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Micro-organism extraction from biological samples using DEP forces enhanced by osmotic shock

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On the road towards efficient diagnostics of infectious diseases, sample preparation is considered as the key step and remains a real technical challenge. Finding new methods for extraction of micro-organisms from a complex biological sample remains a major challenge prior to pathogen detection and analysis. This paper reports a new technique capturing and isolating micro-organisms from a complex sample. To achieve the segregation of pathogens and blood cells, dielectrophoretic forces applied to bioparticles previously submitted to an osmotic shock are successfully implemented within a devoted microfluidic device. Our device involves an electrode array of interdigitated electrodes, coated with an insulating layer, to minimize electrochemical reactions with the electrolyte and to enable long-time use. The electric field intensity inside the device is optimized, considering the insulating layer, for a given frequency bandwidth enabling the separation of bioparticles by the dielectrophoretic forces. Our predictions are based on analytical models, consistent with numerical simulations (using COMSOL Multiphysics) and correlated to experimental results. The method and device have been shown to extract different types of micro-organisms spiked in a blood cell sample. We strongly believe that this new separation approach may open the way towards a simple device for pathogen extraction from blood and more generally complex samples, with potential advantages of genericity and simplicity.

1 Introduction

The rapid detection and identification of pathogens in biological samples is a major challenge for microbiological diagnosis. Current diagnostic methods based on bacterial growth and pathogen analysis usually take between 1 and 3 days from sampling to results. In the particular case of sepsis, the initial concentration of bacteria in blood is extremely low¹ and the reference blood culture methods allow the detection of bacterial contamination within 1 to 3 days, with additional 2 days for identification and antibiotic susceptibility testing of the pathogen. In such conditions, the diagnostic test result is used as a confirmation for a therapeutic decision previously taken by the clinician according to other criteria. Several analytical methods have emerged in the past years that have the potential to recover a valuable information from a reduced quantity of pathogens.² Molecular-based methods – mostly quantitative Polymerase Chain Reaction (qPCR) – allow for the detection of a concentration as low as 10 bacteria in 1 mL blood in 2 hours.³ However, such methods remain

costly, complex, fragile and also blind to genetic evolutions of bacteria and very dependent of the purification quality of nucleic acids before amplification. Preparation methods that would rapidly decrease the sample complexity by extracting bacteria from their complex environment would open the way not only to more robust molecular tests, but also to a range of emerging analytical methods that may be simpler and/or provide phenotype-correlated information (mass spectrometry,⁴ optical spectroscopy^{5,6}). Some of these last methods can be very sensitive and could be applied without the time-consuming growth step of the primary sample. For example, several groups have shown the use of microspectroscopy, for single bacteria identification.^{7,8}

However, such methods are very sensitive to the chemical and particulate complexity of the raw samples and good separation of bacteria from the surrounding sample elements is a major challenge that is still poorly addressed by the scientific community. In the mean time, microfluidics and microtechnologies have shown their potential to handle complex biological samples.^{9,10} Management of sample preparation and cell sorting has been reported using a wide variety of methods, such as optical forces,^{11,12,13} magnetophoresis,^{14,15,16} acoustophoresis^{17,18,19} or electric forces.²⁰ Methods that rely on forces generated by an electric field gradient such as dielectrophoresis^{21,22,23,24} are expanding rapidly due to the emergence of micro-systems technology.

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Such methods provide several opportunities to cope with the lack of simple protocols for the sample preparation.

In this paper, we report a method based on the separation and concentration of pathogens from a complex biological sample, namely blood, using a dielectrophoresis (DEP) force in a highly hypotonic solution. The use of such an hypotonic solution as medium for the complex biological sample causes an osmotic shock. Taking advantage from the large tolerance of micro-organisms regarding osmotic shocks, selective lysis, or at least permeabilisation of eukaryotic cells - in particular leucocytes and erythrocytes - occurs in such conditions. This allows achieving the dielectrophoretic separation of micro-organisms versus blood cells with high efficiency.

In this paper we validate this concept, with experiments performed on a devoted microfluidic device. Two types of micro-organisms with very different structures, namely bacteria (*Escherichia coli*) and yeasts (*Candida albicans*), could be handled on the device, and separated from red and white blood cells using dielectrophoresis forces in low conductivity medium (deionized water). The structure of the device was optimised with analytical electric considerations and with numerical simulations performed with Comsol. In order to clearly understand the movement of cell populations under DEP forces, the experiments were carried out on elementary sample mixtures. These sample models demonstrate that the application of DEP forces, combined with an osmotic shock, could be used in a miniaturized fluidic device to separate micro-organisms from whole blood. The method should be robust so that separation may be achieved in a complex biological fluid. We think that this approach might provide disruptive solutions for in-vitro diagnostics of blood infections.

2 Extraction method using dielectrophoresis combined to an osmotic shock

The sorting method proposed in this paper is based on the dielectrophoresis force (DEP force), which occurs when polarisable particles are submitted to an AC electrical field gradient.²⁵ The time average DEP force on a spherical particle, in the case where the electrical field is stationary is:

$$\langle \vec{F}_{DEP} \rangle = 2\pi\epsilon_m r^3 \text{Re}[f_{CM}] \vec{\nabla} |E_{rms}|^2 \quad (1)$$

where r is the particle radius, ϵ_m is the permittivity of the suspending medium, $\text{Re}[f_{CM}]$ is the real part of the Clausius-Mossoti factor and E_{rms} is the root-mean-square electric field. The Clausius-Mossoti factor depends on the field frequency and on the electrical properties of the particle and surrounding medium, as shown in equation 2.

$$f_{CM} = \frac{\epsilon_p^* - \epsilon_m^*}{\epsilon_p^* + 2\epsilon_m^*} \quad (2)$$

where $\epsilon_p^* = \epsilon_p - j\sigma_p/\omega$ and $\epsilon_m^* = \epsilon_m - j\sigma_m/\omega$ are the complex permittivities of the particule and the medium, ω the electric field pulsation, ϵ_p , ϵ_m and σ_p , σ_m are the permittivities and the conductivities of the particule and the medium, respectively.

The sign of the DEP force is given by the sign of the real part of the CM factor. If the particle is more polarisable than the suspending medium, then $\text{Re}[f_{CM}]$ will be positive, and the force is towards the direction of the field gradient (positive dielectrophoresis or DEP+). Conversely if the particle is less polarisable than the medium, then $\text{Re}[f_{CM}]$ will be negative, and the particle moves oppositely to the gradient (negative dielectrophoresis or DEP-). Both polarisabilities depend on the electrical field frequency. In the case of positive DEP, the particle motion will be induced towards the local maxima of the applied electric field, and conversely towards the local minima of the applied electric field in the case of negative dielectrophoresis.

Therefore, to perform spatial DEP separation between two particles, both $\text{Re}[f_{CM}]$ must have opposite sign for a given frequency range. Such frequencies do not necessarily exist, mainly when dealing with biological cells in a physiological medium having a high electric conductivity.

An alteration of the physiological state of a cell can modify the evolution of the CM factor and can sometimes invert the sign of its real part. Indeed, DEP can be used to sort living from dead yeasts for example.²⁶ It is precisely from this observation that we developed our sorting strategy. By using a hypotonic medium, an osmotic shock is selectively induced on blood cells. This leads to biological modifications of the blood cells, such as membrane permeabilization, and CM factor modifications.

The use of the DEP effect to handle particles in suspension within a liquid shows to be relevant in microfluidic structures as it can provide forces several order of magnitude higher than the buoyancy force, and can compete with the fluidic forces. Indeed for a bacterium, a yeast or a lysed red blood cell (respective diameters = 2 μm , 6 μm and 7 μm) the sedimentation velocity v_s due to the buoyancy force reaches respectively $1.4 \cdot 10^{-3} \mu\text{m.s}^{-1}$, $1.3 \cdot 10^{-2} \mu\text{m.s}^{-1}$ and $2 \cdot 10^{-3} \mu\text{m.s}^{-1}$ (equation 3),²⁷ assuming the spherical shape of the cells.

$$v_s = \frac{2}{9} \frac{\rho_p - \rho_m}{\mu} g r^2 \quad (3)$$

where ρ_p and ρ_m are the mass densities of the particle and the

medium, μ the dynamic viscosity, g the standard gravity and r the particle radius. In the case of *E. coli*, its natural motility, which provides much higher velocities than v_s ,²⁸ has to be considered. Comparatively, the DEP-induced velocity of an *E. coli* reaches more than $200 \mu\text{m.s}^{-1}$.²⁷ Since the DEP force is proportional to the cell volume, this velocity is even higher in the case of yeast or blood cells. Finally when an external flow is applied during the DEP trapping experiment, the flow rate should not exceed this DEP-induced velocity to ensure an efficient capture.

However, when applying a non-uniform electric field, DEP is not the only force that can set particules in motion. AC electro-osmosis and electro-thermal effects are commonly discussed.^{29,30} We usually neglect these phenomena in our experiment interpretations because the passivation layer above the electrode pattern dramatically decreases the magnitude of these forces. Moreover, the frequencies we are working with for the binary sorting (several MHz) prevent AC electro-osmosis from interacting with DEP effects.

3 Material and methods

3.1 Device

Device design The DEP force cell sorting device is composed of an electrode array of interdigitated electrodes, coated with an insulating layer, and a microfluidic chamber (see figure 1a). The electrode array consists of 5 pairs of interdigitated electrodes (width=90 μm , gap= 10 μm). The electrodes are coated by an insulating silica layer to minimize electrochemical reactions with the electrolyte and to enable long-time use of the device.

Device fabrication The device was fabricated on a 4 inch silicon wafer, using standard photolithography techniques. A 1 μm silicon oxide layer is obtained by wet oxidation. Layers of titanium and gold (100 and 400nm, respectively) were successively deposited by sputtering. A 200nm thick silicon oxide passivation layer is then deposited by CVD (Chemical Vapor Deposition). Double-sided tape (30 μm thick) topped over the electrodes (Nitto Denko MC-2033) is used to design the sorting chamber. The chamber is finally closed with a coverglass to enable microscopic observation.

3.2 Electric Field Distribution : numerical simulation with ComsolTM

We numerically solved the electric field produced by interdigitated electrodes by using finite element analysis software (Comsol Multiphysics 4.1), taking the frequency of the electric signal into account. By solving Laplace equation, the calculated potential V is used to determine the electric field

($\vec{E} = -\vec{\nabla}V$) from which $\vec{F}_{dep}$ is calculated (proportional to $\vec{\nabla}|E|^2$). Antiperiodic boundary conditions were imposed on both sides of the simulated channel to take into account neighboring electrodes, while zero charge boundary condition was imposed at the top of the channel boundary.

Table 1 experimental parameters used for numerical simulations and analytical considerations (ϵ_0 is the vacuum permittivity)

e_p	l_{gap}	ϵ_p	ϵ_m	σ_m
200 nm	10 μm	$7,5\epsilon_0$	$80\epsilon_0$	10 mS.m ⁻¹

3.3 Analytical model of the passivation layer

To assess its effect on the electric field in the biological medium, the passivation layer is modeled as a capacitive element while the biological medium is approximated by a capacitive and a resistive elements in parallel (figure 1b). We can use the transfer function of this equivalent electric circuit to evaluate the field screening effect of the passivation layer (equation 4). Indeed, the screening effect, which is a function of the electrical frequency, is characterized by the ratio between the circulation of the effective electrical field in the biological medium, and the voltage applied to the electrodes.

$$\begin{aligned} H(j\omega) &= \frac{E_{medium} \cdot d}{U_{applied \text{ to the electrodes}}} \\ &= \frac{Z_m}{Z_m + 2Z_p} \end{aligned} \quad (4)$$

$$\text{with } Z_m = \frac{R_m}{1 + jR_mC_m\omega}, \quad Z_p = \frac{1}{jC_p\omega}, \quad R_m = \frac{1}{\sigma_m} \cdot \frac{l_{gap}}{h_m \cdot w_m},$$

$$C_m = \epsilon_m \frac{h_m \cdot w_m}{l_{gap}} \quad \text{and} \quad C_p = \epsilon_p \frac{h_p \cdot w_p}{e_p}$$

where the p and m indexes stand for the passivation layer and the biological medium respectively, l_{gap} is the mean equivalent path for the electric field between two electrodes, e_p the thickness of the passivation layer, h_m , h_p , w_m and w_p the characteristic length and width of the microchannel and the passivation layer respectively. Substitution of the expressions of Z_m and Z_p into equation 4 yields the expanded equation 5.

$$H(j\omega) = \frac{\frac{C_p R_m}{2} j\omega}{1 + \frac{R_m C_m}{2} (2 + \frac{C_p}{C_m}) j\omega} \quad (5)$$

3.4 Sample preparation

Bacteria. *Escherichia coli* (strain ATCC 35421) are grown overnight in 3mL Tryptic Soy Broth medium at 30°C. Then

a second culture at a 1:50 dilution in the same medium is performed for 2h at 37°C. The bacteria are washed twice with de-ionised water by centrifugation at 10 000 rpm during 5 min and resuspended in de-ionised water at a cell concentration of 5×10^8 colony-forming unit/mL (cfu/mL). The cell concentration is determined by optical absorbance at 550nm. We controlled bacterial viability in de-ionised water using standard plate-count method to enumerate viable bacteria.

Genetically modified *E. coli* cells (BL21) that produce Green Fluorescent Protein are also used : the fluorescence distribution makes the microscopic observation easier, namely when the electrode surface conditions are really poor.

Yeasts. Candida Albicans (strain ATCC 18804) are grown overnight in 10mL Sabouraud medium at 30°C. Then a second culture at a 1:50 dilution in the same medium is performed for 4h at 30°C. The yeasts are washed twice in de-ionised water by centrifugation at 10 000 rpm during 5 min and resuspended in de-ionised water at a cell concentration of 10^7 cfu/mL.

Red blood cells (RBC). Human blood is collected from anonymous healthy donors in EDTA vacuum tubes (BD vacutainer) provided by the French Blood Service. A 1mL sample containing 5×10^9 RBC/mL is centrifuged at 600g for 15 min in order to separate red blood cells from the plasma and the buffy coat. 10 μ L of the centrifuged solution of RBC at a concentration of 10^{10} cells/mL are then collected.

Cell mixtures. RBC suspension is then spiked with one of the previous micro-organism suspension, using the following ratio : 25 μ L of micro-organisms suspension, 1 μ L of RBC suspension and 25 μ L of deionised water. In contact with this hypotonic solution, red blood cells get immediately lysed by osmotic shock. The final concentration of micro-organisms and red blood cell ghosts in the sample are approximately 2.45×10^8 cfu/mL (bacteria) or 4.9×10^6 cfu/mL (yeasts) and 1.95×10^8 RBC/mL, respectively. The increase of the solution electric conductivity due to RBC lysis is measured by a conductivity meter (Meter Lab CDM 210).

1.5 μ L of the solution is finally injected by capillarity in the micro-system. To avoid evaporation and interfering convective movements during the experiments, two oil drops (bioMerieux) were applied at both ends of the chamber.

3.5 Experimental setup

A 10 V_{p-p} sinusoidal signal was supplied by a function generator (Agilent 33250A, frequency range 0-80MHz). The electric signal parameters (amplitude and frequency) are controlled by an oscilloscope (Tektronix TDS640A). A card-edge plug-in connects the device to the generator.

Particule motion was observed with an optical microscope (Zeiss) and a x20 objective (Zeiss LD Epiplan) . The heat produced by the microscope incident light did not produce any convection movement of bioparticules. Images were captured with a CDD camera (Hamamatsu Orca) with a 1344×1024 pixel² resolution (covering a $0.43 \times 0.33 \mu\text{m}^2$ surface). Video acquisition is performed at 3.33 frame/sec. To compute cell velocity, image interpretation of DEP experiments was performed using the image processing software ImageJ with the particle tracker plugin Mosaic.

4 Results and discussion

4.1 Electric field distribution and dependence with the frequency

Analytical characterization of the effect of the passivation layer. The effect of the passivation layer was characterized analytically with the model proposed in the previous section. The resulting first order transfer function (equation 4) is a high pass filter with a cut-off frequency f_c and a gain G_0 defined by equation 6.

$$f_c = \frac{\sigma_m}{2\pi\epsilon_m} \frac{2}{2+\alpha} \quad \text{and} \quad G_0 = \frac{\alpha}{2+\alpha} \quad (6)$$

$$\text{with } \alpha = \frac{l_{gap}\epsilon_p}{\epsilon_m e_p}$$

Then we can assess the consequence of this high pass filter behaviour on the effective tension of the biological medium, as described by equation 7.

$$\begin{aligned} \text{if } f \geq f_c \text{ then } E_{medium}.d &= G_0.U_{applied} \\ \text{if } f \leq f_c \text{ then } E_{medium}.d &= G_0 \cdot \frac{f}{f_c} \cdot U_{applied} \end{aligned} \quad (7)$$

The electric field pulsation is thus a key parameter to determine the electric field intensity within the biological medium and thus the DEP force applied to various biological particles. If the working frequency is higher than the cut-off frequency, the electric field inside the micro-channel will be hardly screened by the passivation layer. On the contrary, if lower than the cut off frequency, the passivation layer will weaken the transmitted electric field.

This cut-off frequency highly depends on the biological medium frequency (as proved by equation 6), and thus will take different values depending on the suspension medium used during the experiments (figure 1c).

With the experimental conditions used for the micro-organism extraction (described in the Results section), the cut

Fig. 1 (a) Description and dimensions (not to scale) of a vertical section of the microfluidic device for cell separation using DEP. (b) Electric modelisation for frequency behaviour : the device can be described as a high-pass filter. (c) Analytical modelisation of the cut-off frequency as a function of the biological medium conductivity (the other parameters used in the modelisation are given in table 1) Red lines represent the medium conductivities used in the experiments. Blue crosses give values of the working frequencies chosen for the experiments

off frequency is around 700 kHz, which indicates the electric field is hardly shielded by the passivation layer at the working frequencies chosen to perform the separation (20 MHz). In addition, when using the DEP force in deionised water, the cut-off frequency is much lower (around 7 kHz), which enables to use lower working frequencies, such as 100 kHz.

Numerical solution. The determination of the spatial distribution of the electric field and thus the direction of the DEP force (shown in figure 2a) enables to distinguish two specific areas : i) the edges of the electrodes that correspond to posi-

tive DEP collection zone, and ii) the top of the sorting chamber above the center of the electrodes where particles are repelled by negative DEP.

Taking into account that electric field intensity and thus DEP forces decrease dramatically with the distance from the electrodes as illustrated by figure 2b (DEP force intensity being proportional to electric field gradient, as shown in equation 1), the microsystem height is limited to 30 μm for DEP sorting: this height was set as a compromise between the sorting efficiency and the volume of the sorting chamber. It also allows the use of complex biological samples with eukaryote cells such as leucocytes without clogging the micro-system since these cells can reach a size of 20 μm.

The parametric study of the electric field estimation for different electric signal frequencies (figure 3) confirms the previous modelisation of the passivation layer which screens the electric field in the medium when the electric signal frequency is lower than the cut-off frequency.

Discussion and comparison between analytical and simulation results. When computing the cut-off frequency and the gain of our micro-system high pass filter, we observed a very good fit between analytical and simulation results. These results are detailed in table 2.

Table 2 Comparison between analytical and simulation results for the estimation of the high pass filter cut-off frequency and gain

	analytical results	simulation results
f_c	675 kHz	900 kHz
G_0	0.70	0.73

The cut-off frequency determined by the analytical model involves the assumption of the mean equivalent path for the electric field between two electrodes (l_{gap}). We can make a correlation between the analytical model and the simulation results by computing the l_{gap} parameter used in the analytical model from the gain G_0 estimated by the simulation : to get a gain in the analytical model that equals the gain set by the simulation ($G_0 = 0.73$), the l_{gap} parameter has to be reevaluated to 11.5 μm. This means that the actual path of the electric field between two electrodes is slightly longer than the value of the gap.

To perform the most efficient sorting, the electric field frequency will have to be higher than the cut-off frequency. In the case where a lower frequency has to be used (in order to tune the CM factor transition), the efficiency of the DEP trap will decrease. To keep the same efficiency with low frequencies as the one we get with high frequencies, the screening can be managed by using a higher voltage on the

Fig. 2 (a) $|E|$ distribution (surface) and $\vec{\nabla}|E|^2$ direction (normalized arrows) inside a vertical section of the sorting micro-system (simulation parameters are itemized in table 1). (b) Estimation of x and y components of $\vec{\nabla}|E|^2$ for different heights above the electrodes (supply voltage frequency = 100MHz).

electrodes or by reconsidering the passivation layer thickness.

Fig. 3 (a) Estimation of $|E|$ for different electric signal frequencies (at a given distance above the electrodes = $0\mu\text{m}$). The estimation of $|E|$ with no passivation layer is given as a reference to compute the electric field screening produced by the passivation layer. (b) Evolution of $|E|_{\text{max}}$ in the micro-channel (at a given distance above the electrodes = $0\mu\text{m}$) as a function of the frequency.

One main benefit of this passivation layer is to decrease dramatically the AC electro-osmosis and electro-thermal effects that commonly appear beside DEP force when non-uniform electric field is applied. Moreover, the frequencies used for the binary sorting (several MHz) prevent AC electro-osmosis from interacting with DEP effects. These phenomena will be thus neglected in our experiments interpretations.

In order to validate the proposed methodology, all experiments described here after were carried out in low conductivity medium. In deionised water, the microbiological sample has a conductivity around $0.1\text{mS}\cdot\text{m}^{-1}$. When dealing with red blood cells, the cell lysis can increase the conductivity of the sample up to $20\text{mS}\cdot\text{m}^{-1}$.

4.2 Handling micro-organisms using the DEP force

The working frequencies we used to perform DEP+ and DEP- on micro-organisms (3MHz and 100kHz, respectively) are higher than the cut-off frequency we computed previously (around 7kHz when $\sigma_{bio} = 0.1 \text{ mS} \cdot \text{m}^{-1}$). Thus we can assume that the passivation layer doesn't screen the electric field within the biological medium.

Handling bacteria by DEP. Figure 4a displays how fluorescent *E. coli* bacteria distribute within the device while an AC electrical field is applied. Micro-organisms are collected at the edge of the electrodes when they exhibit positive DEP at 3MHz, while they levitate on the top of the fluidic chamber, above the center of the electrodes in the case where they exhibit negative DEP at 100kHz.

Either in positive or negative DEP regime, we observed that *E. coli* bacteria lined up with the field lines. This behavior, described as electro-orientation has already been noticed and explored in other papers.^{31, 32} This phenomenon is especially striking in these *E. coli* experiments because of their rod shapes.

Handling yeasts by DEP. Figure 4b displays how *C. albicans* yeasts distribute within the device while an AC electrical field is applied. Both equilibrium DEP positions are the same as in the previous *E. coli* experiments. When submitted to DEP- at 100 kHz, yeasts get collected in levitation at the top of the chamber. When submitted to DEP+, yeasts gather at the edges of the electrodes at 3MHz.

Some cells do not exhibit the same general trend, as shown especially on figure 4b. Some yeasts (5%) are adsorbed on the silicon oxide bottom surface of the device, and the DEP force is not high enough to desorb them. Some other yeasts (15%) stay in low electrical field regions (DEP-) independent of the signal frequency. This effect is certainly a consequence of the electroporation of the yeast walls. We already noticed in previous work the general trend of permeabilised cells to obey DEP-.³³

For both *E. coli* bacteria and *C. albicans* yeasts, the DEP force is far more intense than the buoyancy, and thus the cells levitate above the electrodes in a DEP- equilibrium position.

4.3 Pathogen separation from blood cells in a low conductivity medium

In order to get a relevant behavior of the mixtures, comparable to the one of clinical samples, we selected biological species that present similar shapes and structures to the ones found in real blood samples. So mixtures of blood cells with *E.*

coli bacteria or *C. albicans* have been used to validate our methodology.

The dilution of the sample in low conductivity medium allows both positive or negative DEP, when tuning the field frequency. As it is an essential step in our binary sorting protocol. Indeed, lowering the biological medium osmolarity selectively disrupts the membrane of the blood cells. Such a lysis occurs on red blood cells,³⁴ while **most** micro-organisms keep functional thanks to their robust cellular walls (table 3). Following this osmotic shock, blood cells populations and microorganisms will be directed oppositely by the DEP force when immersed in the same electric field gradient.

Table 3 Viability of micro-organisms once suspended in deionised water (viability assessed by a standard agar plate count method³⁵)

species	30 min in DI water	4h in DI water
<i>E. coli</i>	99 ± 2 %	92 ± 7%
<i>C. albicans</i>	77 ± 13%	72 ± 11 %

Figure 4c-d illustrates the spatial DEP separation of micro-organisms from red blood cells. This separation has been tested with different mixtures (*E. coli* (4c) and *C. albicans* (4d)).

When submitted to a 20MHz frequency signal, more than 92% of micro-organisms experience a DEP+ force and thus concentrate on the edges of the electrodes (table 4). Simultaneously, altered red blood cells experiment a DEP- force and gather on the top of the micro-system above the center of the electrodes.

Table 4 Micro-organisms trapping (DEP+) and release (DEP-) efficiency

species	trapping by DEP+ (20 Mhz)	release by DEP- (50 kHz)
<i>E. coli</i>	97 %	94 %
<i>C. albicans</i>	92 %	56 %

The release efficiency (table 4) was determined using only the DEP- force to repel the micro-organisms. While the majority of *E. coli* can be released by a DEP- force, only half of the yeasts are removed from the surface of the gap-electrode interface. The difference in the release rate between *E. coli* and *C. albicans* can be explained by the motility of *E. coli* cells that prevent them from non-specific interactions with the surface of the device. The use of an external flow could be a good option to increase this release rate.

Fig. 4 Illustration of negative and positive dielectrophoresis for fluorescent *E. coli* (a) and *C. albicans* (b). Micro-organisms exhibiting DEP+ collect at the edge of the electrodes (frequency = 3MHz), whereas micro-organisms exhibiting DEP- levitate on the top of the chamber, in the center of the electrodes (frequency = 100kHz). Illustration of negative and positive dielectrophoresis respectively for red blood cells and *E. coli* bacteria (c) or *C. albicans* yeasts (d) separation in low conductivity medium ($\sigma = 10 \text{ mS.m}^{-1}$, $f = 20 \text{ MHz}$). Magnification shows a lysed red blood cell, a *E. coli* bacterium and a *C. albicans* yeast.

Fig. 5 White blood cells undergoing negative dielectrophoresis ($f=20\text{MHz}$)

The DEP behavior of white blood cells (WBC) in low osmotic medium was also investigated. A high concentrated WBC solution (prepared with a BD vacutainer CPTTM following manufacturer instructions) was used to carry out this experiment, since a low concentration of WBC in whole blood is not convenient for properly characterizing their DEP response. White blood cells undergo the same DEP- movement than red blood cells (figure 5).

4.4 DEP force and bacteria velocity

From equation 1, we can theoretically compute the velocity of the cells, as they obey to Stokes' law in the micro-channel (equation 8).

$$v_{cell} \propto \nabla|E|^2 \quad (8)$$

To ensure that DEP is the only force that sets the cells in motion without the interaction of any other electrohydrodynamic forces, an analysis of the cell trajectory and velocity was performed.

The positions of 40 *E. coli* cells were tracked during the DEP+ stage (working frequency = 20MHz) and then plotted as a function of the distance from the electrode gaps (figure 6). Each data set corresponds to one tracked cell. The closest the bacterium is to the gap, the highest its velocity. Since the evolution of *E. coli* velocity in the x-direction fits perfectly with the x-component of $\nabla|E|^2$ distribution, this confirms our supposition that dielectrophoresis is the only force that governs cell motion, being much more intense than buoyancy of fluidic forces.

Fig. 6 Experimental *E. coli* velocity evolution with the distance from the electrode gaps (dark grey areas) and simulated x-component $\nabla|E|^2$ (red line). Each data set corresponds to one *E. coli* cell trajectory. The x-component of $\nabla|E|^2$ is computed for a height = $2\mu\text{m}$ above the electrodes. This confirms the proportional relationship between the cells experimental velocity and the x-component of $\nabla|E|^2$.

5 Conclusions

In this study, we developed a method and an associated microfluidic device for the extraction and concentration of pathogens from a suspension of blood cells. This device has been optimised with analytical and numerical electric considerations. Our method is based on the large tolerance of micro-organisms towards osmotic shocks. A hypotonic medium selectively alters blood cells and changes their dielectric properties while keeping most micro-organisms functional. This osmotic shock homogenizes the reaction of altered blood cells in a field gradient, as they experience negative dielectrophoresis, while micro-organisms experience positive dielectrophoresis. Interdigitated electrodes were used to create a highly non-uniform electric field required to perform the dielectrophoretic sorting. The performance of the device was validated on two very different pathogen species: indeed the generic aspect of the method is a key issue, as the nature of the pathogen is usually not known prior to its isolation in real biological samples. Nevertheless, this method requires the use of a low osmolarity suspension medium : a dilution of the analyte is thus essential. In order to improve this step, a carrier medium exchange module should be integrated upstream in the microfluidic device.

We believe that our device can contribute to filling the

critical gap in sample preparation between the collection of potentially contaminated samples and the analysis of pathogens in the case of blood contamination. Our results demonstrate the feasibility of pathogen extraction from a complex sample such as blood, using the combination of DEP forces and osmotic shock. We believe that developing this approach could provide the de-complexification step needed upfront of bacterial characterization methods (optical spectroscopy, mass spectrometry, sequencing) that are known to be strongly affected by the chemical and physical complexity of raw samples.

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