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Abatement of 3-methylbutanal and trimethylamine with combined plasma and photocatalysis in a continuous planar reactor

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Abstract

This paper deals with the 3-methylbutanal ((CH₃)₂CHCH₂COH) removal with the help of a nonthermal surface plasma discharge coupled with photocatalysis. The capability of this process for gas treatment was studied. A planar reactor system was developed in order to perform the effect of adding photocatalytic material in plasma surface discharge barrier dielectric (SDBD) zone on (i) 3-methylbutanal removal, (ii) selectivity of CO₂ and CO, (iii) byproducts formation such as ozone formation.

It was found that the influence of the UV light generated by SDBD reactor was very low. The activation of the photocatalyst media could be negligible. Whereas, the introduction of external UV light to the process improves significantly the removal efficiency of 3-methylbutanal (3MBA) and the mineralization. A synergetic effect was observed by combining plasma SDBD and photocatalysis from all experiments and with other pollutant such as trimethylamine (N(CH₃)₃). Moreover, the byproducts of 3MBA were identified and evaluated with plasma SDBD, photocatalysis and plasma SDBD/photocatalysis combination.

Keywords:

Synergetic effect; planar reactor; Plasma SDBD/photocatalysis process; VOC removal

1. Introduction

The continual release of toxic gases into the atmosphere from variety of sources (due to industrial discharges, transports, use of paints, domestic activities, etc.) has resulted in the gradual degradation of the environment [1]. This consequence, in turn, has motivated investigations into new methods of reducing and, if possible, preventing these harmful emissions [2]. An increasing awareness of these emissions has resulted in legislation requiring stringent enforcement of new regulations having the goal of improving the quality of the environment [2]. As a result, many conventional techniques were proposed to remove VOCs such as, ozone oxidation [4], incineration[5], combustion [6], adsorption [7], absorption and photocatalysis [3, 8,14, 39, 40, 42-44].

Photocatalysis is an heterogeneous process between a solid phase (catalyst) containing a semiconductor usually titanium dioxide (TiO_2) and the gas phase [9, 40, 42, 43]. The catalyst is activated by photons provided by an ultra violet (UV) radiation (sunlight or UV lamps) [10-12, 14, 44]. This technique has proven its ability to mineralize a large number of VOCs with low energy consumption [9, 13]. Thus it appears to be a promising process for remediation of air polluted by VOCs. Heterogeneous photocatalysis using TiO_2 has several advantages: (i) the catalyst is cheap, (ii) it operates at ambient temperature, (iii) the byproducts are usually CO_2 and H_2O , (iv) no other chemical reagent is needed.

Recently, the Nonthermal plasma (NTP) has been investigated, first time, by many researchers for various applications such as removal of pollutants. The main advantage of these non equilibrium plasmas consists in the ability to generate high-energy electrons, while keeping the background gas close to room temperature[15]. Thus, a highly reactive environment is created without spending energy on gas heating as in thermal processes [15, 16]. The energetic electrons excite, dissociate and ionize the gas molecules producing chemically active species[17].

In recent years, plasma dielectric barrier discharge (DBD) has been investigated for the abatement of volatile organic compounds including methanol [40], benzene [18], dimethylamine [19], toluene [20, 21]and hydrogen sulfide [22].

The use of a catalyst in the plasma zone was reported to improve the efficiency in VOC removal and CO_2 formation [30, 32, 37, 40]. The goal of this study was to try to combine the advantages of photocatalysis and NTP by combining the two technologies in the same reactor which should be able to treat larger flowrate than the laboratory reactors usually used. Moreover, we can expect to observe a synergy effect by combining volumic plasma with photocatalyst in a small reactor at flowrate equal to $200 \text{ mL} \cdot \text{min}^{-1}$ [24, 26].

A coupled system of surfacic plasma/photocatalysis in pilot reactor is established in the present work to study the effect of adding UV external on the pollutant degradation and byproducts formation. 3-methylbutanal (3MBA) and trimethylamine (TMA) were chosen as target pollutants since these compounds were main molecules detected in the exhaust gases from animal quartering centers.

2. Experimental details

2.1. Reactor design and setup details

The planar reactor consists of a rectangular cross section (135mm×135mm) and is 1m length. It is made of polymethyl methacrylate (PMMA) material. Two plates, 4mm thickness, are arranged parallel to the length of the reactor and permit to hold up the catalyst media and the two electrodes. The distance between the two plates, which is also the air gap, can be modified. The planar photocatalytic reactor was equipped with eight UV lamps in order to ensure a good radiation distribution (Fig. 1). The length of the irradiated zone is 0.8m. The photocatalytic support surface is equal to 0.19 m². The used fluorescent UV lamp (Philips under reference PL-S 9W/10/4P, 0.012m bulb diameter, 0.135m bulb length) had a major wavelength peak emission at 355nm. The centerlines of the lamps were separated by a distance of 0.01m.

The design of this reactor (Figure.2) was the subject of a Patent Application (BFF 11L1040/GB) [27].

The nonthermal plasma, of surface dielectric barrier type, is generated by a 2 mm thickness grid with wire electrodes shaped as a rectangle. The distance between two wire electrodes was 20 mm. The outer electrode, connected to the ground, is a 1 mm thick and 80 cm length copper foil. The electrodes were attached around the glass plate which its thickness (4 mm) corresponded to the distance between them. The applied high voltage is about 30 kV/40 mA and is a sine waveform. It was delivered by a TREK_30kV high voltage amplifier coupled with a generator BFi OPTILAS.

Figure 1: sectional drawing (a) and Schema (b) of plasma SDBD coupled with photocatalysis in planar reactor.

The applied voltage to the plasma SDBD was measured with a 1000:1 high voltage probe (North Star SN_1704010). The NTP was obtained by submitting the electrodes to a sinusoidal electric high voltage ranging from 0 to 30 kV at a 50 Hz frequency. A 2,5 nF capacitance (C_m) was positioned between the outer electrode and the ground connection in order to collect the charges transferred through the reactor. The applied voltage (U_a) and the high capacitance voltage (U_m) were measured by LeCroy high voltage probes and recorded by a digital oscilloscope (Lecroy Wave Surfer 24 Xs, 200 MHz). A schematic illustration of the plasma SDBD setup is shown in Fig.2.

(a) (b)
Fig 2: (a) General scheme for coupling plasma SDBD and photocatalysis, (b) photographs of plasma SDBD in planar reactor.

2.1. Polluted flow generation

A centrifugal compressor is used with ambient air. The flow rate is controlled by a flow meter (Bronkhorst In-Flow). 3MBA(>99.7%, Sigma–Aldrich, Switzerland) and TMA(50wt. % solution in water, Sigma–Aldrich, Switzerland) were used. Each pollutant is continuously injected by means of a syringe/syringe driver system (Kd Scientific Model 100) through a septum into the gas stream and a heating system covering the injection zone sets the gas temperature and facilitates the VOC vaporization ahead of the static mixer (Fig.3).

Figure 3: Schematic view of the experimental setup

2.2. Apparatus and Analysis

For the analysis, a FISIONS Gas chromatograph coupled with a flame ionization detector (GC-FID) is used. 3MBA and byproducts separation are performed by a Chrompack FFAP-CB column (25 m of length 0.32 mm of external diameter 0.32mm), which is specially adapted for volatile fatty acids. Nitrogen gas constitutes the mobile phase. The identification of byproducts is done by Gas Chromatograph-Mass spectrometer (GC-MS) (Thermo Scientific) equipped with an infrared (IR) detector. Under these conditions, the detection limit of 3MBA and formed byproducts was 0.02ppmv. All injections are performed manually and repeated three times with a syringe of 500 μ l. Analysis conditions are as follows (Table 1).

Table 1: Analysis conditions for the gas chromatograph

A standard iodometric titration method was used to estimate the formation of the downstream ozone. Thus, at the outlet of the plasma reactor a constant flow rate of 200 L/h was bubbled on iodine solution. The CO₂ has been analyzed by a Fourier Transform Infrared (FTIR) spectrophotometer brand Environnement SA (Cosma Beryl reference 100). CO concentrations were measured by CO ZRE gas analyzer. Temperature and relative humidity were measured with a TESTO 445 probe.

2.3. Photocatalytic material

The used material is a coated Glass Fiber Tissue (GFT) with 6.5 g/m² of colloidal silica to ensure the fixation of 6.5 g/m² of P25-Degussa titanium dioxide nanoparticles. It is supplied by Ahlstrom Research and Services. P25-Degussa nanoparticles were made of two titanium dioxide allotropic forms, 80% is anatase, 20% is rutile. The coating process consists of an impregnation of glass fibers by SiO₂ and TiO₂ nanoparticles suspension in pure water using Ahlstrom industrial size-press. Specific surface area was measured according to BET method and was equal to 20.6 m² g⁻¹. Preparation process is precisely described in the study of Enriquez and co-workers [14] and Ahlstrom Patent [28].

3. Results and Discussion

The average temperature was equal to 20 °C. It should be noted that, whether the UV lamp could potentially heat up the air, the measured outlet temperature of the gas never exceeds the above-mentioned value. This is due to the nature of the open continuous reactor where the air-flow evacuates the heat.

3.1. Removal of 3-methylbutanal

The VOC Removal Efficiency (RE) is defined as:

$$RE(\%) = \frac{C_{in} - C_{out}}{C_{in}} \times 100 \% \quad (1)$$

Where C_{in} and C_{out} are the inlet and outlet concentration of 3MBA (mg.m⁻³) respectively.

Moreover we use the Lissajous plot method (Manley, 1943) for calculating mathematically the power input (P) (eq.2).

$$P (W) =E (J) \times F (Hz) \quad (2)$$

Where P is the input power (W), E is the injected energy (J) and F is the frequency (Hz). The value of input power is varied by changing the applied voltage (Ua). In fact, the injected energy (E) per cycle dissipated in the DBD reactor is equal to the area of Lissajous curve (Fig.2).A Lissajous curve was obtained by plotting the charges transferred by the plasma versus the voltage applied to the reactor, as shown in figure 2.

The quantity of charges Q (μC) transferred by the discharge was measured by multiplying the capacitance C_m(nF) by the applied voltage U_a (kV) in the plasma SDBD reactor [45].

In the case of fig.2, the discharge power was estimated to be 6 W.

After the specific energy (SE) is then calculated as:

$$SE(J/L) = P(W) / [1000 \times Q(m^3/h)/3600] \quad (3)$$

Where SE was the specific energy (J/L), Q was the flowrate (m³/h).

Figure 4: Lissajous curve obtained at 50 Hz.

3. Results and discussion

The main target of this work was to study the removal of 3MBA by plasma coupled with TiO₂ without external UV in order to investigate the effect of UV light from the SDBD reactor in TiO₂ activation.

The effects of several parameters, such as specific energy (SE), residence time in the reactor and inlet concentration on the contaminant removals were investigated.

The domain of gas flowrate, inlet concentration tested, UV intensity, and the applied voltage of plasma SDBD were summarized in Table 2.

Table 2: Parameters of plasma DBD+TiO₂/UV reactor

3.1. Influence of UV generated by plasma on TiO₂

3.1.1. On removal of 3-methylbutanal

During the present study, concentration of 3MBA was kept constant (50 mg.m^{-3}) in order to understand the influence of SE on the performance of the reactor. Moreover, the applied voltage was varied between 12 and 29 kV that corresponds to SE of 5 and 16 J.L^{-1} , respectively. As seen from Fig. 5, with the two processes (plasma only and plasma with TiO_2 without external UV), removal of 3MBA increases with increasing the SE. In fact, the radicals and the excited species which were produced by the energetic electrons in the discharge phase could efficiently oxidize 3MBA and accordingly improved the RE of 3MBA. This result is in agreement with works on plasma SDBD removal of methanol [40], acetylene [23] and toluene [20, 21].

On the other hand, Fig. 5 shows that the RE of 3MBA was not enhanced in presence of photocatalyst without external UV. So, the UV light from the plasma SDBD was very weak to activate the TiO_2 . Its contribution to the removal of 3MBA in plasma SDBD/photocatalysis combination reactor could be ignored. Similar results have been reported in the literature for some VOCs [23, 24].

Figure 5: Dependence of RE on SE in situ in different plasma systems without external UV ($[3\text{MBA}] = 50 \text{ mg m}^{-3}$, $Q = 10 \text{ m}^3 \text{ h}^{-1}$, $T = 20 \text{ }^\circ\text{C}$, $\text{RH} = 50\%$).

3.1.2. On selectivities of CO and CO_2

The CO_2 overall selectivity (CO overall selectivity can be also defined) may be a useful parameter to assess the performance of the plasma SDBD towards 3MBA removal. It allows estimating the mineralization rate i.e. the ultimate reaction step, of each process of oxidation.

The CO_x selectivity is expressed as follow (eq. 4):

$$\{\text{CO}_x \text{'s overall selectivity (\%)}\} = \frac{[\text{CO}_x]_{\text{out}} - [\text{CO}_x]_{\text{in}}}{5 \times [3\text{MBA}]_{\text{in}} \times \{\% \text{ RE}\}} \times 10^4 \quad (4)$$

where $x = 1$ for CO and $x = 2$ for CO_2 . $[\text{CO}_x]_{\text{in}}$ and $[\text{CO}_x]_{\text{out}}$ were the inlet and outlet concentration of carbon mono/dioxide respectively (ppmv). $[3\text{MBA}]_{\text{in}}$ was the inlet concentration of 3MBA (ppmv). The number 5 was the stoichiometric coefficient of the removal reaction.

Figure 6.a: Variation of CO and CO₂ selectivities vs. the SE using two processes without external UV: empty symbol = selectivity of CO₂ and full symbol = selectivity of CO ([3MBA] = 50 mgm⁻³, Q = 10m³h⁻¹, T= 20 °C, RH = 50%).

Fig. 6.a shows the selectivity of CO_x (CO and CO₂). As seen, the selectivity of CO_x was bad and never close to 100%. In fact, the selectivity to CO₂ was around 19 % at 16 J.L⁻¹. Moreover, we note that the increase of SE leads to an increase of overall selectivities. This is due to more electrons and reactive species (such as [•]O and [•]OH) which were formed when the SE increased and then much molecules of 3MBA were oxidized into CO₂ and CO [26, 40, 46]. In fact an increase in SE from 5, 2 to 16 J.L⁻¹ leads to CO and CO₂ overall selectivity increased from 3 to 12 % and from 9 to 19 %, respectively. These results are in agreement with works on removal of methanol [40], acetaldehyde [30] and acetylene [26, 31].

We can also note that the presence of photocatalyst on the plasma zone, does lead to more mineralization.

The others byproducts in the exit of reactor were identified and evaluated. To evaluate the validity of the analysis method i.e. to be sure that the majority of byproducts were detected, mass carbon balance was estimated (fig.6.b).

In fact, mass carbon balance CB (%) was calculated from the sum of acetone (CH₃COCH₃), acetic acid (CH₃COOH), CO₂ and CO as follows:

$$CB(\%) = \frac{[CH_3COOH] + [CH_3COCH_3] + [CO_2] + [CO]}{5 \times [3MBA]^{in} \times \left\{ \% IRE \right\}_{Isov}} \times 100\% \quad (5)$$

where [CH₃COOH], [CH₃COCH₃], [CO] and [CO₂] were respectively the concentration of acetic acid, acetone, carbon monoxide and carbon dioxide (ppmv). Figure 6.b shows that with these processes the mass carbon balance was achieved. This means that the majority of organic byproducts are detected. Moreover, we obtained the same byproducts using two processes without external UV.

Fig.6.b. Variation of mass balances and byproducts of 3MBA with residence time using plasma alone and plasma with TiO₂ ([3MBA] = 50 mg m⁻³, Q = 10m³ h⁻¹, T= 20 °C, RH = 50%).

3.1.3. On the ozone formation

Ozone is an inevitable byproduct in a NTP. Atomic oxygen was generated by O_2 dissociation due to impact with high energy electrons (reaction 1).

Atomic oxygen is a strong oxidizer, but its stability is very limited. Due to fast recombination processes, the lifetime is only a few microseconds at atmospheric pressure [4, 16, 38, 39]

Atomic oxygen reacts successively with O_2 in three-body collisions, forming ozone by the following reaction:

where M can be either molecular oxygen or molecular nitrogen [4].

As seen from Fig 7, when the SE increases, the quantity of ozone increases as well. That could be explained by the fact that more electrons and reactive species (such as $\cdot O$) were formed and then leads to ozone production (reactions 1 & 2) [16, 38, 39].

Figure 7: Dependence of the ozone formation on SE on in situ under different plasma systems without external UV ($[3MBA] = 50 \text{ mg m}^{-3}$, $Q = 10 \text{ m}^3 \text{ h}^{-1}$, $T = 20 \text{ }^\circ\text{C}$, $RH = 50\%$)

Moreover, it is interesting to note that the presence of photocatalyst without external UV surface enhances the quantity of ozone in the outlet flow. Thus, this experiment illustrates that the active species generated ($\cdot O$) by plasma are able to react with other species like fibers of TiO_2 than to recombine with oxygen molecules for forming ozone (reaction 2). This result is similar to the work of Allegraud [32].

3.2. Combination of plasma-photocatalysis with external UV

The UV light generated by plasma SDBD is very weak to activate the TiO_2 . Its contribution to the 3MBA removal by plasma SDBD/photocatalysis combination reactor could be ignored. Thus, we introduced eight external UV light into the planar reactor to activate the photocatalyst media. Moreover, 3MBA removal experiments were carried out under three

configurations: photocatalysis ($\text{TiO}_2 + \text{UV}$), plasma and plasma SDBD/photocatalysis coupling (Plasma SDBD/ $\text{TiO}_2 + \text{UV}$). The removal efficiency, mineralization and by-products formation are determined.

It is important to note that without photocatalyst media, 3MBA removal is not affected by UV radiations.

3.2.1. On the removal efficiency

On Figure 8, the variation of 3MBA removal efficiency, by coupling process, as a function of the sum of removal efficiency due to plasma and photocatalysis is represented.

We can see that 3MBA removal by coupling plasma and photocatalysis was about 5 to 15% higher than the sum of the conversions recorded, under the same conditions, for plasma and photocatalysis alone.

For example, when $[\text{3MBA}] = 50 \text{ mgm}^{-3}$ and $Q = 4 \text{ m}^3 \cdot \text{h}^{-1}$, by photocatalysis alone, the removal efficiency of 3MBA was around 25 %. When NTP alone ($\text{SE} = 13.7 \text{ J} \cdot \text{L}^{-1}$) was used, the 3MBA removal reaches to 48 %. By coupling plasma SDBD and photocatalysis, the 3MBA removal increased to 83% (10% higher than the contribution of each process).

This synergetic effect was observed under various experimental conditions (Fig.8)

This synergy may be assigned to:

- The contribution of reactive species, formed by plasma SDBD, in photocatalytic mechanisms [23, 37, 40].
- The desorption of by-products attached at TiO_2 surface by plasma. This leads to renewal of catalytic surface and so improves conversion and mineralization processes [24, 36]

Figure.8: 3MBA removal efficiency by coupling process vs the sum of removal efficiency of plasma and photocatalysis at different residence time, inlet concentration and specific energy in planar reactor ($T = 20^\circ \text{C}$, $\text{RH} = 50\%$, $I = 20 \text{ W} \cdot \text{m}^{-2}$).

So as to better understand the presence of synergetic effect with plasma and photocatalysis, others experiments with TMA were carried out.

Figure 9 shows the variation of the TMAremoval with flowrate using the three configurations at SE=13 J.L⁻¹.

Figure 9: TMAremoval with flow rate for the different tested configurations (SE=13 J.L⁻¹, [TMA] = 145 mg/m³, RH=50%, T= 20 °C).

On the other hand, figure 9 illustrates the results for TMAremoval for the photocatalysis alone (UV), plasma SDBD alone (without TiO₂) and for the coupling of plasma SDBD and photocatalysis. By photocatalysis alone (irradiation of TiO₂ by external UV light), 24% of the TMA was removed. When plasma SDBD was used alone and at Q= 4 m³.h⁻¹, the TMA removal reaches to 36% without photocatalyst.

By coupling plasma SDBD and photocatalysis, the TMAremoval increased to 74%. Thus, the TMA removal by coupling plasma SDBD and photocatalysis was 14% higher than the sum of the removals recorded at the same conditions for plasma SDBD alone and photocatalysis alone. With this pollutant, we note that the synergistic effect was higher than that with 3MBA. Thus, whatever the pollutant was used, experimental results when plasma SDBD and photocatalysis were combined show a better efficiency in removal than the simple addition of the two processes, revealing then a synergy effect which it appears for all the values of tested flowrate.

3.2.2. On the selectivity of CO₂

The CO selectivity can be considered as negligible for plasma and plasma SDBD /photocatalysis coupling processes.

We note that, with photocatalysis alone the final concentration of CO was lower than the detection limits of CO ZRE analyzer (<0.05ppmv). This result is in agreement with works on photocatalytic degradation of fatty acids [33], cyclohexane [34] and trichloroethylene (TCE) [9]. On other hand, CO detection could be obviously affected by the residence time under otherwise identical conditions. In fact, with decomposition of gas-phase dimethyl methylphosphonate [46], photocatalysis alone can produce a very low amount of CO.

CO₂ selectivity for the photocatalysis alone (UV), plasma SDBD alone and for the coupling processes is presented in figure 10. One can note that when combining the two processes

carbon dioxide selectivity was improved compared to plasma SDBD alone whatever is the value of SE.

By photocatalysis alone, the selectivity of CO₂ was around 59%. When plasma SDBD alone was used the CO₂ selectivity is 19 % at SE = 16 J.L⁻¹. But by coupling these technologies, the CO₂ selectivity is about 40%, an intermediate value between photocatalysis alone and plasma SDBD alone.

Thus, total mineralization by TiO₂ photocatalysis is well-known.

Fig 10: Variation of the overall selectivity of CO₂ vs. SE using the three processes([3MBA] =50 mg.m⁻³, Q = 10m³.h⁻¹, T= 20 °C, RH=50%, I= 20 W.m⁻²).

We note that with photocatalysis alone and plasma SDBD/photocatalysis coupling processes, the detected byproducts are propionic acid, acetone and acetic acid. We note that with plasma alone, the detected byproducts are acetone and acetic acid.

3.2.3. On ozone formation

The residual ozone concentration at the reactor exit for each process (plasma alone and the combined process) is represented in figure 11. The result proves that the amount of ozone formed by plasma SDBD alone is higher to that due to the combined plasma SDBD/TiO₂+UV. These results suggest that UV can play a role either in inhibiting the ozone formation or in ozone decomposition [38, 40].

Thus, this experiment illustrates that the active species generated ([•]O) by plasma are able to more oxidize 3MBA and also to react with oxygen molecules for forming ozone [37-40].

Using the study result of Taranto and co-workers [40] the activation of TiO₂ by UV radiation can reduce the formation of ozone or favor its destruction by the following reaction [9, 38, 40]:

Atomic oxygen thus-formed can play a role in the removal of 3MTBA. This result is in agreement with work of methanol removal [40].

We note that photocatalyst reactor alone does not produce ozone.

Figure 11: Variation of amount of ozone with the SE using two processes ([3MBA]= 50 mg.m⁻³, Q = 10m³.h⁻¹, T= 20 °C, RH = 50%, I= 20 W.m⁻²).

In order to more investigate this ozone behavior, the planar reactor was operated in two parts: the first part was with plasma SDBD alone and the second part with photocatalytic process (TiO₂ + UV). The quantification of the ozone was done at the outlet of each part.

The result shows that the amount of ozone was reduced when TiO₂ catalyst is irradiated by UV (fig. 12).

At SE equal to 16 J.L⁻¹, the ozone concentration in the first part is 61 ppmv and decreases to 48 ppmv at the exit of the reactor (the second part). The same behavior is seen with SE equal to 9 J.L⁻¹. These results show that UV irradiation is able to promote ozone elimination. Ozone can also contribute to 3MBA removal on the photocatalytic surface [40].

This behavior is another reason to explain the synergetic effect between plasma SDBD and photocatalysis.

Figure 12: Variation of amount of ozone with the SE using two parts of planar reactor([3MBA]= 50 mg.m⁻³, Q = 10m³.h⁻¹, T= 20 °C, RH = 50%, I= 20 W.m⁻²).

4. Conclusions

The goal of this paper was to compare the behavior of 3MBA removal when catalysis (TiO₂ without external UV) and plasma SDBD are combined, to each process taken separately in order to determine whether or not a synergy effect was present. Our result showed that the UV light from the SDBD reactor was very weak to activate the TiO₂. Its contribution to the removal of 3MBA in plasma SDBD/photocatalysis combination reactor could be ignored.

For each operating parameter, we had unambiguously shown that a synergetic effect for the 3MBA and TMA removal can be observed when NTP is coupled with TiO₂ catalyst irradiated by external UV.

The behavior of combining plasma SDBD and photocatalyst in the same planar reactor had shown that the ozone can be easily decomposed.

409

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Table:Table 1: Parameters of plasma SDBD+TiO₂/UV reactor

Parameter	Value & domain
Gas temperature	Ambient (293 K)
Gas pressure	Atmospheric pressure (1 atm)
Relative humidity	50±5 %
Applied voltage	12 to 29 kV
Gas flowrate	4 to 10 Nm ³ h ⁻¹
Inlet concentration	50 to 100 mg m ⁻³
UV intensity	20 W m ⁻²

Table 2:Analysis conditions for the gas chromatograph

Gas pressure			Zone temperature	
N ₂ (gas carrier, kPa)	H ₂ (kPa)	Air (kPa)	Injector (°C)	Oven (°C)
105	40	100	110	50

Figures:

Figure 1: Schema (b) and sectional drawing (a) of plasma SDBD coupled with photocatalysis in planar reactor.

Figure 2: (a) General scheme for coupling plasma SDBD and photocatalysis, (b) photographs of plasma SDBD in planar reactor.

Figure 3: Schematic view of the experimental setup

Figure 4: Lissajous curve obtained at 50 Hz.

Figure 5: Dependence of RE on SE on in situ in different plasma systems without external UV ([3MBA] = 50 mg m⁻³, Q = 10 m³ h⁻¹, T= 20 °C, RH = 50%).

Figure 6.a: Variation of CO and CO₂ selectivities vs. the SE using two processes without external UV: empty symbol = selectivity of CO₂ and full symbol = selectivity of CO ([3MBA] = 50 mg m⁻³, Q = 10 m³ h⁻¹, T= 20 °C, RH = 50%).

Figure 6.b. Variation of mass balances and byproducts of 3MBA with residence time using two processes without external UV ([3MBA] = 50 mg m⁻³, Q = 10 m³ h⁻¹, T= 20 °C, RH = 50%).

Figure 7: Dependence of the ozone formation on SE in situ under different plasma systems without external UV ([3MBA] = 50 mg m⁻³, Q = 10 m³ h⁻¹, T= 20 °C, RH = 50%)

Figure.8: 3MBAremoval efficiency by coupling process vs the sum of removal efficiency of plasma and photocatalysis at different residence time, inlet concentration and specific energy in planar reactor (T= 20 °C, RH = 50 %, I= 20 W.m⁻²).

Figure 9: Trimethylamine conversion with flow rate for the different tested configurations (SE=13 J.L⁻¹, [TMA] = 145 mg/m³, RH=50%, T= 20 °C).

Figure 10: Variation of the overall selectivity of CO₂ vs. SE using the three processes ([3MBA] =50 mg.m⁻³, Q = 10 m³.h⁻¹, T= 20 °C, RH=50 %, I= 20 W.m⁻²).

Figure 11: Variation of amount of ozone with the SE using two processes ([3MBA] = 50 mg m⁻³, Q = 10 m³.h⁻¹, T= 20 °C, RH = 50 %, I= 20 W.m⁻²).

Figure 12: Variation of amount of ozone with the SE at exits of plasma alone and combined process in planar reactor ([3MBA] = 50 mg .m⁻³, Q = 10 m³.h⁻¹, T= 20 °C, RH = 50 %, I= 20 W.m⁻²).

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Figure 7: Dependence of ozone formation on the SE in situ under different plasma systems without external UV ($[3\text{MBA}] = 50 \text{ mg m}^{-3}$, $Q = 10 \text{ m}^3 \text{ h}^{-1}$, $T = 20 \text{ }^\circ\text{C}$, $\text{RH} = 50\%$)

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663 Figure.8: 3MBA removal efficiency by coupling process vs the sum of removal efficiency of
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