Morphogenesis and propagation of complex cracks induced by thermal shocks
Blaise Bourdin, Jean-Jacques Marigo, Corrado Maurini, Paul Sicsic

To cite this version:

HAL Id: hal-00911118
https://hal.archives-ouvertes.fr/hal-00911118
Submitted on 28 Nov 2013

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L’archive ouverte pluridisciplinaire HAL, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d’enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.
Morphogenesis and propagation of complex cracks induced by thermal shocks

Blaise Bourdin, Jean-Jacques Marigo, Corrado Maurini, and Paul Sicsic

1Department of Mathematics and Center for Computation & Technology, Louisiana State University, Baton Rouge, LA 70803, USA
2Laboratoire de Mécanique des Solides (UMR-CNRS 7649), École Polytechnique, 91128 Palaiseau Cedex
3Institut Jean Le Rond d’Alembert (UMR-CNRS 7190), Université Pierre et Marie Curie, 4 place Jussieu, 75252 Paris, France
4Institut Jean Le Rond d’Alembert (UMR-CNRS 7190), CNRS, 4 place Jussieu, 75252 Paris, France
5Lafarge Centre de Recherche, 95 Rue de Montmurier 38290 St-Quentin-Fallavier, France

(Dated: November 28, 2013)

We study the genesis and the selective propagation of complex crack networks induced by thermal shock or drying of brittle materials. We use a quasi-static gradient damage model to perform large scale numerical simulations showing that the propagation of fully developed cracks follows Griffith criterion and depends only on the fracture toughness, while crack morphogenesis is driven by the material’s internal length. Our numerical simulations feature networks of parallel cracks and selective arrest in two dimensions and hexagonal columnar joints in three dimensions, without any hypotheses on cracks geometry and are in good agreement with available experimental results.

PACS numbers: 46.15.Cc 62.20.mt

Complex crack patterns are ubiquitous in nature and in technology applications. Yet the theoretical understanding and predictive numerical simulation of how and when complex crack patterns arise (nucleation) and how they evolve (crack propagation) is fraught with challenges. Although approaches based on phase fields [1] or variational regularizations [2] have led to significant advance in the numerical simulation of complex crack patterns, short of introducing initial flaws at the structural scale [3], prescribing ad-hoc stress criteria [4], or accepting global energy minimization arguments whose physical relevance is debated [5–7], the predictive understanding of crack nucleation is still an elusive goal.

It is well-accepted that while Griffith-like models are appropriate for crack propagation at the scale of a structure, they are inadequate for the modeling of crack nucleation in brittle materials. Arguably, finer models, where a microscopic (material) length scale plays a fundamental role, are necessary to determine the critical load and crack geometry at the onset, especially in situations where complex crack patterns arise straight from the nucleation. The consistent combined modeling and numerical simulation of crack nucleation and propagation from the material to the structural length-scale is a challenging and largely open issue.

In this Letter, we study the morphogenesis and the selective growth of complex crack patterns induced by material shrinking under thermal shock. We report unprecedented quantitative agreement between numerical simulations, a theoretical model, and experiments at scales spanning from the material internal length to the structural length-scale. Our numerical simulations predict key features of fracture patterns observed in experiments, such as the formation of periodic patterns and the scaling laws governing their selective propagation in two and three dimensions, and do not require any a priori hypotheses on cracks geometry. The method we use leverages recent progress in the understanding of the links between damage models [10, 11] and the variational approach to fracture [2, 12]. It is based on a rate-independent gradient damage model with stress-softening based on two material parameters: the fracture toughness which rules the evolution of fully developed cracks, and the material’s internal length.

FIG. 1: (color online). Full scale numerical simulation of a ceramic slab submitted to a thermal shock. (a) Damage field from the numerical simulation (blue $\alpha = 0$, red $\alpha = 1$). (b) Experimental results from [8, FIG. 5(d)]. (c) Average crack spacing $d$ as a function of their depth $a$ for (a) and (b). The solid line is an approximate scaling law obtained in [9] by imposing a period doubling condition on a Griffith model. Here $\ell = 46 \mu m$ is the material internal length, $\ell_0 = G_c / (E\beta^2 \Delta T^2) = 14 \mu m$ the Griffith length (loading parameter), $2L = 9.8 \text{ mm}$ the total depth of the slab. See FIG. 2 for the meaning of the distributed damage zone.
which controls the initial stages of crack nucleation.

We investigate the thermal shock of a brittle ceramics, a now classical experimental setup [3, 13, 14] where a sample initially at a uniform temperature $T_0$ is quenched in a cold bath at temperature $T_0 - \Delta T$. We consider a rectangular slab $\Omega$ exposed to the thermal shock through its thin faces only. We focus first on very thin slabs, which we represent by a two-dimensional body in plane stress. We assume that within the range of temperatures involved, the material properties remain constant. Denoting by $\mathbf{u}$ the displacement field and $\varepsilon = (\nabla \mathbf{u} + \nabla^T \mathbf{u})/2$ the linear strain tensor, we consider for the sound material a linear elastic behavior of energy density $\psi_0(\varepsilon) = A_0(\varepsilon - \varepsilon^{th}_0) \cdot (\varepsilon - \varepsilon^{th}_0)/2$ where $A_0$ is the isotropic elastic stiffness tensor. The inelastic deformation induced by the time-dependent temperature field $T_i$ is $\varepsilon^{th}_t = \beta(T_i - T_0)\mathbb{I}$, where $\mathbb{I}$ is the identity matrix. The index $t$ is meant to highlight the dependence on time. We neglect the cracks influence on heat transfer so that the temperature field $T_i$ solves the heat equation $\partial_t T_i - k_0 \nabla^2 T_i = 0$ on $\Omega$. Phase changes, non-uniform convection and other nonlinear aspects of the heat exchange between the fluid and the sample are neglected by assuming that the temperature of the domain boundary exposed to the thermal shock is constant and equal to that of the water bath, i.e. $T_i = T_0 - \Delta T$. Inertial effects are not considered because the diffusion velocity of the temperature field is much slower than the wave speed in the material at the relevant scales in time and space. This hypothesis is universally accepted in the literature on thermal shock problems [3, 4, 9, 14, 15]. We model material failure using a gradient damage model characterized by the energy function

$$E_t(\mathbf{u}, \alpha) = \int_{\Omega} \left[ \frac{\psi_0(\varepsilon)}{s(\alpha)} + \frac{G_c}{c_w} \frac{w(\alpha)}{\ell} + \ell |\nabla \alpha|^2 \right] d\mathbf{x}, \tag{1}$$

where $\alpha$ is a scalar damage field varying between 0 (sound material) and 1 (fully damaged material), $G_c$ is the material’s fracture toughness, $\ell$ an internal length, and $c_w = \int_0^1 \sqrt{w(s)} ds$ a normalization constant. In a time-discrete setting, the quasi-static evolution is obtained by solving at time $t_i$ the following minimization problem $\min_{\mathbf{u}, \alpha \geq 0, \alpha_i} E_t(\mathbf{u}, \alpha)$, where the unilateral constraint on $\alpha$ enforces the irreversibility condition on the damage. The compliance function $s$ and the energy dissipation function $w$ should be chosen such that (1) converges as $t \to 0$ to a Griffith–like energy $\int_{\Omega} \psi_0(\varepsilon) d\mathbf{x} + G_c \mathcal{S}(\Gamma)$, where $\mathcal{S}$ is the surface measure of the crack $\Gamma$ [2, 16, 17]. In this model, material interpenetration in the fully damaged area is possible. In all the simulations presented here, it can be checked a posteriori that this issue does not present itself. Here, we use $s(\alpha) = 1/(1 - \alpha)^2$ and $w(\alpha) = \alpha$, a choice motivated by the convenience of its numerical implementation and specific analytical studies [11, 18]. With this choice the damage model has a stress-softening behavior and remains purely elastic without damage until the stress reaches the critical value:

$$\sigma_c := \frac{G_c E w'(0)}{2 c_w \ell s'(0)} = \sqrt{3G_c E \frac{\beta}{8\ell^2}}. \tag{2}$$

The relation above may be used to determine the numerical value of the internal length for a specific material from the knowledge of its elastic limit $\sigma_c$, Young modulus $E$, and fracture toughness $G_c$ [18]. The present model is in many aspects similar to the phase-field models of fracture developed independently [19]. Those with single-well dissipation potentials [1, 20] are in the form of (1) with $w(\alpha) = c(1 - g(1 - \alpha))$, where $g(\phi) = 4\phi^3 - 3\phi^2$. One significant difference is that while phase-field models typically involve some form of viscous regularizations, our formulation is rate-independent. In addition, the current literature based on phase-field models is concerned only with the propagation of a pre-existing cracks and does not consider the initiation problem.

The dimensional analysis of the energy (1) highlights three characteristic lengths: the geometric dimension of the domain $\ell$, the internal length $\ell$ and the Griffith length $\ell_0 = G_c/(E\beta^2 \Delta T^2)$. Using the material’s internal length as the reference unit, the problem can be reformulated in terms of two dimensionless parameters, the dimension of the structure $L/\ell$ (a geometric parameter) and the intensity of the thermal shock $\ell_0/\ell$ (a loading parameter). This is a significant departure from the classical Griffith setting where the only relevant parameter is $L/\ell_0$ [4, 5, 9].

Figure 1 compares the experiment from [8, FIG. 5(d)] (1 mm $\times$ 9.8 mm $\times$ 50 mm ceramic slab, $\Delta T = 380^\circ$C) with the damage field from a numerical solution of the gradient damage model. The material properties, communicated by the authors of [8] are $E = 340$ GPa, $\nu = 0.22$, $G_c = 42.47$ Jm$^{-2}$, $\sigma_c = 342.2$ MPa, and $\beta = 8 \times 10^{-6}$ K$^{-1}$, which using (2) gives $\ell = 46$ mm and $\ell_0 = 14$ mm. As our model is rate independent its solution are independent of $k_0$, up to a change of time scale. The numerical results are obtained through a finite element discretization and the approach of [2, 18, 21]. The main technical difficulties are the constrained minimization of a non-convex energy, and the need for a spatial discretization adapted to the material length-scale scale $\ell$. Cracks correspond to the localized bands where $\alpha$ goes from 0 to 1 and back to 0. The qualitative agreement between experiments and simulation is very good. In particular, our simulations reproduce the key phenomenon: the emergence of a periodic array of parallel short cracks at the initiation and their selective propagation toward the interior of the slab. Figure 1(c) shows a quantitative comparison between the numerical simulation of FIG. 1(a) and experimental data from [8] by plotting the average crack...
is a three-dimensional version of the simulation on a plate of thickness 1 mm, for in uniaxial and reaches its maximum value at the surface of the thermal shock. Since \( \sigma_{\text{max}} = E\beta\Delta T \)

The second series of simulations focuses precisely on the crack nucleation process and hence on short times. In this setting, one can assume that the domain is semi-infinite so that the geometric parameter \( L/\ell \) is infinite and the only parameter is the intensity of the thermal shock \( \ell_0/\ell \). For an undamaged material, the stress is uniaxial and reaches its maximum value \( \sigma_{\text{max}} = E\beta\Delta T \) at the surface of the thermal shock. Since \( \left( \frac{\sigma_{\text{max}}}{\sigma_c} \right)^2 = 3\ell/8\ell_0 \), for mild-enough thermal shocks \( \ell_0/\ell > 8/3 \), the critical stress is never reached and the solution remains elastic at all time. If \( \ell_0/\ell < 8/3 \), damage takes place at \( t^* \). At \( t = t^* \) the horizontally-homogeneous solution becomes unstable and the damage field develops oscillations of periodicity \( \lambda^* \) (FIG. 2(a)). An analytical solution for the damage field in the first stage of the evolution and its bifurcation and stability analysis is reported in [23], providing semi-analytical results for the periodicity \( \lambda^* \), the damage penetration \( D^* \), and the time \( t^* \) at the bifurcation. Here we perform several simulations varying \( \ell_0/\ell \) and detect the critical parameter at the bifurcation. In Figure 2(b) the numerical simulations (dots) are compared to [23] (solid lines). The good agreement provides an excellent verification of our numerical model. For severe shocks \( \ell_0 \ll \ell \), the results disclose a well-defined asymptotic behavior with \( \lambda^* \sim \sqrt{\ell_0/\ell}, \) \( D^* \sim \ell \), and \( t^* \sim \ell_0/\ell/k_c \). In this regime we observe numerically that all oscillations at the bifurcation develop in fully formed cracks (max \( \alpha = 1 \)), which is not the case for milder shocks \( \ell_0 \sim \ell \). However, the full post-bifurcation analysis remains an open problem at this time.

Experimental studies show that in three-dimensions cracks delineate cells with coarsening polygonal cross-sections [24]. Because of the complexity of the problem, the few available theoretical and numerical studies are based either on simplified two-dimensional models [25, 26] or on strong assumptions on the crack geometry [27]. The numerical simulation and analysis of the full three-dimensional problem is a major challenge for classical fracture mechanics tools and remains therefore largely unexplored.

![FIG. 2: (color online). Crack nucleation: (a) Damage field near the shock surface before (left) and after (right) bifurcation time \( t^* \) for \( \ell_0/\ell = 0.107 \) showing the bifurcation of a horizontally-homogeneous damaged band of depth \( D^* \) toward a periodic solution with wavelength \( \lambda^* \). (b) Wavelength, time and damage penetration in numerical simulations for several intensities of the thermal shock \( \ell_0/\ell \) (dots), compared to the semi-analytical results from [23] (solid lines).](image)

![FIG. 3: (color online). Three-dimensional version of the experiment from FIG. 1(b) showing the transition from two to three-dimensional crack patterns. The simulations are performed on a subdomain of dimension 5 mm × 1 mm × 1 mm and temperature contrast (a) \( 380^\circ\text{C} (\ell_0 = .27 \ell) \); (b) \( 480^\circ\text{C} (\ell_0 = 0.17 \ell) \); (c) \( 580^\circ\text{C} (\ell_0 = 0.12 \ell) \); (d) \( 680^\circ\text{C} (\ell_0 = 0.08 \ell) \).](image)
shows a fully tri-dimensional crack pattern using a classical Griffith-based model requiring an explicit description of the crack surface and its propagation criterion would be prohibitively complex. Instead, our three-dimensional computations are performed through a straightforward extension of the discretization and minimization algorithm for the energy of fracture. Obtaining an accurate scaling law for the cell diameter as a function of the depth as the one of the two-dimensional case of Figure 1 would require simulations on larger domains which would rapidly become computationally prohibitive. Hence, we perform a series of numerical experiments by fixing the loading \( \ell_0 \) and by varying at the same time the internal length \( \ell \) and the domain size \( L \) so as to keep their ratio equal to \( L/\ell = 40 \). The number of elements is kept constant with a mesh size \( h = \ell/5 \). For each computation, we compute the average cell diameter \( d \) as a function of distance from the bottom edge \( a \) using a post-processing software. This process does not involve any adjustable parameter, yet our results match the two-dimensional scaling law of [9] over several orders of magnitude, leading us to conclude that the scale selection mechanism in two and three dimensions are identical. In addition, while the initial phase of the evolution depends strongly on \( \ell \), later time evolution of fully developed cracks at the structural is unaffected by this parameter, matching the general scaling law for a Griffith-based model. This finding is consistent with the properties of the energy functional \( E \), which is known to lead to a Griffith-type propagation criterion [17, 20, 28, 29].

Our simulations show that a purely quasi-static model based on energy minimization can fully explain the formation of imperfect polygonal patterns and their selective coarsening as “maturation” mechanism during propagation, a phenomenon sometimes attributed to non-equilibrium processes [24]. We show that a carefully chosen gradient damage model can be used to account simultaneously for the nucleation of complex crack patterns and their propagation following Griffith criterion. Further works will be carried on to perform a careful statistical analysis of the geometry of the 3D crack patterns and further comparisons to experimental results. The present
modeling framework has a general validity and can be applied to other domains including for example the formation of basalt columns with uniform cross-sectional diameters through the solidification of lava fronts [24] or shaping of biological systems as observed of the scales on the heads of crocodiles [30]. We are also considering stronger thermo-mechanical coupling including the effect of cracks on heat transfer as in [15, 31].

The authors wish to thank Yingfeng Shao for providing the experimental data used in FIG. 1. B.B. work was supported in part by the National Science Foundation grant DMS-0909267. Some numerical experiments were performed using resources of the Extreme Science and Engineering Discovery Environment (XSEDE), which is supported by National Science Foundation grant number OCI-1053575 under the Resource Allocation TG-DMS060014. J.J.M. and C.M. gratefully acknowledge the funding of the ANR program T-Shock OTP J11R087.

* Corresponding author

[18] See Supplemental Material at [URL will be inserted by publisher] for more details on the damage model, its numerical implementation, and the postprocessing methods.
[22] See Supplemental Material at [URL will be inserted by publisher] for the entire evolution from nucleation to crack selection.