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DISTRIBUTED MODEL PREDICTIVE CONTROL OF A HYDRO-POWER VALLEY BY DUAL DECOMPOSITION

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Abstract: In this paper, a suboptimal distributed MPC approach for linear interconnected systems is considered, where it is assumed that the systems are coupled through their control inputs and an optimal reference tracking problem for the overall system is solved. The approach is applied to distributed MPC of a hydro-power valley case study.

Key words: Distributed Model Predictive Control, Interconnected Systems, Constraints.

INTRODUCTION

Model predictive control (MPC) involves the solution at each sampling instant of a finite horizon optimal control problem subject to the system dynamics, and state and input constraints. Solving in a centralized way MPC problems for large-scale systems may be impractical due to the topology of the plant and data communication and the large number of decision variables. Recently, several approaches for decentralized and parallel implementation of MPC algorithms have been proposed, [1] - [4].

In [5] - [8], approaches for distributed/decentralized MPC for systems consisting of linear interconnected subsystems have been developed. The approach in [7] is based on the dual decomposition method [9], where large-scale optimization problems are handled by using Lagrange multipliers to relax the couplings between the sub-problems. In [8], a distributed optimization algorithm based on accelerated gradient methods using dual decomposition is proposed and its performance is evaluated on optimization problems arising in distributed MPC. Also, approaches for distributed MPC for systems composed of several nonlinear subsystems have been proposed (e.g. [10], [11], [12]).

In this paper, a modification of the suboptimal distributed MPC approach [7] is considered, where it is assumed that the interconnected linear systems are coupled through their control inputs and an optimal reference tracking problem for the overall system is solved. The approach is applied to distributed MPC of a hydro-power valley case study, described in [13].

THE HYDRO-POWER VALLEY CASE STUDY

Description

The hydro-power valley is a set of hydroelectric production plants, depending on interconnected water resources (typically along a river) and aiming at producing a given amount of electricity according to a daily power-generation program for each power plant. In each plant, the generated power is a function of the turbine flows, which at the same time influence the reservoir levels that need to be controlled such that they are within the specified limits [13]. The control system design for a hydro-power valley should take into account the fact that the valley can face unpredictable events, such as plant failures or meteorological changes.

The configuration of the considered hydro-power valley is depicted in Fig. 1 [13].

Each power plant in the valley is characterized by the dynamics of its water storage, described as follows [13]:

\[ \frac{dh}{dt} = f_{in} - f_{out} \]  

(1)

where \( h \) denotes the water level, \( S \) the water surface, and \( f_{in}, f_{out} \) the input and output water flows, respectively. These water flows depend on the interconnections between the plants as well as the turbine flows, considered as the control inputs, and disturbance flows. By considering a sampled-data version of equation (1) for a purpose of discrete-time control, and gathering all equations of this form, the whole system is modeled as a classical state space representation [13]:

\[ x(t+1) = Ax(t) + Bu(t) + Ed(t) \]

(2)

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In (2):
\[ \begin{align*}
    x(t) &= [x_1(t), x_2(t), x_3(t)]^T, \quad u(t) = [u_1(t), u_2(t), u_3(t)]^T \\
    d(t) &= [d_1(t), d_2(t), d_3(t)]^T
\end{align*} \]
are the state, control input, and the disturbance input vectors. All state variables are assumed measurable. The matrices of the model (2) are the following [13]:

\[ A = I_{3\times3}, \quad B = \begin{bmatrix}
    -T_{S_1} S_1^{-1} & 0 & 0 \\
    0 & -T_{S_2} S_2^{-1} & 0 \\
    T_{S_1} S_1^{-1} & 0 & -T_{S_2} S_2^{-1}
\end{bmatrix} \quad (5)
\]
where \( T_s \) is the sampling time and \( S_1, S_2, S_3 \) are the cross-sectional areas of the three tanks (see Fig. 1). The following constraints are imposed on the levels in the three tanks and on the flows through the four turbines [13]:

\[ \begin{align*}
    0 & \leq [u_1(t), u_2(t), u_3(t)]^T & \leq 60 \\
    0 & \leq [u_2(t), u_3(t)]^T & \leq 60 \\
    0 & \leq [u_1(t), u_3(t)]^T & \leq 60 \\
    716.2 & \leq x_1(t) & \leq 729.5 \\
    282 & \leq x_2(t) & \leq 287.5 \\
    259.5 & \leq x_3(t) & \leq 268.5
\end{align*} \]

**Decomposition**

The hydro-power valley system, described above, can be decomposed into the following three subsystems:

**Subsystem 1:**
\[ x_1(t+1) = A_1 x_1(t) + B_1 u_1(t) + E_1 d_1(t) \]

with:
\[ \tilde{u}_1(t) = [u_1(t), u_2(t)]^T, \quad A_1 = [-T_{S_1}^{-1} - T_{S_2}^{-1}], \quad E_1 = T_{S_1}^{-1} \]

**Subsystem 2:**
\[ x_2(t+1) = A_2 x_2(t) + B_2 u_2(t) + E_2 d_2(t) \]

with:
\[ \tilde{u}_2(t) = u_2(t), \quad A_2 = [-T_{S_2}^{-1} - T_{S_3}^{-1}], \quad E_2 = T_{S_2}^{-1} \]

**Subsystem 3:**
\[ x_3(t+1) = A_3 x_3(t) + B_3 u_3(t) + B_3 u_3(t) + B_3 u_3(t) \]

with:
\[ \tilde{u}_3(t) = u_3(t), \quad A_3 = [-T_{S_1}^{-1} - T_{S_3}^{-1}], \quad B_3 = T_{S_1}^{-1} \]

It can be seen from equations (9), (11) and (13) that the three subsystems are coupled through their control inputs.

**DISTRIBUTED MPC OF LINEAR SYSTEMS COUPLED THROUGH THEIR INPUTS**

Consider a system composed by the interconnection of \( M \) local subsystems described by the following linear discrete-time models:

\[ x_i(t+1) = A_i x_i(t) + \sum_{j=1}^{M} B_{ij} u_j(t) + E_i d_i(t), \quad i = 1, 2, \ldots, M \]

where \( x_i(t) \in \mathbb{R}^{n_i}, \ u_j(t) \in \mathbb{R}^{n_j}, \) and \( d_i(t) \in \mathbb{R}^{n_i} \) are the state, control input, and disturbance input vectors, related to the \( i \)-th subsystem, and \( A_i \in \mathbb{R}^{n_i \times n_i}, \ B_{ij} \in \mathbb{R}^{n_i \times n_j}, \) and \( E_i \in \mathbb{R}^{n_i \times n_i} \) are constant matrices. It can be seen that the subsystems (15) are coupled through their control inputs. Let the overall state, control input, and disturbance input be denoted by:

\[ x(t) = [x_1(t), x_2(t), \ldots, x_M(t)]^T \in \mathbb{R}^n, \quad n = \sum_{i=1}^{M} n_i \]

\[ u(t) = [u_1(t), u_2(t), \ldots, u_M(t)]^T \in \mathbb{R}^m, \quad m = \sum_{i=1}^{M} m_i \]

\[ d(t) = [d_1(t), d_2(t), \ldots, d_M(t)]^T \in \mathbb{R}^r, \quad r = \sum_{i=1}^{M} r_i \]

The following constraints are imposed on the subsystems:

\[ u_{\text{min},i} \leq u_i(t) \leq u_{\text{max},i}, \quad x_{\text{min},i} \leq x_i(t) \leq x_{\text{max},i}, \quad i = 1, 2, \ldots, M \]

The following assumptions are made:

**A1.** Reference trajectories \( X^{ref} = [x_1^{ref}, x_2^{ref}, \ldots, x_M^{ref}]^T \) and
\[ U^{ref} = [u_1^{ref}, u_2^{ref}, \ldots, u_M^{ref}]^T \]

**A2.** A forecast \( D = [d_1, d_2, \ldots, d_M]^T \)

of the overall disturbance input realization is available for the finite horizon \( T \).

It is supposed that a full measurement \( x = [x_1, x_2, \ldots, x_M]^T \) of the overall state is available at the current time \( t \). The optimal reference tracking problem is considered where the goal is to have the overall state \( x(t) \) and control input \( u(t) \) following the reference signals \( x^{ref}(t) \) and \( u^{ref}(t) \) by minimizing certain performance index. For the current state \( x = [x_1, x_2, \ldots, x_M]^T \), the reference tracking MPC solves the optimization problem:

**Problem P1 (Centralized MPC):**

\[ \min_{x(t)} J(U, x) \]

subject to \( x_0 = x \) and:

\[ x_{i+1} = x_i, \quad i = 1, \ldots, M, \quad k = 1, \ldots, N \]

\[ u_{i+1} = u_i, \quad i = 1, \ldots, M, \quad k = 0, 1, \ldots, N-1 \]

\[ x_{i+1} = x_i + \sum_{j=1}^{M} B_{ij} u_{j+1} + E_i d_i, \quad i = 0, 1, \ldots, N-1 \]

\[ u_{i+1} = u_i + \sum_{j=1}^{M} B_{ij} u_{j+1} + E_i d_i, \quad i = 0, 1, \ldots, N-1 \]

with \( U = [u_1, u_2, \ldots, u_M]^T \) and the cost function given by:

\[ J(U, x) = \sum_{k=0}^{N-1} \sum_{i=1}^{M} J_i(x_{i+1}, u_{i+1}) \]

Here:

\[ J_i(x_{i+1}, u_{i+1}) = ||x_{i+1} - x_i^{ref}||_Q^2 + ||u_{i+1} - u_i^{ref}||_R^2 \]

is the stage cost for the \( i \)-th subsystem with corresponding weighting matrices \( Q_i, R_i > 0, \) and \( N \) is a finite horizon. It is supposed that \( N < T \) (T being the specified finite horizon of the reference trajectories and the disturbance forecast, cf. assumptions A1 and A2). The sets \( X_i \) and \( U_i \) are defined by:

\[ X_i = \{ \tilde{x}_i \in \mathbb{R}^{n_i} \mid x_{\text{min},i} \leq x_i, x_{\text{max},i} \} \]

\[ U_i = \{ \eta_i \in \mathbb{R}^{m_i} \mid u_{\text{min},i} \leq u_i, u_{\text{max},i} \} \]

and they represent convex (polyhedral) sets.

Problem P1 can be decomposed by using the dynamic dual decomposition approach [7], [9]. The following *decoupled* state equations can be formulated:

\[ x_i(t+1) = A_i x_i(t) + B_i u_i(t) + v_i(t) + E_i d_i(t), \quad i = 1, \ldots, M \]

with the additional constraints that:
\[ v_i(t) = \sum_{j=1}^{N} B_{ji} u_j(t), \quad i = 1, ..., M \quad \text{for all } t \]  

The variable \( v_i \in \mathbb{R}^N \) can be interpreted as the influence of the other subsystems in the update of \( x_i \). Then, the constraints (31) are relaxed by introducing the corresponding Lagrange multipliers \( p_i \in \mathbb{R}^N \) (also referred to as prices) in the cost function (26) and the following distributed reference tracking MPC problem is formulated:

**Problem P2 (Distributed MPC):**

\[
V^*(\lambda) = \max_{\lambda} \sum_{j=1}^{M} \left( \min_{x_i \in \mathcal{X}} \sum_{k=1}^{N} \left[ L\left(x_{i+1|k}, u_{i+1|k}, x_{i+1|k+1}, u_{i+1|k+1}\right) + \kappa_j^{*} \sum_{j=1}^{M} B_{ij}^T p_j \right] \right)
\]

subject to \( x_{i+1|k} \), constraints (21), (22) and:

\[
x_{i+1|k} = A x_{i|k} + B_i u_{i|k} + v_{i+1|k} + E d_{i+1|k}; \quad i = 1, ..., M; \quad k = 0, 1, ..., N - 1
\]

\[ p_{i+N-1} = 0 \]  

Here:

\[
P = [p_1^T, p_2^T, ..., p_M^T, p_{M+N-1}]^T
\]

with \( p_{i+k} = [p_{i+k}^T, p_{i+k+1}^T, ..., p_{i+k+M-1}^T, ..., p_{i+k+N-1}^T]^T \), \( k = 0, 1, ..., N - 1 \)

\[
U = [u_{i1}^T, u_{i2}^T, ..., u_{iM}^T, u_{iM+1}^T, ..., u_{iM+N-1}^T]^{T}
\]

\[
X = [x_{i1|T}, ..., x_{iM|T}]^T, \quad X_i = [x_{i1|T}, ..., x_{iM|T}]^T, \quad X_{i+N-1} = [x_{i1|T}, ..., x_{iM|T}]^T
\]

\[
V = [v_{i1|T}, ..., v_{iM|T}]^T, \quad V_i = [v_{i1|T}, ..., v_{iM|T}]^T, \quad V_{i+N-1} = [v_{i1|T}, ..., v_{iM|T}]^T
\]

with \( v_{i1|T} = [v_{i1|T}, v_{i2|T}, ..., v_{iM|T}]^T, \quad k = 0, 1, ..., N - 1 \)

Since the problem P1 is convex and the Slater’s condition holds for the inequality constraints (21)-(22), then \( V^{\text{opt}}(\lambda) = V^*(\lambda) \) (there will be no duality gap between the primal and the dual problem [14]).

The inner decoupled optimization problems in problem P2 are Quadratic Programming (QP) sub-problems, since the constraints (33) are linear and the stage cost function \( I_j^P(x_{i+1|k}, u_{i+1|k}, v_{i+1|k}, P) \) is quadratic:

**Problem P3** (i-th QP sub-problem):

\[
V_i^*(P, x_i) = \min_{u_{i+1|k} \in \mathcal{X}_i} \sum_{k=1}^{N} I_j^P(x_{i+1|k}, u_{i+1|k}, v_{i+1|k}, P) \]  

subject to \( x_{i+1|k} = x_i \) and:

\[
x_{i+1|k} \in \mathcal{X}_i, \quad k = 1, ..., N
\]

\[
u_{i+1|k} \in \mathcal{U}_i, \quad k = 0, 1, ..., N - 1
\]

\[
x_{i+1|k} = A x_{i|k} + B_i u_{i|k} + v_{i+1|k} + E d_{i+1|k}; \quad k = 0, 1, ..., N - 1
\]

Denote by \( U_i^* = [u_{i1}^T, u_{i2}^T, ..., u_{iM}^T, u_{iM+1}^T, ..., u_{iM+N-1}^T]^T \), \( X_i^* = [x_{i1|T}, ..., x_{iM|T}]^T \) and \( V_i^* = [v_{i1|T}, ..., v_{iM|T}]^T \) the optimal solution of P3. It should be noted that the optimal solution to these sub-problems depends on the values of the prices \( P \).

From the formulation of the distributed MPC problem P2 it can be seen that the computation of \( U_i^* \), \( X_i^* \) and \( V_i^* \) for given prices \( P \) is completely decentralized. However, finding the optimal prices requires coordination [7]. According to the duality theory [14], \( V_i^*(P, x_i) \), \( i = 1, ..., M \) are concave functions of \( P \). Therefore, the optimal price sequence \( P^* = [p_1^T, p_2^T, ..., p_{M+N-1}]^T \) can be found as the limits of a gradient iteration [7]. Given a price prediction sequence \( P_i^T = [p_{i1}^T, ..., p_{iM}^T, p_{iM+1}^T, ..., p_{iM+N-1}]^T \) for the \( i \)-th iteration, the corresponding sequences \( U_i^N = [u_{i1}^{N^T}, ..., u_{iM}^{N^T}, u_{iM+1}^{N^T}, ..., u_{iM+N-1}^{N^T}]^T \), \( X_i^N = [x_{i1|T}, ..., x_{iM|T}]^T \) and \( V_i^N = [v_{i1|T}, ..., v_{iM|T}]^T \) are computed locally by solving problem P3. Then, the prices can be updated distributively by a gradient step:

\[
p_{i+1|k} = p_{i|k} + \gamma_i^N (v_{i+1|k} - \sum_{j=1}^{M} B_{ij}^T p_j), \quad k = 0, 1, ..., N - 2
\]

with \( p_{i+1|N-1} = 0 \) and \( p_{i+1|N} = 0 \). In [7], a suboptimal algorithm for on-line computation of distributed MPC for linear interconnected systems (coupled through their states) has been suggested, where the prices are updated iteratively by a gradient step (similar to (40)). Also, a stopping criterion for the iterative updates is proposed in [7] that can be locally verified by each subsystem and that guarantees closed-loop suboptimality above a pre-specified level and asymptotic stability of the overall system. The algorithm in [7] is adapted to the case considered here, where the linear systems are coupled through their inputs.

**SIMULATION RESULTS FOR THE DISTRIBUTED MPC OF THE HYDRO-POWER VALLEY**

The distributed MPC approach is applied to the hydro-power valley, described above. The sampling time in the model (2)-(6) is \( T_s = 5 \) [min]. The prediction horizon in the MPC problem is \( N = 6 \) and the weighting matrices in the stage cost (27) are \( Q = 100, i = 1, 2, 3 \) for the first MPC approach described in the previous section is used to generate the four control inputs (turbine flows) for an initial state \( x(t) = [726.4, 283.85, 264.2]^{T} \) [m] and a disturbance \( d_{1}(t) \) in the river flow, shown in Fig. 2 (it is assumed that \( d_{2}(t) = 0 \)). The obtained suboptimal trajectories of the four turbine flows and the water levels in the three tanks are depicted in Fig. 3 to Fig. 9 along with the reference trajectories generated by a supervisory optimization algorithm.

![Fig. 2. The disturbance \( d_{1} \)](image)

![Fig. 3. The control input \( u_{1} \)](image)
It can be seen that the closed-loop trajectories obtained with the suboptimal distributed MPC approach deviate slightly from the reference ones. The accuracy of the tracking of water level $x_1$ can be improved by increasing the requirement for the level of suboptimality of the distributed MPC solution.

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