > \sigma'_h$
- 2 – Rapid depressurization  $\Delta\sigma'_v \sim \Delta p_c$ ;  $\Delta\sigma'_h \sim [\alpha(1-2\nu)(1-\nu)^{-1}-1] \Delta p_c$
- 3 – Slow desorption  $\Delta\sigma'_h < 0$  at  $\epsilon_h \sim 0$
- 4 – Shear failure

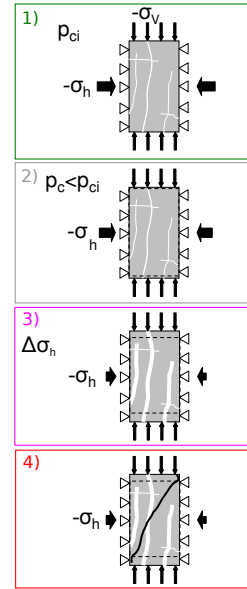


Figure 9: Mechanism for desorption-induced shear failure of coal seams in terms of effective stresses: 2-D Mohr circle representation and stress path.

value expected for poroelastic shrinkage, supporting the fact that desorption played a role decreasing the absolute value of radial stress. The absolute value of total radial stress measured in all experiments showed a clear and steady reduction at constant upstream/downstream pressure ( $\text{CO}_2$  is drained as it desorbs - see Table 2). The resulting stress path (at constant fluid pressure) is a movement of the apex of the Mohr circle in direction up-left, which can only be explained by shrinkage of the solid skeleton, in this case driven by desorption-mechanical coupling.

#### 4.3. Reservoir space analysis

The stress path of the coal reservoir can also be analyzed in terms of total stresses (see Figure 10). First, reservoir depletion under zero-lateral strain induces a poroelastic reduction of the absolute value of total lateral

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10 273 stress equal to  $\Delta\sigma_h = A\Delta p_c$  where  $A = -\alpha(1 - 2\nu)/(1 - \nu)$  (positive when  
11 274 compression stresses are assumed positive – Segall and Fitzgerald (1998)).  
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13 275 Next, desorption-induced shrinkage manifests itself as a decrease of lateral  
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15 276 stress at constant fluid pressure in fractures (assuming that desorbed gas  
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17 277 quickly drains through the fractures). The actual path (a combination of  
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19 278 both phenomena) would depend on the rate of transfer of fluid from the  
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21 279 matrix to the fractures, the permeability of fractures, and the distance of  
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23 280 the coal block to the wellbore. The likelihood to achieve failure depends on  
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25 281 the initial stress conditions, the initial pore pressure, the amount of sorbed  
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27 282 fluid, the drawdown pressure, and the adsorptive-mechanical properties of  
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29 283 the coal matrix. As regards initial stress conditions, coal seams in a normal  
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31 284 faulting environment would be more prone to shear failure by reduction of  
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33 285 lateral stresses than in a reverse or strike-slip faulting environment. Figure  
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35 286 10 highlights the fact that horizontal stresses can decrease significantly more  
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37 287 in sorbing rocks than in non-sorbing rocks subjected to depletion.

#### 38 39 288 *4.4. Application to field conditions and impact of coal failure on seam per-* 40 41 289 *meability*

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43 290 The experimental and modeling results presented in this study are valid  
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45 291 for zero-lateral strain condition with constant total vertical stress. Further  
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47 292 validation is needed in areas where boundary conditions are different, such  
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49 293 as near the wellbore, near hydraulic fractures if any, in the flanks of the  
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51 294 reservoir, and whenever stress overarching develops in the caprock. For ex-  
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53 295 ample, wellbore direction respect to the principal stresses would affect the  
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55 296 state of stresses near wellbore. Casing and perforations if any would also  
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57 297 modify the state of stresses near the wellbore. A coupled numerical solver is

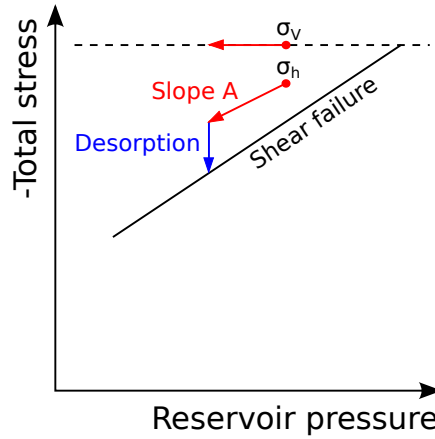


Figure 10: Reservoir space analysis of desorption-induced shear failure in coal seams subjected to depletion.

needed to analyze full scale well production and match modeling predictions to observations in the field at specific sites.

Shear failure in coal seams is not detrimental to permeability per se. For example, induced shear failure within chalk reservoirs in the North Sea is thought to be responsible for keeping high reservoir permeability in spite of significant matrix porosity reduction (Teufel et al., 1991). What is detrimental for permeability is the production of fines during shearing and the loss of hydraulic head due to fines clogging in originally clean fractures. Hence, reservoir management can be aimed at (1) managing fines by casing wellbores or screening the fines, or (2) finding the maximum drawdown pressure for which the coal seam does not fail in shear. Alternative (2) requires a poromechanical model which can capture the reduction of lateral stress induced by desorption (see Section 5).

In addition to  $\text{CH}_4$  depletion,  $\text{CO}_2$  injection may also induce coal shear failure (Palmer, 2008). In the context of the experimental evidence presented

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313 here, this could be explained by an excessive increase of lateral stress induced  
314 by adsorption which could lead to failure in reverse faulting stress regime  
315 within the coal seam.

316 *4.5. Other chemo-thermo-mechanical couplings leading to lateral stress re-*  
317 *laxation and induced shear failure*

318 Natural and anthropogenic lateral stress relaxation phenomena have been  
319 observed in various cases. First, polygonal faults form in the absence of tec-  
320 tonic stresses and are believed to originate from the volumetric contraction  
321 of sedimentary layers; the mechanism of contraction has been linked to wa-  
322 ter expulsion from the pore space upon overburden loading and thermal  
323 contraction (Cartwright and Lonergan, 1996). Recent findings show that  
324 mineral dissolution during rock diagenesis can contribute to a relaxation of  
325 lateral stress in sedimentary basins (Shin et al., 2010). Second, cold water  
326 injection in hot reservoirs causes thermal contraction. Thermal contraction  
327 contributes to decrease lateral stresses. Evidence from enhanced geothermal  
328 energy recovery sites shows significant induced seismicity caused by a com-  
329 bination of rock cooling and reduction of effective stress with ensuing shear  
330 slip of optimally oriented fractures (Majer et al., 2007). Sharp temperature  
331 gradients may even induce open mode fractures and rock spalling (Dikken  
332 and Niko, 1987).

333 **5. Geomechanical modeling**

334 Section 3 presents experimental evidence indicating that desorption under  
335 zero-lateral strain condition leads to reduction of lateral stress, increased  
336 stress anisotropy, and eventually to shear failure. Here we show a numerical

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337 simulation of the experiment V2b (Figures 6 and 7) using a double porosity  
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338 poromechanical model with coal core and matrix parameters measured for  
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12 the same coal by Espinoza et al. (2014). We add an additional numerical  
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339 simulation of what would be expected for the same coal core subjected to  
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15  
340 simulation of what would be expected for the same coal core subjected to  
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341 CH<sub>4</sub> desorption. The shear strength of “dry” coal measured in Section 3.1 is  
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342 used as an upper bound of the shear strength of coal that would be expected  
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343 for coal saturated with gas.

### 22 23 344 *5.1. Theoretical modeling*

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345 We have developed a double porosity poromechanical model for trans-  
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346 verse isotropic coal seams (Nikoosokhan et al., 2012; Espinoza et al., 2014).  
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347 This model is based on the embedment of an adsorptive-mechanical model  
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348 of the coal matrix (which develops adsorption stresses  $s^a$ ) into a larger frac-  
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349 tured poroelastic medium (the coal seam – with stiffness moduli  $C_{ij}$  and Biot  
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35  
350 coefficients  $\alpha_h$  and  $\alpha_V$  relevant to transverse isotropy). Total seam horizon-  
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351 tal stress  $\sigma_h$  and vertical stress  $\sigma_V$  are affected by the strain tensor  $\underline{\underline{\epsilon}}$ , the  
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352 pore pressure in the cleats  $p_c$ , and the adsorption-strain coupling through the  
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353 adsorption stress  $s^a$  weighed by the Biot coefficients. The following applies  
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354 when horizontal stresses are the same in both directions.

$$\begin{cases} \sigma_h &= (C_{11} + C_{12})\epsilon_h + C_{13}\epsilon_V - \alpha_h p_c - (1 - \alpha_h)s^a(p_m) \\ \sigma_V &= 2C_{13}\epsilon_h + C_{33}\epsilon_V - \alpha_V p_c - (1 - \alpha_V)s^a(p_m) \end{cases} \quad (1)$$

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355 The adsorption stress  $s^a(p_m)$  developed by the coal matrix depends on  
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356 the amount of adsorbed fluid in the coal matrix  $n_m(p_m, \epsilon_m)$  and swelling  
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357 properties of the coal matrix as follows,  
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$$s^a(p_m) = \int_0^{p_m} \left. \frac{\partial n_m}{\partial \epsilon_m} \right|_{p_m} \bar{V}_b(p_m) dp_m \quad (2)$$

where the thermodynamical pressure  $p_m$  is the pressure of the bulk fluid at the same chemical potential of the adsorbed phase in the coal matrix.  $\bar{V}_b(p_m)$  is the molar volume of the fluid phase in bulk conditions. The amount of adsorption in the coal matrix  $n_m$  depends on fluid thermodynamical pressure  $p_m$  as well as on the coal matrix strain  $\epsilon_m$  (Brochard et al., 2012). A first order approximation permits expressing this amount as

$$n_m(p_m, \epsilon_m) = n_{m0}(p_m) [1 + c(p_m)\epsilon_m] \quad (3)$$

where  $n_{m0}(p_m)$  is the adsorption isotherm at zero volumetric strain, here approximated as a Langmuir type isotherm on pressure  $n_{m0}(p_m) = n_0^{max}[p_m/(p_m + p_{L0})]$ , and  $c(p_m)$  is the adsorption-strain coupling coefficient. The coal seam poroelastic coefficients relate to initial cleat macroporosity  $\phi_{c0}$  and the bulk modulus of the coal matrix  $K_m$  through micromechanical equations shown elsewhere (Espinoza et al., 2014).

The pressure  $p_m$  at the coal matrix can be different from the fracture cleat pressure  $p_c$  if the coal matrix and the seam are not in thermodynamical equilibrium. Reservoir depletion implies a change of fluid pressure in fractures  $\Delta p_c$  (fracture drainage) and a change in the coal matrix thermodynamical equilibrium pressure  $\Delta p_m$  (desorption). Under zero-lateral strain condition, the changes of lateral stresses and vertical strain are the following (Equation 1):

$$\begin{cases} \Delta\sigma_h &= \left(\frac{C_{13}}{C_{33}}\alpha_V - \alpha_h\right)\Delta p_c + \left[\frac{C_{13}}{C_{33}}(1 - \alpha_V) - (1 - \alpha_h)\right]\frac{ds^a(p_m)}{dp_m}\Delta p_m \\ \Delta\varepsilon_V &= \frac{1}{C_{33}}\alpha_V\Delta p_c + \frac{1}{C_{33}}(1 - \alpha_V)\frac{ds^a(p_m)}{dp_m}\Delta p_m \end{cases} \quad (4)$$

377 where

$$\begin{cases} \frac{C_{13}}{C_{33}} &= \frac{E\nu_3}{E_3(1-\nu)} \\ \frac{1}{C_{33}} &= \frac{1-\nu-2(E/E_3)\nu_3^2}{E_3(1-\nu)} \end{cases} \quad (5)$$

378 in terms of Young's modulus parallel to the bedding plane  $E$ , Poisson's ratio  
 379 in the bedding plane  $\nu$ , Young's modulus perpendicular to the bedding plane  
 380  $E_3$  and Poisson's ratio in planes perpendicular to the bedding plane  $\nu_3$ .

381 Notice that both  $\sigma_h$  and  $\varepsilon_V$  depend on variations of the fluid pressure in  
 382 the cleats  $\Delta p_c$  (conventional poroelastic path) and variations of fluid pressure  
 383 in the coal matrix  $\Delta p_m$  (desorption path).

### 384 5.2. Model parameters

385 Previous work from the authors measured the adsorptive-mechanical prop-  
 386 erties of the coal cores tested in this study (Espinoza et al., 2014). Table 3  
 387 summarizes the best fitting parameters of the fully coupled double-porosity  
 388 transverse isotropic poroelastic model introduced above.

### 389 5.3. Numerical simulation of $CO_2$ desorption experiment at zero-lateral strain 390 condition

391 Let us simulate experiment V2b shown in Figures 6 and 7. The experi-  
 392 ment follows the loading path summarized in Table 4.

393 Event (4) depletion-desorption is decomposed into the variation of pres-  
 394 sure in the cleats  $\Delta p_c$  and then coal matrix desorption  $\Delta p_m$ . Figure 11

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Table 3: Parameters of poroelastic model for coal cores with dual porosity, i.e., cleat and coal matrix porosity.

Core scale	Matrix scale
$E = 2736$ MPa	$K_m = 5000$ MPa
$E_3 = 2551$ MPa	$n_0^{max} = 2.4$ mol/L (CO <sub>2</sub> )
$\nu = 0.267$	$p_{L0} = 1.6$ MPa (CO <sub>2</sub> )
$\nu_3 = 0.267$	$c = 11$ (CO <sub>2</sub> )
$\phi_{c0} = 0.08$	

Table 4: Desorption experimental pressure-stress path and boundary conditions for experiments V2b.

Event	Axial stress $\sigma_r$	Radial stress $\sigma_a$	Fluid pressure $p_c$
1) Dry loading to isotropic state of stress	0 to -12 MPa (Prescribed)	0 to -12 MPa (Prescribed)	None
2) CO <sub>2</sub> injection and adsorption at constant confining stress	-12 MPa (Prescribed)	-12 MPa (Prescribed)	0 to 10 MPa (Prescribed)
3) Increase of stress anisotropy to the initial state of stress	-12 to -30 MPa (Prescribed)	-12 to -15 MPa (Prescribed)	10 MPa (Prescribed)
4) Depletion-desorption	-30 MPa (Prescribed)	variable to maintain $\Delta\varepsilon_r = 0$	10 to 1 MPa (Prescribed)

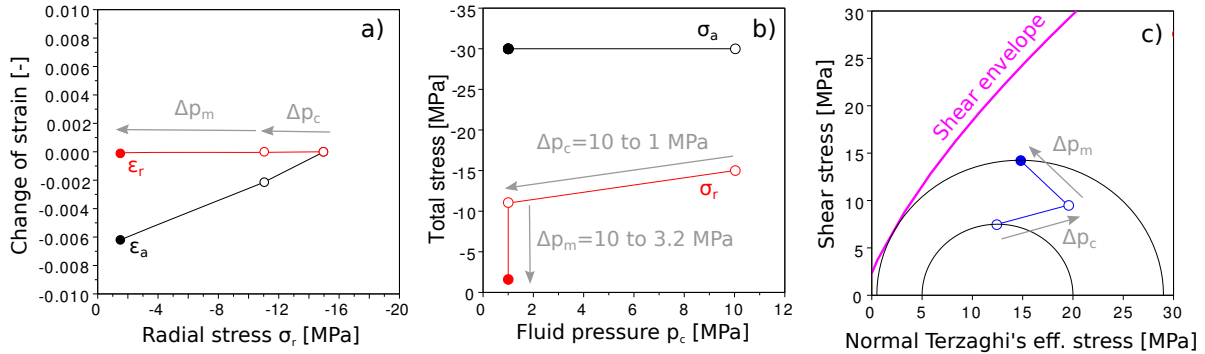


Figure 11: Numerical simulation of coal core depletion-desorption of CO<sub>2</sub> under zero-lateral strain condition. (a) Change of strains. (b) Total stresses. (c) Terzaghi's effective stress Mohr circle.

395 shows the numerical simulation results starting from event (4). Deformation  
 396 is taken as a reference equal to zero at the beginning of event (4).

397 The pressure drawdown promotes gas drainage from fractures and gas  
 398 desorption from the coal matrix. The poroelastic response of fractures is  
 399 proportional to  $\Delta p_c = -9$  MPa and promotes a shortening of the specimen  
 400  $\Delta \epsilon_a = -0.002$ , reduction of total radial stress  $\Delta \sigma_r = -4$  MPa, and movement  
 401 of the apex of the effective stress Mohr circle in up-right direction with a  
 402 decrease of the maximum ratio of shear to normal effective stress. The effect  
 403 of desorption is proportional to  $\Delta p_m$ . As  $p_m$  decreases, the specimen shortens  
 404 further in vertical direction, radial stress becomes less compressive, and the  
 405 apex of the effective stress Mohr circle moves in up-left direction. In Figure  
 406 11,  $p_m$  varies from 10 MPa to 3.2 MPa. The thermodynamic pressure of the  
 407 coal matrix cannot go lower because the core fails in shear at  $p_m = 3.2$  MPa.  
 408 Hence, the modeling results suggest that experiment V2b shown in Section  
 409 3 would have failed for any drawdown pressure lower than  $\sim 3.2$  MPa using

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410 CO<sub>2</sub>.

411 We simulate the loading path followed upon depressurization for all des-  
412 orption experiments in zero-lateral strain condition. The simulation is based  
413 on the initial stress and pressure conditions shown in Table 2 assuming that  
414 cleat depressurization occurs first  $\Delta p_c$  and desorption follows  $\Delta p_m$ . The final  
415 simulation pressure-stress point is chosen to be the point at which effective  
416 stresses reach the Hoek-Brown criterion (Experiment V2a,V2b, and V3b) or  
417 the point at which Terzaghi's radial effective stress becomes zero  $\sigma_r + p_c = 0$   
418 (Experiment V3a). The latter condition reflects the fact that the radial con-  
419 fining pressure (radial stress) cannot be set lower than the fluid pressure  
420 experimentally because the fluid would escape into the confining fluid.

421 Table 5 summarizes the values of cleat pressure, radial stress and thermo-  
422 dynamic pressure in the coal matrix at the final pressure-stress simulation  
423 point. The simulation predicts shear failure for experiment V2a as opposed  
424 to what is observed experimentally, although the difference between  $p_{mf}$  and  
425  $p_{cf}$  is small suggesting that the model was not too far from predicting the  
426 right value. Experiment V3a starts with a low axial stress, thus it is not  
427 expected to fail even if lateral stress goes to zero, however, numerical sim-  
428 ulation help calculate the reduction in lateral stress to near zero effective  
429 lateral stress as observed experimentally. The model does predict the shear  
430 failure of experiments V2b and V3b. Furthermore, the numerical simula-  
431 tion suggests that these experiments were ended (because of shear failure)  
432 significantly before achieving thermodynamical equilibrium  $p_{mf} > p_{cf}$ .

Table 5: List of simulated CO<sub>2</sub> zero-lateral strain desorption experiments: final pressure-stress conditions. Initial conditions are described in Table 2.

Simulated Experiment	Final pressure in cleats $p_{cf}$ [MPa]	Predicted radial radial stress at the end of the test $\sigma_{rf}$ [MPa]	Predicted coal matrix fluid pressure at the end of the test $p_{mf}$ [MPa]	Hoek-Brown criterion achieved? Shear failure [Y/N]
V2a	1.0	-1.0	1.6	Y
V3a	0.5	-0.5	3.5	N
V2b	1.0	-1.5	3.2	Y
V3b	1.0	-1.5	3.2	Y

#### 5.4. Numerical simulation of analogous desorption experiment with CH<sub>4</sub>

Let us now simulate what the response of an analogous experiment using CH<sub>4</sub> would be. We roughly assume that coal would swell about a third as much with CH<sub>4</sub> compared to CO<sub>2</sub> at the same fluid pressure (see Section 4.1). Hence, we approximate the parameters of the coal matrix with  $n_0^{max} = 1.2$  mol/L and  $c = 6$ . The simulation follows the path stipulated in Table 4 and the results are shown in Figure 12. Clearly there is less pronounced reduction of radial stress due to desorption in this case compared to the case with CO<sub>2</sub> desorption. As expected, the fracture poroelastic response is exactly the same in both cases.

The model predicts that shear failure does not occur with CH<sub>4</sub> given the initial pressure-stress conditions, even though  $p_m$  reaches the drawdown pressure  $p_m = p_c = 1$  MPa. Field scale seams have negligible unconfined compression strength, hence, the friction strength of fractures could be chal-

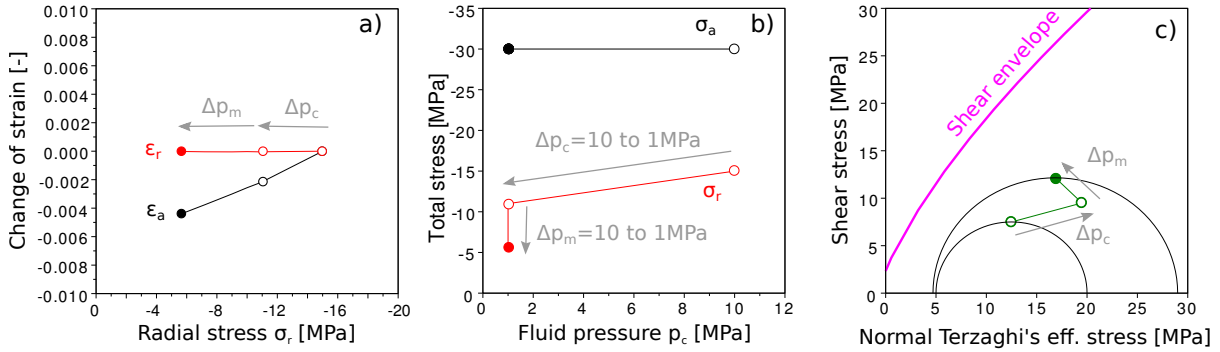


Figure 12: Numerical simulation of coal core depletion-desorption of CH<sub>4</sub> under zero-lateral strain condition. (a) Change of strains. (b) Total stresses. (c) Terzaghi's effective stress Mohr circle.

lenged by change of stresses induced by desorption. Even with CH<sub>4</sub>, the increase of stress anisotropy and movement of the apex of the Mohr circle in up-left direction may induce state of stress with ratio of shear stress to effective normal stress high enough to promote shear failure of existent fractures and fines production.

## 6. Conclusions

Deep coal beds have unique transport and mechanical properties, and hence, they require particular completion and production strategies. Desorption-induced coal shrinkage is advantageous because it increases permeability upon depletion. Yet, extensive coal mechanical failure and fracture plugging with fines has sometimes been observed after steep increases of permeability. It is known that near-wellbore stress concentration and fracture poroelastic response help increase stress anisotropy in the reservoir rock upon depletion and may favor shear failure. Far from the wellbore, the coal seam is

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10 461 expected to follow compression under zero-lateral strain and constant total  
11 462 vertical stress. At this condition, we show through triaxial experiments that  
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13 463 reduction of lateral stress induced by the shrinkage of the coal matrix during  
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15 464 gas desorption can significantly favor coal shear failure far from the well-  
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17 465 bore. Performed tests show a clear increase of stress anisotropy induced by  
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19 466 desorption, in some cases leading to shear failure.

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21 467 The stress path under zero-lateral strain condition depends on variations  
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23 468 of pore pressure in the coal cleats and on variations of stresses caused by gas  
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25 469 desorption from the coal matrix. In general, two parts of the stress path can  
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27 470 be recognized: (1) conventional stress path characterized by the poroelastic  
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29 471 coefficient  $\alpha(1 - 2\nu)/(1 - \nu)$  and induced by variation of the fluid pressure  
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31 472 in the cleats  $p_c$ , and (2) desorption-induced decrease in lateral stress defined  
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33 473 by the adsorptive-mechanical properties of the coal matrix and promoted by  
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35 474 a variation of adsorption stress in the coal matrix. The steep slope of the  
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37 475 desorption-induced path can reach the failure envelope and promote shearing  
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39 476 sooner than would happen for a conventional non-adsorptive reservoir rock.

40 477 Coal failure can be predicted by knowing the original state of stresses,  
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42 478 coal shear failure envelope, and the mechanical-adsorptive properties of the  
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44 479 coal. We developed a model that links all these variables and showed its  
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46 480 application to match laboratory experiments. Coupled numerical simula-  
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48 481 tion considering more realistic boundary conditions and completion details  
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50 482 is needed to validate our findings to specific field observations. To the best of  
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52 483 our knowledge, this is the first model that offers a consistent analysis on the  
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54 484 depletion of coal seams and ensuing failure, incorporating explicitly a stress  
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56 485 path solely due to desorption.



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491 improving this manuscript.  
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492 **7. Symbols**

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$\alpha$	Biot coefficient [-]
$\varepsilon$	Strain [-]
$\phi_c$	Macroporosity [-]
$\mu$	Friction coefficient [-]
$\nu$	Poisson's ratio [-]
$\sigma$	Total stress [Pa]
493 $\sigma'$	Effective stress [Pa]
$\tau$	Shear stress [Pa]
$A$	Poroelastic depletion slope [-]
$C_{ij}$	Stiffness tensor coefficient [-]
$E$	Young's modulus [E]
$p_m$	Thermodynamical pressure of the coal matrix [Pa]
$p_c$	Pressure in cleats [Pa]

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