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# Paleomagnetic full vector record of four consecutive Mid Miocene geomagnetic reversals

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#### Abstract

Seventy Mid Miocene lava flows from flood basalt piles near Neskaupstadur (East Iceland) were sampled, which provide a quasi-continuous record of geomagnetic field variations. Samples were collected along the Profile B of Watkins and Walker (1977), which was extended about 250 m farther down in a neighboring stream bed. Published radiometric age determinations (Harrison et al., 1979) range from 12.2 to 12.8 Ma for the sampled sequence. Four reversals were recorded in this profile, with 18 transitional lavas found within or between 17 normal and 30 reversed polarity flows. The large amount of transitional lavas and the large virtual geomagnetic pole dispersion for stable field directions are noteworthy as such features are commonly observed in Icelandic lavas and manifest in a far-sidedness of the average VGP. The reason for this characteristic, which could be related to an anomaly beneath Iceland, a global field phenomenon, local tectonics, and/or non-horizontal flow emplacement, is scrutinized. Non-horizontal flow emplacement is likely in volcanic environments particularly if the sampled lavas are located on the paleoslopes of a central volcano.

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From the difference of the observed paleomagnetic mean directions to the expected directions assuming a geocentric axial dipole (GAD), a paleoslope which would explain the observed difference was calculated numerically. The obtained dip and dip direction point consistently to a possible volcanic extrusion center of the lavas. The determined paleodip, however, proved to be significantly too high compared to the usual slope of a central volcano, suggesting further reasons for deviations from the GAD. Other datasets of this age from Europe also show enhanced VGP dispersion, suggesting further contributions of geomagnetic origin for this observation. Basically all reversal paths move across the Pacific. Transitions were identified as belonging to C5An.1r - C5Ar.3r based on the Astronomically Tuned Neogene Timescale (Lourens et al., 2004). We selected 122 samples for paleointensity measurements using a modified Thellier method including tests for alteration and multidomain bias. 85 of the measured samples yielded data of sufficient quality to calculate paleointensities for 26 lava flows. The average paleointensity for stable field directions was 23.3  $\mu$ T, whereas the intensity drops to a minimum of 5.8  $\mu$ T during field transitions. The stable field intensities represent only about half of the present day field. The sawtooth pattern of intensities, which is characterized by a sharp increase of intensity directly after a reversal and then followed by a gradual decrease towards the next reversal, was not found in this study.

Key words:

Paleomagnetism, absolute paleointensity, Eastern Iceland, Mid Miocene,

Geomagnetic reversals

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#### 1 1 Introduction

The Earth's magnetic field has changed its polarity many times in the past. It is not known in detail how the geomagnetic field behaves during a reversal, but many results show a decrease of field intensity, likely related to a decreased dipole component, and multipole components, which become stronger (e.g. Merrill and McFadden, 1999; Leonhardt and Fabian, 2007). Detailed records of transitional fields were mostly obtained from sediments. In the work of Clement (1991), Tric et al. (1991) and Laj et al. (1991) the transitional VGPs were predominantly found within two approximately antipodal longitudinal bands across America and Asia. Some theories state the existence of this preferred longitudes of the virtual geomagnetic poles (VGPs) due to local flux concentrations of radial components and lower temperatures at the CMB. However, other studies (Prévot and Camps, 1993; Langereis et al., 1992; Leonhardt and Fabian, 2007) could not confirm these preferred longitude sectors. Beside geomagnetic reversals, the field behavior during stable polarities is subject of detailed research. The field's intensity was found to follow an asymmetric saw tooth pattern, which is characterized by a decrease before 17 reversals and a large sudden recovery after the polarity change (Valet and Meynadier, 1993). However, remanences in sediments are often affected by post-depositional reorientation and the magnetic torque acting on the particles may not be sufficient to orient them properly (Tauxe, 1993). Furthermore the remanence acquisition can also be severely delayed (Roberts and Winklhofer, 2004), if sedimentation rate is low. In contrast to sediments, volcanic rocks record a geologically instantaneous field (Prévot et al., 1985) and provide the possibility to determine absolute paleointensities. Unfortunately, volcanic

- 26 activity is usually very short lived and sporadic. Therefore, magnetic measure-
- ments at volcanic sequences are often of weak temporal resolution and cover
- only short time intervals.
- Exeptional long time inervals, however, have been found particularly in Ice-
- land (Watkins and Walker, 1977) and Kerguelen Archipelago (Camps et al.,
- 2007). The flood basalt piles in East Iceland, cover an enormous age range and
- they are highly suitable for paleomagnetic measurements due to the extrusion
- of one lava flow per 10 kyr, a mean extrusion rate which is assumed to be quite
- homogenous in the lower part of the pile (Watkins and Walker, 1977). Previ-
- ous paleomagnetic projects in Eastern Iceland are the work of Watkins and
- Walker (1977) in Neskaupstadur and of Kristjansson (1995) at the neighbor-
- ing peninsula. Watkins and Walker (1977) magnetistratigraphically correlated
- <sup>38</sup> 700 successive lavas in the flood basalt pile, ranging from 13.6 to 2.0 Ma in
- <sup>39</sup> age. Herrero-Bervera et al. (1999) repeated the Watkins and Walker profiles
- 40 C and D (12.09-10.21 Ma) for a more detailed examination of transitional
- lava flows and reversal paths. In this study, profile B of Watkins and Walker
- (1977) was repeated and extended 200 m farther down to determine the direc-
- tional behavior and absolute paleointensity variation across geomagnetic field
- 44 reversals, as well as to analyze the full vector record during stable polarity
- 45 intervals.

#### <sup>46</sup> 2 Geological setting and field work

- 47 Samples were taken from lava flows of the flood basalt pile mountain Nipokol-
- 48 lur (65.157 °N, 13.656 °W) near Neskaupstadur, Eastern Iceland. These flood
- 49 basalts are well stratified and dip towards the active zone due to spreading

(Walker, 1974). The regional dip in the flood basalts piles of Neskaupstadur varies from 8° at sea level to 4° at mountain summits. On average this regional dip decreases with 1-1.5° per 200 m altitude (Kristjansson, 1995) due to down-dip thickening of the lava flows (Walker, 1964). The average accumulation rate of the basalt piles of 700-1000 m per Myr is decreasing with altitude. Due to intensive erosion only 1200 m altitude of the originally 10 km thick plateaus is left today (Krafft, 1984). Glaciers created the fjords in the Quaternary (Kristjansson, 1995), leaving outstanding outcrops of the basalt piles. In principle, we followed profile B of Watkins and Walker (1977) (see Fig. 1), but extended it farther down to 199 m altitude (original profile was down to 550 m). With a total of 70 lava flows an altitude of about 500 m was covered. Within the sampled profile some dykes (about 2 m wide) came close to the sites. A minimum distance of 9 m was always kept to prevent a thermally induced magnetic overprint of the dyke. Below site 20 we had to proceed the profile in a neighboring stream bed, as a very broad dyke crosses the outcrops of our section and the minimum distance could not be maintained anymore. Within the section also pillow lavas were found, which presumably formed in some shallow temporary ponds (Walker, 1974). Individual lavas were distinguished by red beds or paleosoils as well as top and basal breccia of the flow. Six samples per site with a diameter of one inch (2.54 cm) were cored using a gasoline-powered portable drill with a water-cooled diamond bit. Whenever possible samples were drilled horizontally distant and in the lower third of a lava flow in order to avoid any reheating from later flows above.

#### 3 Methods and Results

#### 74 3.1 Rock Magnetism

For a preselection and eligibility testing of the samples for paleointensity determinations, rock magnetic measurements were carried out for one sample per site, including isothermal remanent magnetization (IRM) aquisition, back field curves and hysteresis measurements with a peak field of 900 mT and thermomagnetic measurements with a peak temperature of 700 °C at the variable field translation balance (VFTB) of Petersen instruments. Hysteresis measurements revealed that most of the samples are within the PSD range and cluster along the SD-MD mixture lines (Dunlop, 2002) (see Fig. 2). Thermomagnetic results are discussed in the following together with ore microscopy. Furthermore, we performed measurements of the anisotropy of magnetic susceptibility on a representative part of the collection to test for the possibility of anisotropy bias in paleointensity determination and to analyze the flow directions of the lava flows (Henry et al., 2003). All investigated samples are found to be isotropic, based on anisotropy values well below 1.5%.

#### 89 3.2 Thermomagnetic curves and ore microscopy

- Samples were classified into four groups based on microscopy and thermomag-
- netic experiments (see Fig. 3). Ore microscopic observations of 14 samples
- helped to determine the oxidation state of the magnetic rock and to identify
- 93 the remanence carriers.
- Group 1 samples (5 % of samples) show two Curie temperatures, one around

- 200°C and the other at 450°C. The lower Curie temperature is likely related to unoxidized regions in the titanomagnetites as shown in the ore microscopy picture. Accumulation of ferrofluid along cracks in these titanomagnetites suggests a secondary maghemitization, which is responsible for the second Curie temperature. The dominant Curie temperature of group 2 (10 %) range between 250°C and 100 430°C. As shown in the microscopy picture, cracks are abundant in the mag-101 netic minerals, likely induced by shrinking during low temperature oxidation. 102 Therefore this magnetic phase is interpreted to be titanomagnemite. Skeletal 103 and cruciform structures can also be observed, which are a result of late crys-104 tallization of the TM into an already firm matrix, typical for tholeitic magmas
- oxidized grains are present, carrying a primary magnetization above 450°C. 107 Judging from ore microscopy, group 3 samples (25 %) are very similar to group 108 2 samples, except for the fact that the presence of a high temperature oxidized 109

(Carmichel et al., 1960). Additionally, a minor ammount of high temperature

titanomagnetite is clearly visible in the thermomagnetic curve. 110

105

106

Samples of group 4 (60 %)(Fig. 3) are characterized by single Curie temper-111 atures between 500° and 580°C. Beautiful exsolution lamellae were found in 112 these samples, indicating high temperature oxidation. Highly oxidized phases 113 are relatively insensitive to further oxidation under laboratory conditions, 114 which is an excellent qualification for any paleomagnetic analysis. Only sam-115 ples from sites, where this behavior was observed, were subjected to paleointensity determinations.

#### 18 3.3 Paleodirections

NRM measurements were carried out in the magnetically shielded laboratory of the LMU in Niederlippach. A cryogenic magnetometer for the weaker mag-120 netized samples and a spinner magnetometer for the stronger ones were used 121 to determine the samples' remanences. Half of the samples per site were sub-122 jected to alternating field demagnetization (up to 200 mT) and the other half 123 was thermally demagnetized (up to 600 °C) with at least 14 steps. Measure-124 ments of the susceptibility with a Geofyzika KLT-3 minikappa bridge after 125 every heating step helped to recognize the onset of chemical alteration of the 126 thermally treated samples. Typical demagnetization diagrams for normal, re-127 versed and transitional directions are shown in Fig. 4a. For over 90 % of all 128 samples of Neskaupstadur the orthogonal projection is characterized by a sta-129 ble directional component. Despite their age most samples only carry a minor 130 viscous overprint, which is demagnetized between 100 and 150 °C (see Fig. 4). 131 For some samples principle component analysis could not be applied. Those 132 directions were evaluated using great circle techniques (McFadden and McEl-133 hinny, 1988) (see Fig. 4b). Few samples contain a major magnetic overprint 134 or a unstable direction with a too small unaffected NRM to be evaluable (see 135 Fig. 4c). Only samples with a confidence cone  $\alpha_{95} < 12^{\circ}$  and a concentration parameter k > 40 (calculated using Fisher (1953) statistics) were included 137 into further evaluation of the paleodirections. 138 Tilt corrections had to be applied to the dataset, as the center of Iceland sub-139 sided due to spreading effects and the weight of the glaciers and extrusions. 140 Thus, the flood basalt pile near Neskaupstadur has an regional tilt of about 141 4-8° to 264°W. In most previous studies (Watkins and Walker, 1977; Krist-

jansson, 1995; Herrero-Bervera et al., 1999) it is assumed that the flood basalts flow over very far distances with negligible slope and were emplaced subhor-144 izontally. Therefore a tilt correction to horizontal is applied to the Tertiary 145 basalt piles in Eastern and Western Iceland with a dip direction pointing towards the central ridge and a dip varying with altitude due to down-dip 147 thickening. The same approach is used here for initial analysis and its valid-148 ity will be discussed below. By linear interpolation the dip values of the lava 149 flows were calculated to vary from 7 ° for the sites JD-10 (150-300 m), 6 ° for 150 the sites 11-25 (300-450 m), 5 ° for the sites 27-45 (450-600 m) to 4 ° for the 151 uppermost sites 46-64 (600-761 m). 152

Four reversals were found within the section (see Fig. 5) with the transitional 153 directions of the sites 51-46B (denoted reversal D below), 36-29 (reversal C), 154 16-14 (reversal B) and 11-05 (reversal A). The sites 62-58 are assumed to repre-155 sent an excursion, the sites 00-JD could indicate the termination of a preceding reversal. Using a cut-off colatitude for transitional lavas of 41.3 ° (McElhinny 157 and McFadden, 1997) we found 18 transitional, 30 reversed and 17 normal 158 polarities in the section. From 6 sites no reliable paleodirection could be de-159 rived. At a first glance the inclinations represent the expected values of a GAD pretty well (see Fig. 5). The declination scatters, but this is a typical feature 161 at high latitudes.

Numerous dykes are found within the lava pile of eastern Iceland. In our profile, the minimum distance between dyke and sampling locality was 9 m (for the sampling spot at flow JD). In order to identify any possible magnetic overprint by later intrusion of this 5 m thick dyke, this dyke was sampled as well (site DY). Different directions between dyke and lava flow indicate that his dyke did not affect the remanence at our our sampling spot. The possible influence of

dyke reheating was also investigated by a contact test close to site 13. This lava flow is crossed by a relatively thin dyke ( $\approx$ 3m). Four samples were taken from 170 the dyke itself, another four in increasing distances (0.7 to 2.6 m) from the 171 dyke. All samples show a similar directed and relatively strong overprint up to 172 370°C. Above this temperature distinctively different directions are observed 173 between dyke and lava flow, already at closest distance of 0.7 m. Most dykes 174 along the sampled profile are of similar or less width compared to the dyke 175 crossing the section at site 13. Thus the minimum distance of more then 9 m 176 to the dyke, which was kept for all sites, is sufficient to prevent sampling of reheated rocks.

#### 179 3.4 Paleointensities

The intensity of the TRM in the flood basalts depends on the amount of mag-180 netic minerals, their composition, grain size and grain shape, the decay of the 181 magnetization with time and, of course, the ancient magnetic field. For the 182 paleointensity measurements in this study the MT4 method (modified Thellier 183 type four, containing alteration (CK), tail (TR) and additivity checks (AC)) 184 (Leonhardt et al., 2004) was used. The laboratory field inside the shielded fur-185 nace, applied during heating and cooling, was chosen to be 30  $\mu$ T, about half of 186 the present day field, because of the high amount of transitional lavas and due 187 to the presumed Miocene dipole low (Prévot et al., 1985). The samples of 8mm 188 diameter and 7mm length were magnetized along the z-axis and kept in the 189 same position within in the furnace during all temperature steps to minimize 190 bias from temperature gradients and field variations. Due to the small sample 191 size slightly larger orientation errors occur in the x-y plane, leading to more

scattered horizontal components on the orthogonal projections. Paleointensity determinations, however, are unaffected. ThellierTool4.11 (Leonhardt et al., 194 2004) was used to analyze the paleointensity determinations. All analyzes are 195 characterized by origin pointing stable directional component in agreement 196 with its directional analysis, NRM fractions f above 30% (average 73%), at 197 least 5 successive data point, quality factors q above 2.3 (average 15.8), minor 198 alteration contribution (< 10%) determined both from the individual check 199 differences and from the cumulative difference, and finally, the absence of any 200 significant MD contribution as tested by tail checks ( $\delta t^* < 5\%$  below the maxi-201 mum unblocking temperature) and additivity checks. For a determination of a 202 site mean value, only sites with more than two eligible samples were accepted. 203 If more than two successful determinations are available for a site, then a 204 weighted mean of the paleointensity and its uncertainty was calculated using 205 the quality factor q (Coe et al., 1978) in order to emphasize intensity determi-206 nations of higher quality. For six sites only 2 determinations were successful, 207 thus, the maximum possible uncertainty is given there. Tab. 2 summarizes 208 the paleointensity results for the all measured samples. Magnetomineralogical 209 changes during heating are the main reason for rejecting individual measure-210 ments. For some weakly affected samples corrections for these alterations were 211 applied (Valet et al., 1996) using the cumulative alteration difference if any 212 significant contribution from MD remanence could be excluded based on tail 213 checks. Furthermore, check corrected samples (for an explanation of the cumu-214 lative alteration difference see Leonhardt et al. (2004)) were only included if 215 additivity checks then fit the expected pTRM values suggesting a preservation 216 of essential TRM properties despite laboratory magnetomineralogical changes 217 and if at least one value per site could be determined without corrections. One 218 third of the collection was analyzed by applying the correction technique. The

mean paleointensity of 23.3  $\mu$ T for stable polarities across the section is very low. The values including reversals range from a minimum of 5.8  $\mu$ T at site 32 to 22.8  $\mu$ T at site jb and their average with 13.3  $\mu$ T is about half of the non-transitional periods.

#### 224 4 Discussion

#### 225 4.1 $Stable\ polarity\ fields$

Magnetostratigraphic correlation. Due to their stratigraphic succession, 226 the flood basalt piles in Eastern and Western Iceland provide an independent 227 geomagnetic timescale back to 13 Myr ago (Harrison et al., 1979), which can be 228 correlated with marine magnetic anomalies. At first we compared our data to 229 the results of profiles A and B of Watkins and Walker (1977), which are based 230 on two measurements for each directional unit. Based on flow descriptions, 231 similar altitude, and their position relative to pronounced red beds, some lava 232 flows (see Table 1) could be unambiguously correlated to profile B of Watkins 233 and Walker (1977). Above these flows a direct flow-to-flow correlation between 234 Watkins and our work is not possible, because of slightly different sampling 235 routes. Based on altitude measurements, however, both profiles can be com-236 pared and paleodirectional comparisons yield mostly similar results, although 237 some differences in particular for transitional directions are also observed. 238 Watkins sampled older lava flows down to sea level in a different stream bed 239 some hundred meters to the east, denoted profile A (Watkins and Walker, 240 1977). Based on directional results, our data shows similar prominent features 241 as a composite A+B section of Watkins and Walker (1977). One discordance 242

concerns the 12d chron (Opdyke, 1972). Instead of a normal polarized site at this altitude as stated by Watkins and Walker (1977) we found a tran-244 sitional VGP in the northern hemisphere. The normal directions could have 245 been missed due to gaps (35m gap between site 10 and 11 and 60m between 246 site 13 and 14) in our section. Another possibility would be the insufficient demagnetization in the previous work and thus, no 12d normal chron in the 248 previously sampled section. Correlation to global timescales like the Astro-249 nomically Tuned Neogene Timescale ATNTS2004 (Lourens et al., 2004)(see 250 Fig. 7) and radiometric dating of overlying and underlying profiles (McDougall 251 and Schmincke, 1976; Harrison et al., 1979) give an age ranging from 12.2 to 252 12.8 Ma for the section, which is within the marine anomaly 5A. Based on 253 this correlation the sampled section ranges from C5Ar.2r to C5An.1r. 254

**Deviations from GAD field.** A positive class B reversal test confirmed that 255 the mean values of the normal and reversed polarity data show a good antipo-256 dality, indicating that no overprints, insufficiently removed secondary compo-257 nents or rotations falsify the VGPs. Although statistically not significant as 258 the uncertainty ellipse includes the geographic pole, the average normal and 259 reversed VGPs yield a slight right-handedness. Such right-handedness, how-260 ever, can be observed in data from all over Iceland, independent of age and 261 location (Kristjansson and Jonsson, 2007). As the right-handedness is inde-262 pendent of the location in Iceland and found in Eastern and Western Iceland, 263 neither rotational effects nor relocalization due to spreading can be the cause. 264 Some suggested possible explanations are a magnetic anomaly beneath Iceland 265 (Kristjansson and Jonsson, 2007), maybe connected to the plume, or a per-266 sistent non axial-dipole field. All VGPs within the cut-off colatitude of 41.3° 267 (McElhinny and McFadden, 1997) were used to determine the VGP scatter 268

around the spin axis. McElhinny and McFadden (1997) proposed a angualr standart deviation of 20.2° for latitudes between 60° and 70° for the last 5 Myr. 270 In this study we determined a slightly enhanced between site angular stan-271 dard deviation of 23.2° with upper and lower confidence limits of 30.2° and 272  $18.9^{\circ}$  (Cox, 1969). The VGP latitudes in this study show a tendency to decrease from the moun-274 tain tops to the sea level. However, as will be shown in the following, these 275 low VGP latitudes are an artefact due to the applied dip correction based on 276 the assumption of horizontal emplacement of the lavas. If there was an initial 277 topography like central volcanoes, which can have a slope up to 10°, then 278 the flood basalts already had an initial dip during deposition and correction 279 towards horizontal emplacement falsifies the result. Also the down-dip thick-280 ening (Walker, 1964) of the lava flows suggests an initial dip. To determine 281 this paleoslope, which would explain the low VGP latitudes (see Fig. 8), the 282 magnetic vector  $v_{\text{GAD}}$ , which would be derived from a GAD, was rotated to 283 the measured vector  $v_{\text{measured}}$ . The paleodip and paleodip direction describing 284 this rotation were found numerically. 285 For a determination of the measured vector  $v_{\text{measured}}$  the in situ mean direc-286 tions were determined for each group of samples, which represent a polarity 287 chron, to randomize the effects of paleosecular variation (see Fig. 8). VGPs 288 from group one do not cluster very well, presumably an effect of the ending 289 of a preceding reversal. Group two only contains three sites, which is not 290 enough to average out paleosecular variation. The groups three, four and five 291 give good mean directions. However, sites 59-61 were not included into the 292 calculation of the mean direction of group five, because of their excursional 293 character. The  $v_{\rm GAD}$  for the Neskaupstadur latitude consists of the expected 294 inclination of I = 77.0 and declination of D = 0. This GAD vector was rotated

about all possible paleodips  $(0-\frac{\pi}{2})$  and paleodip directions  $(0-2\pi)$ . Thus, the expected  $v_{\text{rotated GAD}}$  was determined. The norm of the vector subtraction 297  $|v_{measured} - v_{rotated\ GAD}|$  was calculated and the minimum of the resulting ar-298 ray (minimum deviation of the two vectors) gives the best-fitting paleodip and 299 paleodip direction (see Tab. 3 and Fig. 8). 300 The determined paleodip directions vary from 4° to 36° and are assumed to 301 represent the flow direction of the flood basalts. By tracking back the direc-302 tion where the lava flows came from (184-216°) Reydarfjordur central volcano, 303 which is about 15 km away from Neskaupstdur, might be interpreted as pos-304 sible extrusion source (see also Fig. 1). 305

However, the calculated paleodips of 19° to 41° are far too high for the slope 306 of central shield volcanoes, which usually have a slope up to 10° (Schmincke, 307 2000). Thus, it has to be assumed, that the observed low VGP latitudes are 308 not solely an effect of the paleoslopes and effects like a regional anomaly or 309 a global field effect have to be taken into account. Remarkably, lower VGP 310 latitudes than expected were not only found in Icelandic lava flows, but as well 311 in the sedimentary datasets of Abdul Aziz et al. (2000) from Calatayud Basin 312 in NE Spain (41.17°N, 1.28°E) and of Hüsing et al. (2007) from northern Italy 313 (43.59°N, 13.56°E), which are of the same age. Despite the remancences of 314 these sediments could be affected by inclination shallowing, all the data from 315 different sites together suggest that the low VGP latitudes are most likely 316 a global field effect. Nevertheless, for a more conclusive statement further 317 datasets, particularly from the southern hemisphere, should be taken into 318 account. 319

Paleointensity variation between reversals. For the two lowermost stable polarity intervals too few site were eligible for paleointensity determinations

and thus no record of the intensity behavior could be obtained. During the polarity chron C5Ar.1r, the paleointensity builds up from site 18 with 8.5  $\mu$ T 323 to site 28 with 39.6  $\mu$ T. Above site 35 a large scatter in intensity is observed. 324 Instead of a slow increasing field intensity, the sites 39 (15.5  $\mu$ T) as well as 43 325  $(14.3 \mu T)$  represent low values for a normal polarity interval at high latitudes. 326 The low intensity of site 43 can be interpreted as being related to the onset 327 of the next reversal. During the last reversed polarity chron of this section 328 (C5An.1r) the intensity reaches high values at site 55 (41.4  $\mu$ T). Finally, a low 329 paleointensity value (site 61) during C5An.1r is from a post-excursional site. 330 Overall, the field is characterized by lower paleointensity values compared to 331 the present day field. The VDM, calculated from the paleointensities of the 332 inter-reversal sites, is  $3.2 \pm 1.5 \cdot 10^{22} Am^2$ . This is about half of the present 333 dipole moment  $(8 \cdot 10^{22} Am^2)$  and even lower the previously published values 334 for the Miocene  $(5.9 \pm 0.8 \cdot 10^{22} Am^2$  (Leonhardt et al., 2000) and  $6 \cdot 10^{22} Am^2$ 335 (Juárez et al., 1998)). However, a VDM about  $3.2 \cdot 10^{22} Am^2$  is close to the 336 low-field level of  $4-5 \cdot 10^{22} Am^2$  suggested by Shcherbakov et al. (2002) and 337 Heller et al. (2003).

#### 339 4.2 Transitional fields

Reversal paths. Although polarity transitions are geologically spoken so quick that it is difficult to find volcanic rocks that preserve a complete and accurate record, many transitional directions were found in the Nipukollur section. This is surprising looking at the relatively low extrusion rate of approximately one flow per 10 kyr. Fig. 9 shows the VGPs of the four transitions recorded in the sequence. VGPs of contemporary Spanish and Italitan data

sets (Abdul Aziz et al., 2000; Hüsing et al., 2007) were compared to the results of this study. The oldest reversals C5Ar.2r-C5Ar.1n (see Fig. 9a) is a 347 R-N transition. Prior to the reversed field direction some transitional poles 348 are found east of Patagonia. A first transitional VGP from site 06 is found in Indochina. Sites 07 and 08 show transitional VGP offshore of South Ameri-350 cas west coast, before reaching the stable field direction in Scandinavia and 351 Siberia. Comparisons to Watkins and Walker (1977) dataset of profile A indi-352 cate that site 06 is significantly older the sites 07 and 08. Therefore its field 353 direction is assumed to be related to the C5Ar.2n normal chron and not the 354 reversal C5Ar.2r-C5Ar.1n. No transitional directions are found in the Spanish 355 data set (Fig. 9a). The N-R reversal B from C5Ar.1n to C5Ar.1r only contains 356 one clearly transitional data point (site 15) in the middle of the Pacific close 357 to Hawaii (Fig. 9b). Similar Pacific longitudes are observed in the European 358 data which are, however, only weakly defined. A similar post-reversal swing 359 in (Fig. 9b) is found in all three data sets. The R-N reversal C begins with a 360 swing from Antarctica to Australia and back again (site 29). Such directional 361 changes, sometimes referred to as precursors, occasionally accompany reversals 362 (Valet, 2003). After this onset-excursion the VGP path spans straight across 363 the Eastern Pacific and clusters (two lava flows) somewhat south of Hawaii. 364 Such clusters could describe the stop-and-go behavior of reversals (Hoffman, 365 1992) or just be an effect of rapid extrusion of lavas. With East-West swings 366 across Alaska the VGP moves to stable directions in Northern Canada and 367 the Arctic. Similar directions as in the initial excursion and the post-reversal 368 North American VGP cluster are observed in the Italian dataset, suggesting a 369 dipolar dominance during these phases. The last C5An.2n to C5An.1r reversal D (see Fig. 9d) begins in the Arctic Ocean. Then the VGPs cluster near the 371 Ninety-East-Ridge (site 47-49) and move on to Antarctica. Ten lava flows later

a post-reversal excursion starts from Antarctica first in the direction of Cape Hope (site 58) but swings on to a near-equatorial VGP near French Polynesia 374 (site 59) and moves on to south of Malaysia (site 60) and near Ninety-East-375 Ridge (site 61) before coming back to Antarctica. This post-reversal excursion 376 seems to be similar to the termination loops found by Prévot et al. (1985), 377 which show a trend to be anticlockwise in the southern hemisphere (Jacobs, 378 1984). With a last swing to the Amundsen Sea north of Marie Byrd Land (site 379 63 and 64) the sampled section ends. In almost all cases transitional directions 380 can only be found in the final hemisphere, which can be interpreted as a gen-381 eral trend for the reversals to start pretty fast. This is in good agreement with 382 the observation, that the termination paths are characterized by bigger loops 383 and more intermediate directions than the onset path (Herrero-Bervera, 1986; 384 Jacobs, 1984). A tendency for the Icelandic VGPs to be found in the Pacific 385 (Kristiansson and Jonsson, 2007) can be affirmed with this study (Fig 9). 386

Intensity variations across a transition. Unfortunately, below site 18 only few sites were suitable for paleointensity measurements. A general trend of the 388 intensities to decrease during the transitional states (Fig. 5) was found. Dur-389 ing the reversals A and C the intensity even drops to values below 10  $\mu$ T. 390 These observations are in agreement with the common observation that tran-391 sitions are accompanied by a substantial decrease in the mean intensity of 392 the dipole field (see (Merrill and McFadden, 1999) and references therein). 393 Remarkably the intensity also drops to below-transitional values during the 394 C5An.1n chron. Pre- and post-reversal loops unfortunately yielded no paleoin-395 tensity data, except for site 61, a post-excursional lava, which is characterized by a low intensity of 6.8  $\mu$ T. Despite the high ratio of transitional lavas to 397 non-transitional lavas, none of the four transitions provides a sufficient amount

of data to give a detailed picture of the field's intensity behavior during a reversal. Most likely the frequency of the extrusion of lavas (approximately one lava per 10 kyr) was not high enough to provide a complete record of the field in transition. Furthermore, it is noteworthy that normal polarity results are characterized on average by lower intensity values than reversed polarity lavas.

#### 405 5 Conclusions

The Watkins and Walker (1977) profile B in the flood basalt pile near Neskaup-406 stadur, Eastern Iceland, was resampled and extended about 250 m farther 407 down. The paleomagnetic record of this flood basalt section contains four geo-408 magnetic field reversals. By correlating the directional data first to the data 409 from Watkins and Walker (1977) and then to the astronomically tuned global 410 timescale (Lourens et al., 2004) the section was identified to range from the 411 reversed C5An.1r chron to the reversed C5Ar.2r and thus cover about 700 kyr 412 of extrusions, approximately between 12.2 and 12.8 Myrs ago. Altogether 18 413 transitional lavas were identified, characterized by a VGP deviation from the 414 geographic poles of more than 41.3°. The paleosecular variation is slightly 415 enhanced in this section. The VGPs during the polarity chrons show a gen-416 erally lower latitude than expected from a GAD field. Possible reasons for 417 this deviation are related to a local anomaly beneath Iceland, a global field 418 phenomenon and/or non-horizontal flow emplacement. Flood basalts normally 419 flow over very large distances with negligible slope and thus, a bedding cor-420 rection to the horizontal plane was carried out at first like it is done in most 421 earlier studies. Using a numerical method the paleodip and paleodip direction,

which could be responsible for the rotation of the VGPs expected from a GAD to the measured VGPs, were determined. The calculated flow direction points 424 consistently towards a possible volcanic source, the Reydarfjordur central vol-425 cano. The calculated average paleodip  $(24.7^{\circ})$ , however, seems to be too high 426 for the slope of a central volcano, which usually have a slope of maximum 427 10°. Thus, non-horizontal flow emplacement cannot be the only reason for the 428 observed VGP deviation. Other studies on Mid Miocene sediments of Italy 429 and Spain (Hüsing et al., 2007; Abdul Aziz et al., 2000) also revealed large 430 deviations from the GAD. Thus, the too low VGP latitudes from Iceland are 431 most likely not a local, but a global field effect. This conclusion is also in ac-432 cordance with the low mean paleointensity of 23.3  $\mu$ T which represents about 433 half of the present field intensity. The saw-tooth pattern (Valet and Mev-434 nadier, 1993), a fast rebuilding field after the termination of a reversal and a 435 slow decay of the intensity during the polarity interval, was not found during 436 the polarity intervals in this study. Contradicting the saw-tooth hypothesis, 437 the paleointensities would even suggest an inverse feature: an increase of pale-438 ointensity for one investigated polarity interval (C5Ar.1r). The reversal paths 439 of the VGPs run across the Pacific or Eastern Asia. Generally all paths are 440 in the far-sided hemisphere outside of the proposed longitudinal bands. Other 441 studies on Mid Miocene sediments (Hüsing et al., 2007; Abdul Aziz et al., 442 2000) also revealed far-sided reversal paths across the Pacific and E-Asia. Due to a low resolution the VGPs paths could not be compared in detail. Never-444 theless, similar precursors and post-reversal loops were found in all studies, 445 indicating a dipole dominance shortly before and after the reversals. Transi-446 tional layas are characterized by a very low paleointensity, below 10  $\mu$ T for two reversals. Altogether, the low intensities and low VGP latitudes suggest a 448 larger influence of non-dipolar terms for Mid Miocene geomagnetic field than

so compared to today.

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- Fig. 1. **Left:** Sampled section as seen from the lighthouse of Neskaupstadur. Original profile B of Watkins and Walker (1977) indicated with the dashed line. The bold line marks the sampled section of this study. **Right:** Overview about previous paleomagnetic projects in Eastern Iceland (modified after Kristjansson (1995)).
- Fig. 2. Day plot (Day et al., 1977) with mixture lines and boundary values according to Dunlop (2002). The samples cluster within the PSD range along the SD-MD mixture lines.
- Fig. 3. Ore microscopy of samples from different rock magnetic groups: Group 1 contains 5 % of samples, group 2 10 %, group 3 25 % and group 4 60 %. Samples were covered with ferrofluid, except right picture of group 2 and the group 3 picture, which were examined under polarized light.
- Fig. 4. Orthogonal projections of **a**) stable directions (Site 28 with reversed polarity, 46 with normal polarity and transitional JD transitional) and **b**) great circle (Site 46B) and **c**) rejected samples (Site 10)
- Fig. 5. Paleodirections (declination and inclination) for each sampled site and absolute paleointensites for eligible sites versus altitude. The dashed lines denote the values expected from a GAD. The polarity log was generated using a cut-off colatitude of  $41.3\,^{\circ}$  (McElhinny and McFadden, 1997) with black for normal, white for reversed and grey for transitional lava flows. Reversals are numbered from A to D and polarity chrons denoted after global timescale (for correlation see Fig. 7.)
- Fig. 6. Arai plots of site 12 and 25 together with orthogonal projections (black circle for declination and white circle for inclination). The dashed lines indicate the linear segment used for the calculation of paleointensity. Triangles denote the alteration check step, gray squares the additivity checks.
- Fig. 7. Correlation of VGPs to the results of Watkins and Walker (1977) and to global timescales like the ATNTS of Lourens et al. (2004).

Fig. 8. Trend of VGPs to lower latitudes for the lower section of the profile. The grey line shows the bedding corrected data with the values of the regional tilt, the black line the in situ data. The mean VGP latitudes are calculated for each group of stable field directions and given in Tab. 3. The mean inclination is shown with a black star. Results of the MATLAB<sup>TM</sup> calulations of the paleoslope are shown for each group. See text for more information.

Fig. 9. VGP paths projected on the globe for transitions in the Neskaup-stadur/Nipukollur section. a) is the oldest R-N transition, d) the youngest N-R transition. The black star denotes the Icelandic site. The dashed grey lines is based on the Spanish data set, the pointed dark grey on the Italian data set.

Table 1: Directional results

| Section   Color   Co   | Site      | Altitude   | n/N             | $\mathbf{D}_g$ | $\mathbf{I}_g$ [°] | $\mathbf{D}_s$ | $\mathbf{I}_s$ | k   | $\alpha_{95}$ | F                  | VGP                | VGP               | Pol.                |
|--|-----------|------------|-----------------|----------------|--------------------|----------------|----------------|-----|---------------|--------------------|--------------------|-------------------|---------------------|
| 63 7,0 5/6 268 7.29 305.5 76.1 173 5.8 197.0 44.88 T 62 735 5/6 198.5 7-199 175.4 1-80.8 49 11.1 151.8 8-82.9 R 61 727 5/6 84.4 -50.7 84.4 -40.7 30.9 4.4 6.8 93.7 -22.9 T 61 727 5/6 84.2 -50.7 84.4 -40.7 30.9 4.4 6.8 93.7 -22.9 T 63 76 77 17 5/6 84.2 -50.7 84.4 -40.7 30.9 4.4 6.8 93.7 -22.9 T 64 77 18 18 18 18 18 18 18 18 18 18 18 18 18   |           |            | - / -           | [°]            |                    | [°]            | [°]            |     | [°]           | $[\mu \mathbf{T}]$ | long. $[^{\circ}]$ | lat. $[^{\circ}]$ |                     |
| 62 735 5/6 198.5 -79.9 175.4 -80.8 49 11.1 1 154.8 -82.9 R 61 727 4/5 84.4 -50.7 84.4 -67. 30.4 4 6.8 30.37 -22.9 T 60 727 4/5 86.2 -44.5 67.3 -40.7 328 5.5 106.3 -121.1 T 60 727 4/5 86.2 -44.5 67.3 -40.7 328 5.5 106.3 -121.1 T 60 727 4/5 86.2 -44.5 6.2 29.4 -40.5 6.3 29.1 1.2 1.2 T 60 729 4/7 29.7 -40.5 29.5 1.2 1.2 1.2 T 60 729 6/7 185.3 -74.2 160.1 -74.4 161 5.3 40.1 -83.4 R 65 7 70.9 6/7 185.3 -74.2 160.1 -74.4 161 5.3 40.1 -83.4 R 66 84. 4/6 174.6 -76.7 158.1 -76.2 29.0 6.1 -78.4 -80.5 R 65 664 6/8 154.6 -76.7 158.1 -74.2 161 5.3 .8 40.1 -83.4 R 67 75 7/7 275.7 -80.0 281.5 -81.2 1919 2.5 41.4 121.6 -72.3 R 63 669 6/6 284.9 -78.8 255.3 -81.2 1919 2.5 41.4 121.6 -72.3 R 63 669 6/6 284.9 -78.8 255.3 -81.2 1919 2.5 41.4 121.6 -72.3 R 63 669 6/6 284.9 -78.8 255.3 -80.8 182.5 0.3 7.8 187.2 -60.9 R 64 669 6/8 184.9 -78.8 255.3 -80.8 182.5 0.3 7.8 187.2 -60.9 R 64 669 6/8 284.9 -78.8 255.3 -80.8 182.5 0.3 25.1 295.5 -80.9 R 64 669 6/8 284.9 -78.8 255.3 -80.8 182.5 0.3 25.1 295.5 -80.9 R 64 669 6/8 284.9 -78.8 255.3 -80.8 182.5 0.3 25.1 295.5 -80.9 R 64 669 6/8 284.9 -78.8 255.3 -80.8 182.5 0.3 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2  |           | 761        | 6/6             |                |                    |                |                |     |               |                    |                    |                   | R                   |
| 61 731 5/6 844 -50.7 84.4 -46.7 309 4.4 6.8 93.7 -22.9 T  60 727 4/5 66.2 -44.5 67.3 -40.7 326 5.1 106.3 -12.1 T  539 718 5/6 224.7 -49.5 289.8 -53.1 485 3.5 1 224.4 -22.6 T  547 718 6/6 159.5 -56.2 154.1 -14.8 90 7.3 3.5 1 224.4 -22.6 T  55 6624 6/7 159.6 -56.2 154.1 -14.8 90 7.3 3 4 48.4 8.8 5.7 8  55 6624 6/7 159.5 -56.2 154.1 -14.8 90 7.3 3 4 48.4 8.8 5.7 8  55 6624 6/7 159.5 -58.3 1 335.5 8.12 1919 2.5 41.4 121.6 -7.3 8 8 18.7 2  52 666 6/8 26.4 9 -76.8 26.5 3 -80.8 182 5.0 37.8 205.5 -60.9 R  52 666 6/6 264.9 -76.8 265.3 -80.8 182 5.0 37.8 205.5 -60.9 R  51 652 6/6 6/8 225.9 78.9 288.8 1.7 328 3.7 25.1 203.1 -77.0 R  48 60 60.6 6/6 325.9 -78.9 288.8 1.7 328 3.7 25.1 203.1 -77.0 R  48 60 60.6 6/6 36.5 24.1 10.8 -8.7 8 5.9 33.8 1.7 328 3.7 25.1 203.1 -77.0 R  48 60 60 6/6 355.8 5.2 37.8 7.8 7.9 3.8 8 8.0 10.3 9 6.8 11.0 T  46 (200 6) 6/6 355.8 5.2 37.8 7.9 3.8 8 8.4 1.0 T  47 612 5/7 5/7 5/7 5/7 5/7 5/7 5/7 5/7 5/7 5/7   | 62        | 740<br>725 | 5/6             |                |                    |                |                |     | ე.ბ<br>11 1   |                    | 197.0              |                   | B                   |
| 58 713 6/7 159.6 -56.0 151.1 -51.8 90 7.1 26.5 -56.4 R 56 77 7097 6/6 183.3 -74.2 169.1 -74.4 161 5.3 40.1 -78.4 -80.5 R 56 684 4/6 171.6 -76.7 158.1 -76.2 230 6.1 78.4 -80.5 R 55 687 6/7 7/7 27.5 -80.0 284.5 -84.8 233 3.8 187.2 -72.3 R 55 667 7/7 27.5 -80.0 284.5 -84.8 233 3.8 187.2 -72.3 R 56 687 6/6 27.5 -80.0 284.5 -84.8 233 3.8 187.2 -72.3 R 57 660 6/6 264.9 -76.8 265.3 -80.8 187.5 -80.0 27.8 R 51 652 6/6 225.9 -78.9 208.8 -81.7 328 3.7 25.1 203.1 -77.0 R 50 629 5/5 162.8 -67.2 153.9 -66.1 61 9.9 38.6 -60.9 R 49 619 5/6 111.4 -54.4 109.1 50.8 72 9.1 74.0 -30.3 T 48 616 5/5 81.6 -47.3 81.8 -43.3 75 8.9 91.6 -91.4 T 47 612 4/4 75.5 -37.8 75.9 -33.8 150 10.3 98.8 -11.0 T 46B 609 6/6 365.8 75.2 337.4 74.5 47 9.9 91.6 49.4 T 47 612 4/4 75.5 -37.8 75.9 -33.8 150 10.3 98.8 -11.0 T 46B 609 6/6 365.8 75.2 337.4 74.5 47 9.9 24.4 5 79.0 N 44 (BB20) 595 6/6 47.0 75.0 32.0 78.6 55 9.1 14.3 49.2 77.1 N 41 586 5/5 348.4 75.9 32.9 74.6 237 5.0 253.8 76.0 N 42 590 6/6 47.0 75.0 32.0 78.6 55 9.1 14.3 49.2 77.1 N 41 586 5/5 348.4 75.9 329.9 74.6 237 5.0 253.8 76.0 N 39 583 6/7 351.6 60.9 342.8 60.3 496 3.0 15.5 197.0 61.2 N 39 583 6/7 351.6 60.9 342.8 60.3 496 3.0 15.5 197.0 61.2 N 38 571 5/5 340.6 60.9 342.8 60.3 496 3.0 15.5 197.0 61.2 N 38 571 5/5 340.6 60.9 342.8 60.3 496 3.0 15.5 197.0 61.2 N 38 571 5/5 340.6 60.9 342.8 60.3 496 3.0 15.5 197.0 61.2 N 38 586 6/6 318.8 77.4 300.5 73.7 278 4.0 26.0 273.0 63.0 N 39 583 6/7 351.6 60.9 342.8 60.3 496 3.0 15.5 197.0 61.2 N 36 560 6/6 38.5 75.3 18.0 17.3 76.9 1.1 3.9 6.8 -10.0 7.3 1.2 N 37 560 6/6 4/6 348.8 50.0 343.9 49.4 75.5 3.3 10.4 190.2 53.7 N 38 580 6/6 318.8 77.4 300.5 6.2 1.1 16.0 7.1 17.2 N 38 571 5/5 340.6 6.9 34.8 50.0 34.9 6.0 1.1 37.0 18.2 14.4 25.3 T 31 422 5/5 340.0 60.9 34.8 50.0 34.9 6.0 1.1 37.0 18.5 14.2 25.8 19.0 18.2 14.2 14.2 26.8 1.1 11.2 N 38 580 6/6 380.1 75.3 18.1 317.3 15.2 40 10.8 12.4 14.2 26.8 1.9 14.2 14.2 26.8 1.1 14.2 26.8 1.1 14.2 26.8 1.1 14.2 26.8 1.1 14.2 14.2 26.8 1.1 14.2 14.2 26.8 1.1 14.2 14.2 26.8 1.1 14.2 14.2 14.2 14.2 14.2 14.2 14.2 |           | 731        |                 |                |                    |                |                |     |               | 6.8                | 93.7               | -22.9             | Т                   |
| 58 713 6/7 159.6 -56.0 151.1 -51.8 90 7.1 26.5 -56.4 R 56 77 7097 6/6 183.3 -74.2 169.1 -74.4 161 5.3 40.1 -78.4 -80.5 R 56 684 4/6 171.6 -76.7 158.1 -76.2 230 6.1 78.4 -80.5 R 55 687 6/7 7/7 27.5 -80.0 284.5 -84.8 233 3.8 187.2 -72.3 R 55 667 7/7 27.5 -80.0 284.5 -84.8 233 3.8 187.2 -72.3 R 56 687 6/6 27.5 -80.0 284.5 -84.8 233 3.8 187.2 -72.3 R 57 660 6/6 264.9 -76.8 265.3 -80.8 187.5 -80.0 27.8 R 51 652 6/6 225.9 -78.9 208.8 -81.7 328 3.7 25.1 203.1 -77.0 R 50 629 5/5 162.8 -67.2 153.9 -66.1 61 9.9 38.6 -60.9 R 49 619 5/6 111.4 -54.4 109.1 50.8 72 9.1 74.0 -30.3 T 48 616 5/5 81.6 -47.3 81.8 -43.3 75 8.9 91.6 -91.4 T 47 612 4/4 75.5 -37.8 75.9 -33.8 150 10.3 98.8 -11.0 T 46B 609 6/6 365.8 75.2 337.4 74.5 47 9.9 91.6 49.4 T 47 612 4/4 75.5 -37.8 75.9 -33.8 150 10.3 98.8 -11.0 T 46B 609 6/6 365.8 75.2 337.4 74.5 47 9.9 24.4 5 79.0 N 44 (BB20) 595 6/6 47.0 75.0 32.0 78.6 55 9.1 14.3 49.2 77.1 N 41 586 5/5 348.4 75.9 32.9 74.6 237 5.0 253.8 76.0 N 42 590 6/6 47.0 75.0 32.0 78.6 55 9.1 14.3 49.2 77.1 N 41 586 5/5 348.4 75.9 329.9 74.6 237 5.0 253.8 76.0 N 39 583 6/7 351.6 60.9 342.8 60.3 496 3.0 15.5 197.0 61.2 N 39 583 6/7 351.6 60.9 342.8 60.3 496 3.0 15.5 197.0 61.2 N 38 571 5/5 340.6 60.9 342.8 60.3 496 3.0 15.5 197.0 61.2 N 38 571 5/5 340.6 60.9 342.8 60.3 496 3.0 15.5 197.0 61.2 N 38 571 5/5 340.6 60.9 342.8 60.3 496 3.0 15.5 197.0 61.2 N 38 586 6/6 318.8 77.4 300.5 73.7 278 4.0 26.0 273.0 63.0 N 39 583 6/7 351.6 60.9 342.8 60.3 496 3.0 15.5 197.0 61.2 N 36 560 6/6 38.5 75.3 18.0 17.3 76.9 1.1 3.9 6.8 -10.0 7.3 1.2 N 37 560 6/6 4/6 348.8 50.0 343.9 49.4 75.5 3.3 10.4 190.2 53.7 N 38 580 6/6 318.8 77.4 300.5 6.2 1.1 16.0 7.1 17.2 N 38 571 5/5 340.6 6.9 34.8 50.0 34.9 6.0 1.1 37.0 18.2 14.4 25.3 T 31 422 5/5 340.0 60.9 34.8 50.0 34.9 6.0 1.1 37.0 18.5 14.2 25.8 19.0 18.2 14.2 14.2 26.8 1.1 11.2 N 38 580 6/6 380.1 75.3 18.1 317.3 15.2 40 10.8 12.4 14.2 26.8 1.9 14.2 14.2 26.8 1.1 14.2 26.8 1.1 14.2 26.8 1.1 14.2 26.8 1.1 14.2 14.2 26.8 1.1 14.2 14.2 26.8 1.1 14.2 14.2 26.8 1.1 14.2 14.2 14.2 14.2 14.2 14.2 14.2 |           | 727        | $\frac{3}{4}/5$ |                |                    |                |                |     |               | 0.0                |                    |                   | $\hat{ar{	ext{T}}}$ |
| 57   |           | 718        | 5/6             |                |                    |                |                |     |               |                    | 224.4              | -22.6             | ${ m T}$            |
| 56 684 4/6 174.6 -76.7 158.1 -76.2 230 6.1 78.4 -80.5 R 55 687 6/6 150.5 -83.1 133.5 -81.2 1919 2.5 44.4 121.6 -76.3 R 54 673 7/7 263.4 8.06 266.4 -84.6 487 2.7 191.1 -63.7 R 52 660 6/6 26.1 -76.8 80.6 266.4 -84.6 487 2.7 191.1 -63.7 R 51 662 6/6 6/6 22.9 -76.8 265.3 -80.8 182 5.0 37.8 205.5 -60.9 R 51 662 6/6 16.6 16.6 16.8 -67.8 18.3 -67 |           | 713        |                 |                |                    |                |                |     |               |                    | 26.5               |                   | $\mathbf{R}$        |
| 55 681 6/6 150.5 -83.1 133.5 -81.2 1919 2.5 41.4 121.6 -72.3 R 54 673 7/7 275.7 -80.9 284.5 -84.8 233 3.8 187.2 -0.9 R 53 669 7/7 265.4 -80.6 266.4 -84.6 487 2.7 1911.1 -83.7 8 51 662 6/6 26.9 -76.8 265.3 -80.8 185.5 0 37.8 205.5 -0.09 R 51 662 6/6 26.9 -76.8 265.3 -80.8 185.5 0 37.8 205.5 -0.09 R 51 662 6/6 5/6 261.9 -76.8 265.3 -80.8 185.7 2.5 1 203.1 -77.0 R 51 662 6/6 5/5 81.6 -47.3 81.8 -43.3 75 8.9 9.6 6 30.3 R 48 6/6 5/5 81.6 -47.3 81.8 -43.3 75 8.9 9.6 6 39.3 R 47 6/12 4/4 75.5 -37.8 75.9 -33.8 150 10.3 96.8 -11.0 T 46/12 6/09 0/4 46/12 6/09 0/4 46 6/06 6/6 35.5 80.0 334.8 79.4 235 4.4 23.3 291.6 79.5 N 45 (BB21) 598 6/6 355.8 75.2 337.4 74.5 47 9.9 244.5 79.0 N 44 (BB2) 599 6/6 44.6 69.0 34.5 72.6 308 3.8 84.1 72.3 N 43 592 6/6 47.0 75.0 32.0 78.6 55 9.1 14.3 49.2 77.1 N 42 509 6/6 5/5 5.9 1.2 33.6 80.8 136 5.1 22.5 343.0 83.1 N 43 592 6/6 34.6 69.0 34.5 72.6 308 3.8 84.1 72.3 N 44 500 6/6 25.9 70.2 32.0 78.6 55 9.1 14.3 49.2 77.1 N 45 (BB2) 595 6/6 36.6 35.9 79.3 32.0 78.6 55 9.1 14.3 49.2 77.1 N 46 506 6/6 5/5 5.9 17.0 32.0 78.6 55 9.1 14.3 49.2 77.1 N 47 506 6/6 36.9 32.9 70.3 32.0 78.6 55 9.1 14.3 49.2 77.1 N 38 571 5/5 340.0 73.1 326.0 71.3 76 9.1 5.7 24.3 N 39 583 6/6 313.8 77.5 32.8 8.0 34.0 73.3 76 9.1 5.7 32.0 34.0 33.8 74.4 53.4 34.4 34.3 75.9 3.3 10.4 190.2 34.3 74.4 54.5 34.3 34.4 540 0/6 31 506 506 6/6 30.9 34.2 8.0 34.4 34.4 27.3 37.4 4.5 3.3 10.4 190.2 57.0 N 36 (BB10) 488 6/6 316.6 30.4 314.4 27.3 27.8 4.0 5.8 22.0 30.8 7.7 1.7 1.9 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7   |           |            | 6/6             |                |                    |                |                |     |               |                    |                    |                   | R                   |
| 54 675 7/7 275.7 80.9 284.5 84.8 253 3.8 187.2 -60.9 R 53 669 6/6 264.9 -76.8 0.66 264.8 46.6 487 2.7 191.1 -63.7 R 52 660 6/6 264.9 -76.8 265.3 80.8 182 5.0 37.8 205.5 -60.9 R 51 662 6/6 25.9 -78.9 208.8 81.7 2.8 37 25.1 203.1 -77.0 R 50 629 5/5 162.8 -67.2 153.9 -66.1 61 9.9 386.6 -68.3 R 49 619 5/6 114.4 -54.4 1091.1 -50.8 72.9 1 74.0 -36.3 R 49 619 5/6 114.4 -54.4 1091.1 -50.8 72.9 1 74.0 -36.3 R 40 619 5/6 114.4 -54.4 1091.1 -50.8 72.9 1 74.0 -36.3 R 47 612 5/4 37 5.7 -37.8 75.9 -33.8 150 10.3 96.6 -10.4 T 46 66 6/6 356.7 80.0 344.8 79.4 235 4.4 23.3 291.6 79.5 N 44 (EB20) 595 6/6 44.6 69.0 34.5 72.6 308 3.8 84.1 72.3 N 42 590 6/6 25.9 79.2 358.7 80.8 176 5.1 32.5 343.0 83.1 N 43 592 6/6 47.0 75.0 32.0 78.6 55 9.1 14.3 49.2 77.1 N 42 590 6/6 25.9 79.2 358.7 80.8 176 5.1 32.5 343.0 83.1 N 40 585 6/6 313.8 77.4 300.5 73.7 278 4.0 26.0 273.0 63.0 N 40 585 6/6 313.8 77.4 300.5 73.7 278 4.0 26.0 273.0 63.0 N 38 571 5/5 348.4 75.9 32.9 74.6 237 5.0 255.8 76.0 N 38 571 5/5 340.6 73.1 326.0 71.3 76 9.1 14.3 49.2 59.3 43.0 83.1 N 38 571 5/5 340.6 73.1 326.0 71.3 76 9.1 14.3 25.5 26.3 N 38 571 5/5 340.6 73.1 326.0 71.3 76 9.1 14.3 25.5 14.0 14.3 34.2 3.3 34.0 83.1 N 39 583 6/6 313.8 77.4 300.5 73.7 278 4.0 26.0 273.0 63.0 N 38 571 5/5 340.6 73.1 326.0 71.3 76 9.1 14.3 49.2 55.8 14.1 37.3 15.2 40 10.8 32.5 34.3 10.4 190.2 53.7 13.3 14.7 2 5/5 186.0 -62.8 176.2 -63.4 13.5 -66.9 0.3 354.1 -69.7 R 30 469 0/4 29 (EB17) 488 6/6 316.5 30.4 314.4 27.3 27.9 40.0 5.8 22.0 30.8 3.7 13.1 472 5/5 186.0 -62.8 176.2 -63.4 13.5 -66.9 0.3 354.1 -69.7 R 26 (EBBC) 460 5/5 186.0 -62.8 176.2 -63.4 13.5 -66.9 9.0 354.1 -69.7 R 31 472 5/5 186.0 -62.8 176.2 -63.4 13.5 -66.9 9.0 354.1 -69.7 R 31 472 5/5 186.0 -62.8 176.2 -63.4 13.5 -66.9 9.0 354.1 -69.7 R 32 (EB10) 488 6/6 316.8 -50.4 188.5 -61.0 152 5.9 330.4 -66.4 R 30 40 40 40 40 40 40 40 40 40 40 40 40 40  |           | 684        | 4/6             |                |                    |                |                |     |               | 41.4               |                    |                   | R                   |
| 53 669 7/7 265.4 8-80.6 266.4 8-84.6 487 2.7 191.1 6-83.7 R 51 652 660 6/6 225.9 -76.8 265.3 8-08.8 125 5.0 37.8 205.5 -60.9 R 51 652 6/6 225.9 -78.9 208.8 -81.7 328 3.7 25.1 203.1 -77.0 R 50 629 5/5 162.8 6-72 153.9 -66.1 61 9.9 38.6 -68.3 R 49 619 5/6 111.4 -54.4 109.1 -50.8 72 9.1 74.0 -86.3 T 48 616 5/5 81.6 -47.3 81.8 -43.3 75 8.9 91.6 19.9 46.6 68.3 R 48 616 5/5 81.6 -47.3 81.8 -43.3 75 8.9 91.6 19.9 46.6 19.9 46.6 19.9 47.7 1086.3 T 48 616 606 606 35.5 8 75.2 37.8 75.9 -33.8 150 10.3 86.8 -11.0 T 4607 607 606 35.5 8 75.2 37.4 74.5 47 9.9 244.5 79.0 N 45 (EB21) 598 6/6 35.8 75.2 337.4 74.5 47 9.9 244.5 79.0 N 44 (EB20) 595 6/6 47.0 75.0 32.0 78.6 55 9.1 14.3 49.2 77.1 N 41 586 5/5 348.4 75.9 329.9 74.6 237 5.0 25.3 8 76.0 N 41 586 5/5 348.4 75.9 329.9 74.6 237 5.0 25.3 8 76.0 N 39 583 6/7 351.6 60.9 342.8 60.3 496 3.0 15.5 197.0 64.2 N 38 571 5/5 340.6 73.1 326.0 71.3 76 9.1 243.1 71.2 N 37 566 6/6 33.8 77.4 30.5 73.7 278 4.0 26.0 273.0 63.0 N 39 583 6/7 351.6 60.9 342.8 60.3 496 3.0 15.5 197.0 64.2 N 37 566 6/6 33.5 52.7 341.1 51.9 10 6.7 195.1 55.4 N 36 562 6/6 34.5 35.7 32.9 32.0 71.3 76 9.1 243.1 71.2 N 37 566 6/6 34.5 35.7 37.7 273.4 10 26.0 273.0 63.0 N 39 583 6/7 351.6 60.9 342.8 60.3 496 3.0 15.5 197.0 64.2 N 37 566 6/6 34.5 52.7 341.1 51.9 10 6.7 195.1 55.4 N 36 562 6/6 34.5 52.7 341.1 51.9 10 6.7 195.1 55.4 N 37 566 6/6 34.5 52.7 341.1 51.9 10 6.7 195.1 55.4 N 38 571 5/5 340.6 6.7 13.3 26.0 71.3 76 9.1 243.1 71.2 N 36 562 6/6 34.5 52.7 341.1 51.9 10 6.7 195.1 55.4 N 37 566 6/6 34.5 52.7 341.1 51.9 10 6.7 195.1 55.4 N 38 571 5/5 340.6 85.8 5.9 18.8 37.3 37.3 52.9 40.0 8 38.8 N 39 583 6/7 35.8 6/6 138.5 88.1 373.3 15.2 40.0 8 33.1 N 39 583 6/6 38.5 86.6 6/8 38.5 88.5 15.0 8.8 N 30 584 1.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0  | 55<br>54  |            | 0/0<br>7/7      |                |                    |                |                |     |               | 41.4               |                    | 60.0              | R<br>D              |
| 52 660 6/6 264.9 -76.8 265.3 -80.8 182 5.0 37.8 205.5 -60.9 R 51 652 6/6 225.9 -78.9 208.8 -81.7 328 3.7 -25.1 203.1 -77.0 R 50 629 5/5 162.8 -67.2 153.9 -66.1 61 9.9 38.6 -68.3 R 48 6/6 5/5 81.6 -47.3 81.8 -43.3 75 8.9 91.6 -10.4 T 48 6/6 5/5 81.6 -47.3 81.8 -43.3 75 8.9 91.6 -10.4 T 46 606 6/6 35.7 80.0 334.8 79.4 235 4.4 23.3 291.6 79.5 N 45 (BB2) 598 6/6 356.7 80.0 334.8 79.4 235 4.4 23.3 291.6 79.5 N 46 (BB2) 598 6/6 356.7 80.0 334.8 79.4 235 4.4 23.3 291.6 79.5 N 43 592 6/6 46.6 6.6 6.6 0.6 0.6 0.7 1.2 0.7  | 54<br>53  |            | 7/7             |                |                    |                |                |     |               |                    |                    |                   | R<br>B              |
| 51   | 52        |            | 6/6             |                |                    |                |                |     |               | 37.8               | 205.5              |                   | R.                  |
| 50 629 5/5 162.8 -67.2 153.9 -66.1 61 9.9 9 38.6 -68.3 R 49 619 5/6 111.4 -54.4 1091 -50.8 72 9.1 774.0 -36.3 T 48 616 5/5 81.6 -47.3 81.8 -43.3 75 8.9 91.6 -19.4 T 46B" 609 0/4 46 690 0/4 46 690 6/6 356.7 80.0 334.8 79.4 235 4.4 23.3 291.6 79.5 N 45 (EB21) 598 6/6 356.8 75.2 337.4 74.5 47 9.9 244.5 79.0 N 45 (EB21) 598 6/6 46.6 68.0 34.5 72.6 308 3.8 S 41 72.3 N 43 592 6/6 47.0 75.0 32.0 78.6 55 91.1 4.3 49.2 77.1 N 42 596 6/6 47.0 75.0 32.0 78.6 55 91.1 4.3 49.2 77.1 N 43 592 6/6 47.0 75.0 32.0 78.6 55 91.1 4.3 49.2 77.1 N 40 565 5/6 25.9 79.2 338.7 80.8 17.5 20.0 23.0 63.0 N 40 565 5/6 25.9 79.2 38.7 80.8 17.5 20.0 23.0 63.0 N 40 565 5/6 25.9 79.2 38.7 80.8 17.5 20.0 25.0 25.0 25.0 25.0 25.0 25.0 25  |           |            | 6/6             |                |                    |                |                |     |               |                    |                    |                   | R                   |
| 47 612 4/4 75.5 -37.8 75.9 -33.8 150 10.3 96.8 -11.0 T  468 609 0/4  46 606 6/6 356.7 80.0 33.8 79.4 235 4.4 23.3 291.6 79.5 N  44 (EB20) 598 6/6 356.8 75.2 337.4 74.5 47 9.9 244.5 79.0 N  44 (EB20) 595 6/6 44.6 66.0 34.5 72.6 308 3.8 84.1 72.3 N  42 590 6/6 25.9 79.2 358.7 80.8 176 51 32.5 333.0 83.1 N  40 585 6/6 313.8 77.4 30.5 73.7 278 4.0 26.0 273.0 63.0 N  40 585 6/6 313.8 77.4 30.5 73.7 278 4.0 26.0 273.0 63.0 N  39 583 6/7 351.6 60.9 342.8 60.3 34.8 96 3.0 15.5 197.0 64.2 N  38 571 5/5 340.6 73.1 326.0 71.3 76 9.1 243.1 71.2 N  36 562 6/6 37.5 52.7 341.1 51.9 101 6.7 195.1 55.4 N  37 566 6/6 30.8 33.9 49.8 50.0 341.9 101 6.7 195.1 55.4 N  38 571 5/5 340.6 73.1 326.0 71.3 76 9.1 243.1 71.2 N  38 571 5/5 340.6 73.1 32.6 71.3 76 9.1 243.1 71.2 N  38 571 5/5 56 6/6 347.5 52.7 341.1 51.9 101 6.7 195.1 55.4 N  36 EB2 6/6 347.5 52.7 341.1 51.9 101 6.7 195.1 55.4 N  37 566 6/6 30.8 18.1 317.3 15.2 40 10.8 214.4 25.3 T  38 (EB14) 551 488 6/6 316.6 30.4 314.4 27.3 278 4.0 5.8 220.0 30.8 T  31 472 5/5 186.0 -62.8 176.2 63.4 135 6.6 9.0 354.1 -69.7 R  30 469 0/4  29 (EB7) 463 5/5 44.1 61.0 49.2 57.0 133 7.1 126.8 -19.6 T  29 (EB7) 43 6/6 204.3 -57.3 197.0 59.5 354 4.1 39.6 316.6 -30.3 N  22 (EB7) 43 6/7 203.3 -61.7 192.5 -64.1 154 5.4 25.0 320.8 -69.5 R  23 442 424 6/6 235.5 -76.2 21.6 81.2 137 5.9 23.4 210.7 -73.7 R  23 48 5/5 186.8 59.4 188.5 -61.0 152 5.9 33.4 4.1 30.9 -69.5 R  18 388 5/6 191.8 -64.1 719.2 -65.6 65 9.6 8.5 348.1 7.7 6.8 11  30 29 6/6 207.7 -66 175.9 -78.2 229 4.4 130.9 -87.3 R  21 40 6/6 202.1 -76.6 175.9 -78.2 229 4.4 130.9 -87.3 R  21 40 6/6 202.1 -76.6 175.9 -78.2 229 4.4 130.9 -87.3 R  21 40 6/6 202.1 -76.6 175.9 -78.2 229 4.4 130.9 -87.3 R  22 410 5/5 157.8 -51.1 151.0 -49.1 205 5.4 S  18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 7.7 E-7.5 6.8 R  19 (EB1) 398 5/6 6/6 176.5 276.5 -73.8 25.5 80.5 123 6.1 15.7 199.1 -55.6 R  10 272 407 07 09 269 0/6  20 407 70 70 70 70 70 70 70 70 70 70 70 70 7   | 50        |            | 5/5             | 162.8          | -67.2              | 153.9          |                | 61  | 9.9           |                    | 38.6               |                   | $^{\mathrm{R}}$     |
| 47 612 4/4 75.5 -37.8 75.9 -33.8 150 10.3 96.8 -11.0 T  468 609 0/4  46 606 6/6 356.7 80.0 33.8 79.4 235 4.4 23.3 291.6 79.5 N  44 (EB20) 598 6/6 356.8 75.2 337.4 74.5 47 9.9 244.5 79.0 N  44 (EB20) 595 6/6 44.6 66.0 34.5 72.6 308 3.8 84.1 72.3 N  42 590 6/6 25.9 79.2 358.7 80.8 176 51 32.5 333.0 83.1 N  40 585 6/6 313.8 77.4 30.5 73.7 278 4.0 26.0 273.0 63.0 N  40 585 6/6 313.8 77.4 30.5 73.7 278 4.0 26.0 273.0 63.0 N  39 583 6/7 351.6 60.9 342.8 60.3 34.8 96 3.0 15.5 197.0 64.2 N  38 571 5/5 340.6 73.1 326.0 71.3 76 9.1 243.1 71.2 N  36 562 6/6 37.5 52.7 341.1 51.9 101 6.7 195.1 55.4 N  37 566 6/6 30.8 33.9 49.8 50.0 341.9 101 6.7 195.1 55.4 N  38 571 5/5 340.6 73.1 326.0 71.3 76 9.1 243.1 71.2 N  38 571 5/5 340.6 73.1 32.6 71.3 76 9.1 243.1 71.2 N  38 571 5/5 56 6/6 347.5 52.7 341.1 51.9 101 6.7 195.1 55.4 N  36 EB2 6/6 347.5 52.7 341.1 51.9 101 6.7 195.1 55.4 N  37 566 6/6 30.8 18.1 317.3 15.2 40 10.8 214.4 25.3 T  38 (EB14) 551 488 6/6 316.6 30.4 314.4 27.3 278 4.0 5.8 220.0 30.8 T  31 472 5/5 186.0 -62.8 176.2 63.4 135 6.6 9.0 354.1 -69.7 R  30 469 0/4  29 (EB7) 463 5/5 44.1 61.0 49.2 57.0 133 7.1 126.8 -19.6 T  29 (EB7) 43 6/6 204.3 -57.3 197.0 59.5 354 4.1 39.6 316.6 -30.3 N  22 (EB7) 43 6/7 203.3 -61.7 192.5 -64.1 154 5.4 25.0 320.8 -69.5 R  23 442 424 6/6 235.5 -76.2 21.6 81.2 137 5.9 23.4 210.7 -73.7 R  23 48 5/5 186.8 59.4 188.5 -61.0 152 5.9 33.4 4.1 30.9 -69.5 R  18 388 5/6 191.8 -64.1 719.2 -65.6 65 9.6 8.5 348.1 7.7 6.8 11  30 29 6/6 207.7 -66 175.9 -78.2 229 4.4 130.9 -87.3 R  21 40 6/6 202.1 -76.6 175.9 -78.2 229 4.4 130.9 -87.3 R  21 40 6/6 202.1 -76.6 175.9 -78.2 229 4.4 130.9 -87.3 R  21 40 6/6 202.1 -76.6 175.9 -78.2 229 4.4 130.9 -87.3 R  22 410 5/5 157.8 -51.1 151.0 -49.1 205 5.4 S  18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 7.7 E-7.5 6.8 R  19 (EB1) 398 5/6 6/6 176.5 276.5 -73.8 25.5 80.5 123 6.1 15.7 199.1 -55.6 R  10 272 407 07 09 269 0/6  20 407 70 70 70 70 70 70 70 70 70 70 70 70 7   |           |            | 5/6             |                |                    |                |                |     |               |                    | 74.0               |                   | ${ m T}$            |
| 46B*   609   |           |            |                 |                |                    |                |                |     |               |                    | 94.6               |                   | $_{\mathrm{T}}$     |
| 46   |           |            | 4/4             | 75.5           | -37.8              | 75.9           | -33.8          | 150 | 10.3          |                    | 96.8               | -11.0             | T                   |
| 44 (EB21) 598 6/6 355.8 75.2 337.4 74.5 47 9.9 244.5 79.0 N 44 (EB20) 595 6/6 44.6 69.0 34.5 72.6 308 3.8 1.8 1.1 72.3 N 42 590 6/6 47.0 75.0 32.0 78.6 55 9.1 14.3 49.2 77.1 N 42 590 6/6 25.9 79.2 358.7 80.8 176 55. 91.1 14.3 49.2 77.1 N 41 586 5/5 348.4 75.9 329.9 74.6 237 5.0 253.8 76.0 N 40 685 6/6 313.8 77.4 30.05 73.7 278 4.0 26.0 253.8 76.0 N 39 583 6/7 351.6 60.9 342.8 60.3 496 3.0 15.5 197.0 642 N 38 571 5/5 340.6 73.1 326.0 71.3 76 9.1 243.1 71.2 N 37 566 6/6 37.5 349.8 50.0 349.8  |           | 609        |                 | 256.7          | 90.0               | 224.0          | 70.4           | 995 | 4.4           | 22.2               | 201.6              | 70.5              | NT                  |
| 44 (EB20)  |           |            | 6/6             |                |                    |                |                |     |               | 23.3               | 291.0              |                   | IN<br>NI            |
| 43 592 6/6 47.0 75.0 32.0 78.6 55 9.1 14.3 49.2 77.1 N 41 586 5/5 348.4 75.9 329.9 71.6 3237 5.0 253.8 76.0 N 41 586 5/5 348.4 75.9 329.9 71.6 237 5.0 253.8 76.0 N 39 583 6/7 351.6 60.9 342.8 60.3 496 3.0 15.5 197.0 64.2 N 38 571 5/5 340.6 73.1 326.0 71.3 76 9.1 243.1 71.2 N 37 566 6/6 30.91.7 5.3 298.4 71.4 226 4.5 25.5 268.7 59.8 N 36 562 6/6 347.5 52.7 341.1 51.9 101 6.7 195.1 55.4 N 37 566 6/6 347.5 52.7 341.1 51.9 101 6.7 195.1 55.4 N 38 571 551 4/5 349.8 50.0 343.9 49.4 755 3.3 10.4 190.2 53.7 N 38 540 76 78 78 78 78 78 78 78 78 78 78 78 78 78  |           | 595        |                 |                |                    |                |                |     |               |                    |                    |                   | N                   |
| 42 590 6/6 25.9 79.2 35.8.7 80.8 176 5.1 32.5 343.0 83.1 N 41 586 5/5 348.4 75.9 329.9 74.6 237 5.0 253.8 76.0 N 40 585 6/6 313.8 77.4 300.5 73.7 278 4.0 26.0 273.0 63.0 N 39 583 6/7 351.6 60.9 342.8 60.3 496. 30 15.5 197.0 64.2 N 38 571 5/5 340.6 73.1 326.0 71.3 76 9.1 243.1 71.2 N 36 562 6/6 347.5 52.7 341.1 51.9 101 6.7 195.1 55.4 N 36 562 6/6 347.5 52.7 341.1 51.9 101 6.7 195.1 55.4 N 35 (EB14) 551 4/5 340.8 50.0 343.9 49.4 755 3.3 10.4 190.2 53.7 N 36 586 6/6 318.5 18.1 317.3 15.2 40 10.8 214.4 25.3 T 32 (EB10) 488 6/6 316.6 30.4 314.4 27.3 278 4.0 5.8 220.0 30.8 T 31 49 0/4 29 (EB7) 469 0/4 29 (EB7) 463 5/5 44.1 61.0 49.2 57.0 133 7.1 126.8 19.6 12.2 12.2 12.2 12.2 12.3 12.2 12.2 12.3 12.2 12.3 12.2 12.3 12.2 12.3 12.2 12.3 12.2 12.3 12.2 12.3 12.2 12.3 12.2 12.3 12.3   |           |            | $\frac{6}{6}$   |                |                    |                |                |     |               | 14.3               | 49.2               |                   | N                   |
| 411 586 5/5 348.4 75.9 329.9 74.6 237 5.0 253.8 76.0 N 30 583 6/7 351.6 60.9 342.8 60.3 496 3.0 15.5 197.0 64.2 N 31 583 6/7 351.6 60.9 342.8 60.3 496 3.0 15.5 197.0 64.2 N 32 586 6/6 30.1 75.3 298.4 71.4 226 4.5 25.5 268.7 59.8 N 33 586 562 6/6 30.1 75.3 298.4 71.4 226 4.5 25.5 268.7 59.8 N 36 562 6/6 347.5 52.7 341.1 51.9 101 6.7 195.1 55.4 N 35 (EB14) 551 4/5 349.8 50.0 343.9 49.4 755 3.3 10.4 190.2 53.7 N 34 540 0/6 348.8 6/6 318.5 18.1 317.3 15.2 40 10.8 214.4 25.3 T 32 (EB10) 488 6/6 316.6 30.4 314.4 27.3 27.8 4.0 5.8 220.0 30.8 T 31 472 5/5 186.0 62.8 176.2 63.4 135 6.6 9.0 354.1 6-9.7 R 29 (EB7) 463 5/5 44.1 61.0 49.2 57.0 133 7.1 126.8 -19.6 T 28 (EB6C) 460 5/6 204.3 57.3 197.0 59.5 334 4.1 39.6 316.6 6-33.3 R 22 4 424 424 6/6 238.5 -76.2 221.6 81.2 137 5.9 23.4 210.7 -73.7 R 23 4 488 6/6 238.5 -76.2 221.6 81.2 137 5.9 23.4 210.7 -73.7 R 23 4 448 6/6 238.5 -76.2 221.6 81.2 137 5.9 23.4 210.7 -73.7 R 23 4 48 5/5 186.3 83.5 138.2 82.2 123 7.4 125.5 9 30.4 469 4/4 424 6/6 238.5 -76.2 221.6 81.2 137 5.9 23.4 210.7 -73.7 R 23 4 48 5/5 186.3 83.5 138.2 82.2 123 7.4 128.5 -73.3 R 22 4/0 5/6 247.5 -65.4 242.6 -71.1 127 6.8 243.9 -59.1 R 23 418 5/5 186.3 83.5 138.2 82.2 123 7.4 128.5 -73.3 R 21 406 4/6 156.2 48.0 150.2 49.1 127 6.9 14.8 27.7 -50.5 R 19 (EB1) 398 6/6 191.8 64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 17 383 6/6 202.1 -76.6 17.9 -78.2 229 4.4 130.9 -87.3 R 19 (EB1) 398 6/6 177.2 -65.0 164.4 -64.7 97 6.9 14.8 27.4 -47.7 T 20 401 6/6 202.1 -76.6 17.9 -78.2 229 4.4 130.9 -87.3 R 19 (EB1) 398 6/6 177.2 -65.0 164.4 -64.7 97 6.9 14.8 27.4 -47.7 T 20 401 6/6 202.1 -76.6 17.9 -78.2 229 4.4 130.9 -87.3 R 19 (EB1) 398 6/6 191.8 64.4 179.2 -65.6 65 9.6 8.5 38.5 1.1 1.5 1.7 26.2 T 10 20 401 6/6 20.6 67.6 25.5 -73.8 83.6 97 6.8 191.7 26.2 T 10 20 401 6/6 20.6 67.6 5.7 5.8 83.6 97 6.8 191.7 26.2 T 10 20 401 6/6 20.6 67.6 5.7 5.8 83.6 97 7 5.8 83.6 97 7 5.8 83.6 97 7 5.8 83.6 97 7 5.8 83.6 97 7 5.5 88 8 191.7 5.5 6.8 R 10 222 97 7/7 262.0 -70.0 261.0 -70.0 261.0 -77.0 187 4.4 48.5 9.7 29.2 1.5 5.8 R 10 222 97 7/7  |           |            | 6/6             |                |                    |                | 80.8           |     |               |                    | 343.0              |                   | N                   |
| 40 585 6/6 313.8 77.4 300.5 73.7 278 4.0 26.0 273.0 63.0 N 39 583 6/7 351.6 60.9 342.8 60.3 496 3.0 15.5 197.0 64.2 N 38 571 5/5 340.6 73.1 326.0 71.3 76 9.1 243.1 71.2 N 37 566 6/6 30.91. 75.3 298.4 71.4 226 4.5 25.5 268.7 59.8 N 36 562 6/6 347.5 52.7 341.1 51.9 101 6.7 195.1 55.4 N 35 (EB14) 551 4/5 349.8 50.0 343.9 49.4 755 3.3 10.4 190.2 53.7 N 34 540 0/6 33 5588 6/6 318.5 18.1 317.3 15.2 40 10.8 214.4 25.3 T 32 (EB10) 488 6/6 316.6 30.4 314.4 27.3 278 4.0 5.8 220.0 30.8 T 31 472 5/5 186.0 -62.8 176.2 -63.4 135 6.6 9.0 354.1 -69.7 R 30° 469 0/4 29 (EB7) 463 5/5 44.1 -61.0 49.2 57.0 133 7.1 126.8 1-96.7 R 28 (EB6C) 460 5/6 204.3 57.3 197.0 59.5 354 4.1 39.6 316.6 -63.3 R 25 443 6/7 20.3 -61.7 192.5 -64.1 154 5.4 25.0 320.8 -66.3 T 24 424 6/6 238.5 -76.2 221.6 -81.2 137 5.9 23.4 210.7 -73.7 R 238 420 5/6 247.5 -65.4 242.6 -71.1 127 6.8 243.9 59.1 R 238 420 5/6 247.5 -65.4 242.6 -71.1 127 6.8 243.9 -59.1 R 238 448 5/5 186.3 -83.5 1382 -82.2 123 7.4 128.5 -73.3 R 238 420 5/6 247.5 -65.4 242.6 -71.1 127 6.8 243.9 -59.1 R 24 424 6/6 238.5 -76.2 221.6 -81.2 137 5.9 23.4 210.7 -73.7 R 238 420 5/6 247.5 -65.4 242.6 -71.1 127 6.8 243.9 -59.1 R 239 448 5/5 186.3 -83.5 1382 -82.2 123 7.4 128.5 -73.3 R 220 401 6/6 202.1 -76.6 175.9 -78.2 229 4.4 130.9 -87.3 R 19 (EB1) 398 6/6 177.2 -65.0 164.4 -64.7 95 6.9 14.8 27.4 -47.7 T 20 401 6/6 202.1 -76.6 175.9 -78.2 229 4.4 130.9 -87.3 R 18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 16 378 5/5 245.9 -75.6 193.1 -78.7 55 9.3 6.8 99.7 24.5 T 10 222 4/0 6/6 27.7 -65.5 73.8 25.5 73.1 42 10.4 7.3 64.2 64.0 N 11 307 6/6 80.8 77.6 77.8 83.6 97 6.8 16.5 64.8 N 10 272 0/7 10 265 5/5 246.7 -19.1 245.8 -25.8 100 8.8 272.9 -22.4 T 10 6 24/5 6/6 60.1 18.3 59.0 24.7 55.5 9.3 6.8 99.7 24.5 T 10 6 24/5 6/6 60.1 18.3 59.0 24.7 55.5 9.3 6.8 99.7 24.5 T 10 6 24/5 6/6 207.7 -4.7 267.8 -71.4 59 8.8 268 0.6 21.1 1.5 9.8 R 10 2229 7/7 282.0 -70.0 261.0 -77.0 187 4.4 48 |           | 586        | 5/5             |                | 75.9               | 329.9          |                | 237 | 5.0           |                    | 253.8              |                   | N                   |
| 38 571 5/5 340.6 73.1 326.0 71.3 76 9.1 243.1 71.2 N 36 562 6/6 347.5 52.7 341.1 51.9 101 6.7 1951 55.4 N 36 562 6/6 347.5 52.7 341.1 51.9 101 6.7 1951 55.4 N 37 568 562 6/6 347.5 52.7 341.1 51.9 101 6.7 1951 55.4 N 38 5(EB14) 551 4/5 349.8 50.0 343.9 49.4 755 3.3 10.4 190.2 53.7 N 34 540 0/6 34 538 6/6 318.5 18.1 317.3 15.2 40 10.8 214.4 25.3 T 32 (EB10) 488 6/6 316.6 30.4 314.4 27.3 278 4.0 5.8 220.0 30.8 T 31 472 5/5 186.0 -62.8 176.2 -63.4 135 6.6 9.0 354.1 -69.7 R 30° 469 0/4 29 (EB7) 463 5/5 44.1 -61.0 49.2 -57.0 133 7.1 126.8 -19.6 T 28 (EB6C) 460 5/6 204.3 -57.3 197.0 -59.5 354 4.1 39.6 316.6 -63.3 R 25 443 6/7 20.3 3-61.7 192.5 -64.1 154 5.4 25.0 320.8 -69.5 R 24 424 6/6 238.5 -76.2 221.6 -81.2 137 5.9 23.4 210.7 -73.7 R 238 420 5/6 247.5 -65.4 242.6 -71.1 127 6.8 243.9 -59.1 R 23 418 5/5 1863 -83.5 138.2 -82.2 123 7.4 128.5 -73.3 R 22 1 400 5/6 202.1 -76.6 150.9 -49.1 205 5.4 4 128.5 -73.3 R 21 400 4/6 156.2 -48.0 150.2 -48.9 179 6.9 14.8 27.4 -47.7 T 20 401 6/6 202.1 -76.6 157.9 -78.2 229 4.4 130.9 -87.3 R 18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 16 378 5/5 215.9 -75.6 193.1 -78.7 66 9.5 219.9 -84.0 R 16 378 5/5 246.7 -19.1 245.8 -25.8 100 8.8 272.9 -22.4 T 16 379 6/6 80.8 77.6 77.8 83.6 97 6.8 11.5 79 19.1 -75.6 4.8 N 10 272 0/7 09 269 0/6 08 266 3/3 267.7 -4.7 267.8 -11.7 194 8.9 255.8 -63.3 T 00 229 7/7 281.6 -76.5 298.6 -82.9 97 6.2 16.1 188.8 -56.3 R 00 222 6/6 237.3 -66.5 226.1 -74.4 59 8.8 21.9 19.7 26.2 T 10 29 6/6 60.1 18.3 59.0 24.7 55 9.3 6.8 99.7 24.5 T 10 277 8/5 246.7 -19.1 245.8 -25.8 100 8.8 272.9 -22.4 T 06 245 6/6 60.1 18.3 59.0 24.7 55 9.3 6.8 99.7 24.5 T 06 245 6/6 60.1 18.3 59.0 24.7 55 9.3 6.8 99.7 24.5 T 07 265 5/5 246.7 -19.1 245.8 -25.8 100 8.8 272.9 -22.4 T 06 245 6/6 60.1 18.3 59.0 24.7 55 9.3 6.8 99.7 24.5 T 07 265 5/5 246.7 -19.1 245.8 -25.8 100 8.8 222.9 24.4 T 06 245 6/6 60.1 18.3 59.0 24.7 55 9.3 6.8 99.7 24.5 T 07 266 6/6 6/7 37.3  |           | 585        |                 |                |                    |                |                |     |               |                    |                    |                   | N                   |
| 37 566 6 6/6 309.1 75.3 298.4 71.4 226 4.5 25.5 268.7 59.8 N 36 562 6/6 347.5 52.7 341.1 51.9 101 6.7 195.1 55.4 N 35 [EB14) 551 4/5 349.8 50.0 343.9 49.4 755 3.3 10.4 190.2 53.7 N 34 540 0/6 33 538 6/6 318.5 18.1 317.3 15.2 40 10.8 214.4 25.3 T 32 [EB10) 488 6/6 316.6 30.4 314.4 27.3 278 4.0 5.8 220.0 30.8 T 31 472 5/5 186.0 62.8 176.2 63.4 135 6.6 9.0 354.1 69.7 R 30° 469 0/4 29 [EB7) 463 5/5 44.1 -61.0 49.2 -57.0 133 7.1 126.8 -19.6 T 28 [EB60] 460 5/6 204.3 -57.3 197.0 -59.5 354 4.1 39.6 316.6 -63.3 R 27 455 6/6 196.8 -59.4 188.5 -61.0 152 5.9 330.4 -66.4 R 25 443 6/7 203.3 -61.7 192.5 -64.1 154 5.4 25.0 320.8 -60.5 R 24 424 6/6 238.5 -76.2 221.6 -81.2 137 5.9 23.4 210.7 -73.7 R 23 418 5/5 186.3 -83.5 138.2 -82.2 123 7.4 128.5 -73.3 R 22 410 6/6 4/6 156.2 -48.0 150.2 -45.9 179 6.9 14.8 27.4 -47.7 T 20 401 6/6 202.1 7-66 175.9 -78.2 229 4.4 130.9 -87.3 R 19 [BB1] 398 6/6 177.2 -65.0 164.4 -64.7 95 6.9 14.8 27.4 -47.7 T 20 401 6/6 202.1 -76.6 175.9 -78.2 229 4.4 130.9 -87.3 R 18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 17 383 6/6 80.9 -75.6 189.9 -64.2 60 8.7 4 7.8 191.7 26.2 T 14 372 6/6 80.8 7.7 -60.5 R 16 378 5/5 215.9 -75.6 189.1 -78.7 66 9.5 8.3 48.1 -72.6 R 17 387 6/6 838.2 8.5 337.4 6.8 74 7.8 191.7 26.2 T 14 372 6/6 80.8 77.6 78.8 83.6 97 6.8 16.5 64.8 N 10 272 0/7 09 269 0/6 08 866 3/3 267.7 -4.7 267.8 -11.7 194 8.9 255.8 -63.3 T 07 265 5/5 246.7 -19.1 245.8 -25.8 100 8.8 272.9 -22.4 T 06 245 6/6 60.1 18.3 59.0 24.7 55.9 36.8 99.7 24.5 T 06 245 6/6 60.1 18.3 59.0 24.7 55.9 36.8 99.7 24.5 T 07 265 5/5 246.7 -19.1 245.8 -25.8 100 8.8 272.9 -22.4 T 06 247 6/6 229.9 -75.6 193.1 -78.7 56.9 18.8 4.9 9.7 24.5 T 09 269 0/6 08 266 3/3 267.7 -4.7 267.8 -11.7 194 8.9 255.8 -63.3 R 00 229 7/7 281.6 -76.5 298.6 -82.9 97 6.2 16.1 188.8 -56.3 R 01 227 8/8 254.0 -67.7 240.7 -77.4 59 9.8 6.9 18.4 59.7 24.5 T 06 245 6/6 200.9 -70.0 261.0 -77.0 187 4.4 48.7 199.1 -55.6 R 00 222 6/6 237.3 -68.5 226.1 -74.4 59 8.8 222.0 304.1 -47.7 T 00 299 6/6 207.1 -32.9 202.9 -36.5 1385 1.8 14.3 316.6 -42.7 T 1JD 299 6 |           | 583        |                 |                |                    |                |                |     |               | 15.5               | 197.0              |                   | N                   |
| 36   |           |            | 5/5             |                |                    |                |                |     |               | 25.5               | 243.1              |                   | N                   |
| 35 (EB14) 551 4/5 349.8 50.0 343.9 49.4 755 3.3 10.4 190.2 53.7 N  34 540 0/6  33 538 6/6 318.5 18.1 317.3 15.2 40 10.8 214.4 25.3 27  32 (EB10) 488 6/6 316.6 30.4 314.4 27.3 278 4.0 5.8 220.0 30.8 T  31 472 5/5 186.0 -62.8 176.2 -63.4 135 6.6 9.0 354.1 -69.7 R  30° 469 0/4  29 (EB7) 463 5/5 44.1 -61.0 49.2 -57.0 133 7.1 126.8 -19.6 T  28 (EB6C) 460 5/6 204.3 -57.3 197.0 -59.5 354 4.1 39.6 316.6 -63.3 R  27 455 6/6 196.8 -59.4 18.5 -61.0 152 5.9 330.4 -66.4 R  25 443 6/7 203.3 -61.7 192.5 -64.1 154 5.4 25.0 320.8 -69.5 R  24 424 6/6 238.5 -76.2 221.6 -81.2 137 5.9 23.4 210.7 -73.7 R  23B 420 5/6 247.5 -65.4 242.6 -71.1 127 6.8 243.9 -59.1 R  23 418 5/5 186.3 -83.5 138.2 -82.2 123 7.4 128.5 -73.3 R  21 406 4/6 156.2 -48.0 150.2 -45.9 179 6.9 14.8 27.7 -50.5 R  21 406 4/6 156.2 -48.0 150.2 -45.9 179 6.9 14.8 27.7 -50.5 R  18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R  18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R  18 388 5/6 202.1 -76.6 175.9 -78.2 229.4 4.7 69.7 18.4 69.6 R  18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R  18 388 5/6 200.9 -62.0 189.9 -64.2 60 8.7 325.8 -70.1 R  19 (EB1) 398 6/6 62.6 67.6 55.5 337.4 6.8 74 7.8 191.7 26.2 T  14 372 6/6 338.2 8.5 337.4 6.8 74 7.8 191.7 26.2 T  14 372 6/6 80.8 77.6 77.8 83.6 97 6.8 16.5 64.8 N  10 272 0/7  09 269 0/6  08 266 3/3 267.7 -4.7 267.8 -11.7 194 8.9 255.8 -63.3 T  06 245 6/6 60.1 18.3 59.0 24.7 55 9.3 6.8 99.7 24.5 T  06 245 6/6 60.1 18.3 59.0 24.7 55 9.3 6.8 99.7 24.5 T  07 265 5/5 246.7 -19.1 245.8 -25.8 100 8.8 272.9 -22.4 T  06 245 6/6 60.1 18.3 59.0 24.7 55 9.3 6.8 99.7 24.5 T  06 245 6/6 60.1 18.3 59.0 24.7 55 9.3 6.8 99.7 24.5 T  07 265 6/6 60.1 18.3 59.0 24.7 55 9.3 6.8 99.7 24.5 T  08 266 3/3 267.7 -4.7 267.8 -11.7 194 8.9 255.8 -63.3 T  09 269 0/6 229 7/7 281.6 -76.5 298.6 -82.9 97 6.2 16.1 188.8 -56.3 R  00 222 97 7/7 281.6 -76.5 298.6 -82.9 97 6.2 16.1 188.8 -56.3 R  01 227 8/8 254.0 -67.7 249.7 -74.5 99 5.6 22.8 304.1 -47.7 T  J.C 209 6/6 207.1 -32.9 202.9 -36.5 1385 1.8 14.3 316.6 -42.7 T  J.D 199 5/6  |           |            | 6/6             |                |                    |                |                |     |               | 25.5               | 208.7<br>105.1     |                   | N                   |
| 34 540 0/6 33 538 6/6 318.5 18.1 317.3 15.2 40 10.8 214.4 25.3 T 32 (EB10) 488 6/6 316.6 30.4 314.4 27.3 278 4.0 5.8 220.0 30.8 T 31 472 5/5 186.0 -62.8 176.2 -63.4 135 6.6 9.0 354.1 -69.7 R 30° 469 0/4 29 (EB7) 463 5/5 44.1 -61.0 49.2 -57.0 133 7.1 126.8 -19.6 T 28 (EB6C) 460 5/6 204.3 -57.3 197.0 -59.5 354 4.1 39.6 316.6 -63.3 R 27 455 6/6 196.8 -59.4 188.5 -61.0 152 5.9 30.4 66.4 R 25 443 6/7 20.33 -61.7 192.5 -64.1 154 5.4 25.0 320.8 -69.5 R 24 424 6/6 238.5 -76.2 221.6 -81.2 137 5.9 23.4 210.7 -73.7 R 23B 420 5/6 247.5 -65.4 242.6 -71.1 127 6.8 243.9 -59.1 8 22 410 5/5 157.8 -51.1 151.0 -49.1 205 5.4 27.7 -50.5 R 21 406 4/6 156.2 -48.0 150.2 -45.9 179 6.9 14.8 27.7 -50.5 R 29 401 6/6 202.1 -76.6 175.9 -78.2 229 4.4 128.5 -73.3 R 19 (EB1) 398 6/6 177.2 -65.0 164.4 -64.7 95 6.9 18.4 -60.6 R 18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 17 383 6/6 200.9 -62.0 189.9 -64.2 60 8.7 325.8 -70.1 R 18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 16 378 5/5 215.9 -75.6 193.1 -78.7 66 9.5 219.9 -84.0 R 18 379 6/6 338.2 8.5 337.4 6.8 74 7.8 191.7 26.2 T 14 372 6/6 49.7 70.6 37.0 75.2 206 4.7 95 6.9 18.4 -60.6 R 18 389 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 17 383 6/6 200.9 -62.0 189.9 -64.2 60 8.7 325.8 -70.1 R 18 380 5/6 6 19.6 80.8 77.6 77.8 83.6 97 6.8 16.5 64.8 N 10 272 0/7 09 269 0/6 08 266 3/3 267.7 -4.7 267.8 -11.7 194 8.9 255.8 -63.3 T 07 265 5/5 246.7 -19.1 245.8 25.5 123 6.1 15.7 199.1 -55.6 R 04 235 0/3 03 233 7/7 281.6 -76.5 298.6 -82.9 97 6.2 16.1 188.8 -56.3 R 00 222 97 7/7 262.0 -70.0 261.0 -77.0 187 4.4 48.7 218.5 -58.4 R 01 227 8/8 254.0 -67.5 298.6 -82.9 97 6.2 16.1 188.8 -56.3 R 00 222 6/6 237.3 -68.5 2261 -74.4 59 8.8 246.6 -69.1 R 00 222 6/6 237.3 -68.5 2261 -74.4 59 8.8 246.6 -69.1 R 00 222 6/6 237.3 -68.5 2261 -74.4 59 8.8 246.6 -69.1 R 00 222 6/6 237.3 -68.5 2261 -74.4 59 8.8 246.6 -69.1 R 00 222 6/6 237.3 -68.5 2261 -74.4 59 8.8 246.6 -69.1 R 00 222 6/6 237.3 -68.5 2261 -74.4 59 8.8 246.6 -69.1 R 00 222 6/6 237.3 -68.5 2261 -74.4 59 8.8 246.6 -69.1 R 00 2 |           | 551        | 4/5             |                |                    |                |                |     |               | 10.4               |                    |                   | N                   |
| 33 538 6/6 316.5 18.1 317.3 15.2 40 10.8 214.4 25.3 T 32 (EB10) 488 6/6 316.6 30.4 314.4 27.3 27.8 4.0 5.8 220.0 30.8 T 31 472 5/5 186.0 -62.8 176.2 -63.4 135 6.6 9.0 354.1 -69.7 R 29 (EB7) 463 5/5 44.1 -61.0 49.2 -57.0 133 7.1 126.8 -19.6 T 28 (EB6C) 460 5/6 204.3 -57.3 197.0 -59.5 354 4.1 39.6 316.6 -63.3 R 27 455 6/6 196.8 -59.4 188.5 -61.0 152 5.9 330.4 -66.4 R 25 443 6/7 203.3 -61.7 192.5 -64.1 154 5.4 25.0 320.8 -69.5 R 24 424 6/6 238.5 -76.2 221.6 -81.2 137 5.9 23.4 210.7 -73.7 R 23B 420 5/6 247.5 -65.4 242.6 -71.1 127 6.8 243.9 -59.1 R 23 418 5/5 186.3 -83.5 138.2 -82.2 123 7.4 128.5 -73.3 R 21 406 4/6 156.2 -48.0 150.2 -45.9 17.9 6.9 14.8 27.4 -47.7 T 20 401 6/6 202.1 -76.6 175.9 -78.2 229 4.4 130.9 -87.3 R 19 (EB1) 398 6/6 177.2 -65.0 164.4 -64.7 95 6.9 18.4 -69.6 R 18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 16 378 5/5 215.9 -75.6 193.1 -78.7 66 9.5 219.9 -84.0 R 15 379 6/6 338.2 8.5 37.4 6.8 74 7.8 191.7 262. T 14 372 6/6 49.7 70.6 37.0 75.2 206 4.7 69.7 73.6 N 11 307 6/6 80.8 77.6 77.8 83.6 97 6.8 191.7 262. T 14 372 6/6 49.7 70.6 37.0 75.2 206 4.7 69.7 73.6 N 11 307 6/6 80.8 77.6 77.8 83.6 97 6.8 191.7 191.7 262. T 14 372 6/6 49.7 70.6 37.0 75.2 206 4.7 69.7 73.6 N 10 272 0/7 09 269 0/6 08 266 3/3 267.7 -4.7 267.8 -11.7 194 8.9 255.8 -6.3 T 07 265 5/5 246.7 -19.1 245.8 -25.8 100 8.8 272.9 -22.4 T 05 240 6/7 276.5 -73.8 285.5 -80.5 123 6.1 15.7 199.1 -55.6 R 04 2255 0/3 03 223 7/7 281.6 -76.5 298.6 82.9 97 6.2 16.1 188.8 -56.3 R 02 229 7/7 282.0 -70.0 261.0 -77.0 187 4.4 48.7 218.5 -58.4 R 01 227 8/8 254.0 -67.7 249.7 -74.5 99 5.6 6 22.8 304.1 -47.7 T 05 240 6/6 220 -70.0 261.0 -77.0 187 4.4 48.7 218.5 -58.4 R 01 227 8/8 254.0 -67.7 249.7 -74.5 99 5.6 6 22.8 304.1 -47.7 T 05 240 6/6 227.1 -32.9 202.9 -36.5 1385 1.8 14.3 316.6 -42.7 T JD 199 5/6 211.3 -26.8 208.2 -30.9 167 5.9 22.0 311.3 -37.9 T   |           | 540        | 0/6             | 013.0          | 00.0               | 010.5          | 10.1           | 100 | 0.0           | 10.1               | 130.2              | 00.1              | 11                  |
| 32 (BB10)  |           |            | 6/6             | 318.5          | 18.1               | 317.3          | 15.2           | 40  | 10.8          |                    | 214.4              | 25.3              | ${ m T}$            |
| 30° 469 0/4 29 (EB7) 463 5/5 44.1 -61.0 49.2 -57.0 133 7.1 126.8 -19.6 T 28 (EB6C) 460 5/6 204.3 -57.3 197.0 -59.5 354 4.1 39.6 316.6 -63.3 R 27 455 6/6 196.8 -59.4 188.5 -61.0 152 5.9 330.4 -66.4 R 25 443 6/7 203.3 -61.7 192.5 -64.1 154 5.4 25.0 320.8 -69.5 R 24 424 6/6 238.5 -76.2 221.6 -81.2 137 5.9 23.4 210.7 -73.7 R 23B 420 5/6 247.5 -65.4 242.6 -71.1 127 6.8 243.9 -59.1 R 23 418 5/5 186.3 -83.5 138.2 -82.2 123 7.4 128.5 -73.3 R 22 410 5/5 157.8 -51.1 151.0 -49.1 205 5.4 27.7 -50.5 R 21 406 4/6 156.2 48.0 150.2 -45.9 179 6.9 14.8 27.4 -47.7 T 20 401 6/6 202.1 -76.6 175.9 -78.2 229 4.4 130.9 -87.3 R 19 (EB1) 398 6/6 177.2 -65.0 164.4 -64.7 95 6.9 18.4 -69.6 R 18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 16 378 5/5 215.9 -65.0 189.9 -64.2 60 8.7 325.8 -70.1 R 16 378 5/5 215.9 -75.6 193.1 -78.7 66 9.5 219.9 -84.0 R 15 373 6/6 338.2 8.5 337.4 6.8 74 7.8 191.7 26.2 T 14 372 6/6 49.7 70.6 37.0 75.2 206 4.7 69.7 73.6 N 11 307 6/6 80.8 77.6 77.8 83.6 97 6.8 16.5 64.8 N 10 272 0/7 09 269 0/6 08 266 3/3 267.7 -4.7 267.8 -11.7 194 8.9 255.8 -6.3 T 06 245 6/6 6/6 60.1 18.3 59.0 24.7 55 9.3 6.8 99.7 24.5 T 06 245 6/6 6/6 266 67.6 55.5 73.1 42 10.4 7.3 64.2 64.0 N 11 307 6/6 22.6 -77.8 83.6 97 6.8 16.5 64.8 N 10 272 0/7 09 269 0/6 08 266 5/5 246.7 -19.1 245.8 -25.8 100 8.8 272.9 -22.4 T 06 245 6/6 6/6 60.1 18.3 59.0 24.7 55 9.3 6.8 99.7 24.5 T 06 245 6/6 6/7 276.5 -73.8 285.5 -80.5 123 6.1 15.7 199.1 -55.6 R 04 235 0/3 03 233 7/7 281.6 -76.5 298.6 -82.9 97 6.2 16.1 188.8 -56.3 R 00 222 7 7/7 262.0 -70.0 261.0 -77.0 187 4.4 48.7 218.5 -58.4 R 01 227 8/8 254.0 -67.7 249.7 -74.5 99 5.6 22.8 304.1 -47.7 T JD 199 5/6 211.3 -26.8 208.2 -30.9 167 5.9 22.0 311.3 -37.9 T   | 32 (EB10) | 488        | 6/6             | 316.6          |                    | 314.4          |                | 278 | 4.0           |                    | 220.0              | 30.8              | ${ m T}$            |
| 29 (EB7) 463 5/5 44.1 -61.0 49.2 -57.0 133 7.1 126.8 -19.6 T 28 (EB6C) 460 5/6 204.3 -57.3 197.0 -59.5 354 4.1 39.6 316.6 -63.3 R 27 455 6/6 196.8 -59.4 188.5 -61.0 152 5.9 330.4 -66.4 R 25 443 6/7 203.3 -61.7 192.5 -64.1 154 5.4 25.0 320.8 -69.5 R 24 424 6/6 238.5 -76.2 221.6 -81.2 137 5.9 23.4 210.7 -73.7 R 23B 420 5/6 247.5 -65.4 242.6 -71.1 127 6.8 243.9 -59.1 R 23 418 5/5 186.3 -83.5 138.2 -82.2 123 7.4 128.5 -73.3 R 22 410 5/5 157.8 -51.1 151.0 -49.1 205 5.4 27.7 -50.5 R 21 406 4/6 156.2 -48.0 150.2 -45.9 179 6.9 14.8 27.4 -47.7 T 20 401 6/6 202.1 -76.6 175.9 -78.2 229 4.4 130.9 -87.3 R 19 (EB1) 398 6/6 177.2 -65.0 164.4 -64.7 95 6.9 18.4 -69.6 R 18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 17 383 6/6 200.9 -62.0 189.9 -64.2 60 8.7 325.8 -70.1 R 16 378 5/5 215.9 -75.6 193.1 -78.7 66 9.5 219.9 -84.0 R 15 373 6/6 338.2 8.5 337.4 6.8 74 7.8 191.7 26.2 T 14 372 6/6 49.7 70.6 37.0 75.2 206 4.7 69.7 73.6 N 12 310 6/6 62.6 67.6 55.5 73.1 42 10.4 7.3 64.2 64.0 N 11 307 6/6 80.8 77.6 77.8 83.6 97 6.8 10.5 64.8 N 10 272 0/7 09 269 0/6 08 266 3/3 267.7 -4.7 267.8 -11.7 194 8.9 255.8 -6.3 T 07 265 5/5 246.7 -19.1 245.8 -25.8 100 8.8 272.9 -22.4 T 06 245 6/6 60.1 18.3 59.0 24.7 55 9.3 6.8 99.7 24.5 T 06 246 6/7 276.5 73.8 285.5 -80.5 123 6.1 15.7 199.1 -55.6 R 04 235 0/3 03 233 7/7 281.6 -76.5 298.6 -82.9 97 6.2 16.1 18.8 -56.3 R 04 235 0/3 03 239 7/7 281.6 -76.5 298.6 -82.9 97 6.2 16.1 18.8 -56.3 R 04 235 0/3 03 239 7/7 281.6 -76.5 298.6 -82.9 97 6.2 16.1 15.7 199.1 -55.6 R 04 235 0/3 03 239 7/7 281.6 -76.5 298.6 -82.9 97 6.2 16.1 15.7 199.1 -55.8 R 04 235 0/3 03 229 7/7 262.0 -70.0 261.0 -77.0 187 4.4 48.7 218.5 -58.4 R 01 227 6/6 237.3 -68.5 226.1 -74.4 59 8.8 246.6 -69.1 R 04 235 0/3 03 229 7/7 262.0 -70.0 261.0 -77.0 187 4.4 48.7 218.5 -58.4 R 01 227 6/6 237.3 -68.5 226.1 -74.4 59 8.8 246.6 -69.1 R 04 235 0/3 03 229 7/7 262.0 -70.0 261.0 -77.0 187 4.4 48.7 218.5 -58.8 R 01 227 6/6 237.3 -68.5 226.1 -74.4 59 8.8 246.6 -69.1 R 04 235 0/3 34.1 -72.6 8.2 20.9 36.5 1385 1.8 14.3 316.6 -42.7 T 1D 1Dykes: |           | 472        | 5/5             | 186.0          | -62.8              | 176.2          | -63.4          | 135 | 6.6           | 9.0                | 354.1              | -69.7             | $\mathbf{R}$        |
| 28 (EB6C) 460 5/6 204.3 -57.3 197.0 -59.5 354 4.1 39.6 316.6 -63.3 R 27 455 6/6 196.8 -59.4 188.5 -61.0 152 5.9 330.4 -66.4 R 25 443 6/7 203.3 -61.7 192.5 -64.1 154 5.4 25.0 320.8 -69.5 R 24 424 424 6/6 238.5 -76.2 221.6 -81.2 137 5.9 23.4 210.7 -73.7 R 238 420 5/6 247.5 -65.4 242.6 -71.1 127 6.8 243.9 -59.1 R 23 418 5/5 186.3 -83.5 138.2 -82.2 123 7.4 128.5 -73.3 R 22 410 5/5 157.8 -51.1 151.0 -49.1 205 5.4 27.7 -50.5 R 21 406 4/6 156.2 -48.0 150.2 -45.9 17.9 6.9 14.8 27.4 -47.7 T 20 401 6/6 202.1 -76.6 175.9 -78.2 229 4.4 130.9 -87.3 R 19 (EB1) 398 6/6 177.2 -65.0 164.4 -64.7 95 6.9 18.4 -69.6 R 18 388 5/6 191.8 -64.4 179.2 -65.6 65 9.6 8.5 348.1 -72.6 R 16 378 5/5 215.9 -75.6 193.1 -78.7 66 9.5 219.9 -84.0 R 15 373 6/6 338.2 8.5 337.4 6.8 74 7.8 191.7 26.2 T 14 372 6/6 49.7 70.6 37.0 75.2 206 4.7 69.7 73.6 N 12 310 6/6 20.6 62.6 67.6 55.5 73.1 42 10.4 7.3 64.2 64.0 N 11 307 6/6 80.8 77.6 77.8 83.6 97 6.8 16.5 64.8 N 10 272 0/7 09 269 0/6 00.6 00.6 00.6 00.6 00.6 00.6 00.6  |           | 469        | 0/4             |                |                    |                |                |     |               |                    |                    |                   |                     |
| 27   |           |            | $\frac{5}{5}$   |                |                    |                |                |     |               | 00.0               |                    |                   | T                   |
| 25   | 28 (EB6C) |            | 5/6             |                | -57.3              |                |                |     |               | 39.6               | 316.6              |                   |                     |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$  |           |            | 6/7             |                |                    |                |                |     |               | 25.0               | 330.4<br>330.8     |                   | R<br>D              |
| 23B  |           | 443        |                 |                |                    |                |                |     |               |                    | 210.7              |                   | R                   |
| 23   |           |            | $\frac{5}{6}$   |                |                    |                |                |     |               | 20.1               |                    |                   | R                   |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 23        | 418        | 5/5             |                |                    |                | -82.2          |     |               |                    | 128.5              |                   | R                   |
| 20   | 22        | 410        | 5/5             |                |                    |                | -49.1          |     | 5.4           |                    | 27.7               |                   | $^{\mathrm{R}}$     |
| 19 (EB1)   |           |            | 4/6             |                |                    |                |                |     |               | 14.8               | 27.4               |                   | T                   |
| 18       388       5/6       191.8       -64.4       179.2       -65.6       65       9.6       8.5       348.1       -72.6       R         17       383       6/6       200.9       -62.0       189.9       -64.2       60       8.7       325.8       -70.1       R         16       378       5/5       215.9       -75.6       193.1       -78.7       66       9.5       219.9       -84.0       R         15       373       6/6       338.2       8.5       337.4       6.8       74       7.8       191.7       26.2       T         14       372       6/6       49.7       70.6       37.0       75.2       206       4.7       69.7       73.6       N         12       310       6/6       62.6       67.6       55.5       73.1       42       10.4       7.3       64.2       64.0       N         10       272       0/7       0/7       0/7       0       0       8       16.5       64.8       N         10       272       0/7       0       0       0       0       0       0       0       0       0       0       0 <t< td=""><td></td><td>401</td><td>6/6</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>R</td></t<>   |           | 401        | 6/6             |                |                    |                |                |     |               |                    |                    |                   | R                   |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |           | 398        |                 |                |                    |                |                |     |               | 0 -                | 18.4               |                   | R                   |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |           |            | 5/6             |                |                    |                |                |     |               | 8.5                | 348.1              |                   | K<br>D              |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |           |            |                 |                |                    |                |                |     |               |                    |                    |                   |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |           |            |                 |                |                    |                |                |     |               |                    |                    |                   | _                   |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |           |            | $\frac{6}{6}$   |                |                    |                |                |     |               |                    |                    |                   |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |           | 310        |                 |                |                    |                |                |     |               | 7.3                | 64.2               |                   |                     |
| 09   | 11        | 307        | 6/6             | 80.8           | 77.6               | 77.8           | 83.6           | 97  | 6.8           |                    |                    |                   | N                   |
| 08   | 10        | 272        | 0/7             |                |                    |                |                |     |               |                    |                    |                   |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 09        |            | 0/6             |                |                    |                |                |     |               |                    |                    |                   |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |           |            | 3/3             |                |                    |                |                |     |               |                    |                    |                   | T                   |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |           | 205        | 5/5<br>6/6      |                |                    |                |                |     |               | 6 9                |                    |                   |                     |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |           | 240<br>210 | 6/7             |                |                    |                |                |     |               |                    |                    |                   |                     |
| 03   |           | 235        | $\frac{0}{3}$   | 210.0          | -10.0              | 200.0          | -00.0          | 120 | 0.1           | 10.1               | 100.1              | -55.0             | 11                  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |           | 233        | $\frac{5}{7}$   | 281.6          | -76.5              | 298.6          | -82.9          | 97  | 6.2           | 16.1               | 188.8              | -56.3             | $\mathbf{R}$        |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |           | 229        | 7/7             |                |                    |                |                |     |               |                    | 218.5              |                   | R                   |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |           | 227        | 8/8             |                |                    |                |                |     |               |                    | 231.1              |                   | $\mathbf{R}$        |
| JB 214 5/5 215.9 -41.8 210.7 -46.2 65 9.6 22.8 304.1 -47.7 T<br>JC 209 6/6 207.1 -32.9 202.9 -36.5 1385 1.8 14.3 316.6 -42.7 T<br>JD 199 5/6 211.3 -26.8 208.2 -30.9 167 5.9 22.0 311.3 -37.9 T<br>Dykes:  |           | 222        | 6/6             |                |                    |                |                |     |               |                    | 246.6              |                   |                     |
| Dykes:   | JA        | 217        | 6/6             |                |                    |                |                |     |               |                    |                    |                   | $\frac{R}{}$        |
| Dykes:   |           |            |                 |                |                    |                |                |     |               |                    |                    |                   | Τ                   |
| Dykes:   |           |            |                 |                |                    |                |                |     |               |                    |                    |                   | T                   |
|  | эD        | 199        | 5/0             | ∠11.3          | -20.0              | 400.4          | -50.9          | 107 | 5.9           | 22.0               | 511.5              | -31.9             | 1                   |
|  | Dykes:    |            |                 |                |                    |                |                |     |               |                    |                    |                   |                     |
| 15 $312$ $5/8$ 19.0 44.8 15.3 47.1 52 10.7 147.0 52.2 N  | 13        | 312        | 5/8             | 19.0           | 44.8               | 13.3           | 47.1           | 52  | 10.7          |                    | 147.0              | 52.2              | N                   |

Table 1: Directional results

| Site | Altitude       | n/N | $\mathbf{D}_{a}$ | $\mathbf{I}_{a}$ | $\mathbf{D}_s$ | $\mathbf{I}_s$ | k   | $\alpha_{95}$ | F             | VGP                          | VGP                         | Pol. |
|------|----------------|-----|------------------|------------------|----------------|----------------|-----|---------------|---------------|------------------------------|-----------------------------|------|
|      | $[\mathbf{m}]$ | ,   | [°]              | [°]              | [°]            | [°]            |     | [°]           | $[\mu {f T}]$ | $\mathbf{long.}\ [^{\circ}]$ | $\mathbf{lat.}\ [^{\circ}]$ |      |
| DY   | 205            | 5/5 |                  |                  | 1.3            | 73.1           | 148 | 6.3           |               | 160.3                        | 83.5                        | N    |

Directional results for all sampled sites. Altitudes (GPS-altitudes in normal fonts, italics for interpolated altitudes), n/N is the number of samples used for the calculation of the mean directions versus the number of samples treated,  $D_g$  and  $I_g$  denote declination and inclination in geographic coordinates,  $D_s$  and  $I_s$  the declination and inclination in stratigraphic coordinates, k and  $\alpha_{95}$  indicate the concentration parameter and the confidence cone, K yields the weighted mean intensity of all suitable specimens of a site (see Table 2), VGP longitude and latitude give the coordinates of the virtual geomagnetic pole. The polarity of each flow are given with K for normal polarity, K for reversed and K for transitional (if the VGP latitude is below K for (McElhinny and McFadden, 1997)). A K following the sample name denotes transitional lava flows, which could only be evaluated with great circle analysis. Based on flow descriptions, similar altitude, and their position relative to pronounced red beds, some lava flows could be unambiguously correlated to profile K of Watkins and Walker (1977). In this case the site name used by Watkins and Walker (1977) is given in parenthesis after our site name. Above and below these flows a direct flow-to-flow correlation between Watkins and our work is not possible, because of slightly different sampling routes. Comparison, however, is possible based on altitude measurements.

572

Table 2: Paleointensity results of Neskaupstadur section

| Site            | Alt. | n/N             | Sample  | $T_{min}$                                 | $T_{max}$         | N                                      | f                   | g              | q                   | w                   | $F_{i}$             | $\sigma F_i$      | F    | $\sigma F$ |
|-----------------|------|-----------------|---|---|-------------------|--|---------------------|----------------|---------------------|---------------------|---------------------|-------------------|------|------------|
| 64              | 761  | 0/2             | 01 1¥   | 400                                       | F00               | 7                                      | 0.70                | 0.70           | 04.0                |                     | 7.0                 | 0.0               | 6.0  | 0.0        |
| 61              | 731  | 3/3             | 61-1*<br>61-4*  | $\frac{400}{400}$                         | $\frac{580}{580}$ | 7<br>7                                 | $0.79 \\ 0.79$      | $0.72 \\ 0.71$ | $24.8 \\ 21.6$      | $\frac{11.1}{9.6}$  | $\frac{7.2}{6.4}$   | $0.2 \\ 0.2$      | 6.8  | 0.3        |
|                 |      |                 | 61-5  | 430                                       | 610               | $\frac{'}{7}$                          | 0.79                | $0.71 \\ 0.75$ | $\frac{21.0}{11.0}$ | $\frac{9.0}{4.9}$   | $6.4 \\ 6.9$        | $0.2 \\ 0.4$      |      |            |
| 55              | 681  | 5/5             | 55-1  | $\frac{430}{280}$                         | 580               | 10                                     | 0.89                | $0.75 \\ 0.77$ | $\frac{11.0}{20.2}$ | 7.1                 | 29.8                | 1.0               | 41.4 | 4.1        |
| 00              | 001  | 0/0             | 55-2  | 100                                       | 520               | 15                                     | 0.48                | 0.84           | 6.0                 | $1.7^{-1}$          | $\frac{23.0}{47.2}$ | 3.1               | 11.1 | 1.1        |
|                 |      |                 | 55-3  | 310                                       | 520               | 7                                      | 0.37                | 0.80           | 4.6                 | 2.0                 | 37.5                | 2.4               |      |            |
|                 |      |                 | 55-4  | 100                                       | 490               | 13                                     | 0.44                | 0.88           | 39.1                | 11.8                | 45.4                | 0.5               |      |            |
|                 |      |                 | 55-5  | 200                                       | 490               | 8                                      | 0.46                | 0.82           | 10.6                | 4.3                 | 47.1                | 1.7               |      |            |
| 52              | 660  | 2/4             | 52-2*   | 200                                       | 460               | 7                                      | 0.33                | 0.80           | 2.6                 | 1.2                 | 29.7                | 3.0               | 37.8 | 6.3        |
| F-1             | 650  | 0./0            | 52-4  | 490                                       | 610               | 5                                      | 0.83                | 0.65           | 27.6                | 16.0                | 38.6                | 0.8               | 05 1 | 1.0        |
| 51              | 652  | 3/3             | 51-2<br>51-3*   | 370                                       | 610               | 9                                      | 0.90                | 0.76           | 18.3                | 6.9                 | 21.4                | 0.8               | 25.1 | 1.9        |
|                 |      |                 | 51-6*   | $\frac{400}{370}$                         | $\frac{610}{550}$ | $\frac{8}{7}$                          | $0.86 \\ 0.82$      | $0.82 \\ 0.78$ | $\frac{20.2}{14.8}$ | $8.3 \\ 6.6$        | $27.6 \\ 26.2$      | $\frac{1.0}{1.1}$ |      |            |
| 49              | 619  | 0/2             | 31-0  | 310                                       | 550               | '                                      | 0.62                | 0.76           | 14.0                | 0.0                 | 20.2                | 1.1               |      |            |
| 46              | 606  | $\frac{3}{3}$   | 46-3*   | 490                                       | 610               | 5                                      | 0.66                | 0.58           | 13.3                | 7.7                 | 19.4                | 0.6               | 23.3 | 1.5        |
|                 |      | -/-             | 46-5  | 390                                       | 580               | 7                                      | 0.88                | 0.77           | 24.8                | 11.1                | 22.5                | 0.6               |      |            |
|                 |      |                 | 46-4  | 20  | 580               | 13                                     | 0.96                | 0.82           | 37.7                | 11.4                | 25.2                | 0.5               |      |            |
| 43              | 592  | 3/3             | 43-2*   | 200                                       | 610               | 12                                     | 0.96                | 0.81           | 25.9                | 8.2                 | 14.8                | 0.4               | 14.3 | 0.8        |
|                 |      |                 | 43-3*   | 490                                       | 610               | 5                                      | 0.58                | 0.56           | 20.4                | 11.8                | 13.2                | 0.2               |      |            |
|                 |      | - 1-            | 43-6  | 20  | 490               | 10                                     | 0.32                | 0.76           | 2.6                 | 0.9                 | 17.5                | 1.6               |      |            |
| 42              | 590  | 3/3             | 42-3  | 20  | 520               | 16                                     | 0.67                | 0.90           | 32.0                | 8.5                 | 31.7                | 0.6               | 32.5 | 2.6        |
|                 |      |                 | 42-4*   | 190                                       | 520               | 11                                     | 0.77                | 0.88           | 5.1                 | 1.7                 | 42.8                | 5.7               |      |            |
| 41              | 586  | 0/3             | 42-6*   | 220                                       | 430               | 8                                      | 0.42                | 0.84           | 10.4                | 4.3                 | 29.7                | 1.0               |      |            |
| $\frac{41}{40}$ | 585  | $\frac{0}{3}$   | 40-3  | 20  | 490               | 10                                     | 0.41                | 0.77           | 2.3                 | 0.8                 | 21.9                | 3.0               | 26.0 | 7.0        |
| 40              | 909  | 2/2             | 40-6  | 100                                       | 460               | 8                                      | $0.41 \\ 0.30$      | 0.83           | $\frac{2.3}{2.4}$   | 1.0                 | 29.9                | $\frac{3.0}{3.1}$ | 20.0 | 7.0        |
| 39              | 583  | 2/2             | 39-4  | 100                                       | 490               | 9                                      | 0.33                | 0.81           | 3.0                 | 1.1                 | 14.8                | 1.3               | 15.5 | 2.1        |
|                 | 000  | -/-             | 39-6*   | 100                                       | 490               | 9                                      | 0.32                | 0.83           | 3.1                 | 1.2                 | 16.2                | 1.4               | 10.0 |            |
| 38              | 571  | 0/3             |   |   |                   |  |                     |                |                     |                     |                     |                   |      |            |
| 37              | 566  | 2/3             | 37 - 1  | 20  | 350               | 6                                      | 0.38                | $0.77^{\circ}$ | 3.0                 | 1.5                 | 26.4                | 2.6               | 25.5 | 2.8        |
|                 |      |                 | 37-6*   | 20  | 460               | 9                                      | 0.75                | 0.86           | 9.2                 | 3.5                 | 25.2                | 1.8               |      |            |
| 36              | 562  | 0/3             |   |   |                   |  |                     |                |                     |                     |                     |                   |      |            |
| 35              | 551  | 3/3             | 35-1  | 350                                       | 610               | 9                                      | 0.98                | 0.80           | 12.8                | 4.8                 | 8.4                 | 0.5               | 10.4 | 1.1        |
|                 |      |                 | 35-3*   | 200                                       | 610               | 12                                     | 0.97                | 0.80           | 38.5                | 12.2                | $\frac{11.4}{7.1}$  | 0.2               |      |            |
| 20              | 400  | 4/4             | 35-4*   | 250                                       | 520               | 8                                      | 0.56                | 0.76           | $\frac{3.4}{6.7}$   | $\frac{1.4}{2.4}$   | 7.1                 | 0.9               | F 0  | 0.0        |
| 32              | 488  | 4/4             | $\frac{32-1}{32-3}$                                       | $\frac{300}{220}$                         | $\frac{610}{580}$ | $\frac{10}{12}$                        | $\frac{1.00}{0.85}$ | $0.82 \\ 0.77$ | $\frac{6.7}{11.4}$  | $\frac{2.4}{3.6}$   | $\frac{4.9}{6.6}$   | $0.6 \\ 0.4$      | 5.8  | 0.8        |
|                 |      |                 | 32-4*   | $\frac{220}{220}$                         | 580               | $\frac{12}{12}$                        | 0.95                | 0.81           | $\frac{11.4}{3.7}$  | 1.2                 | 8.3                 | 1.7               |      |            |
|                 |      |                 | 32-6  | 370                                       | 610               | 9                                      | 0.90                | 0.84           | 8.0                 | 3.0                 | 4.3                 | 0.4               |      |            |
| 31              | 472  | 3/4             | 31-2*   | 370                                       | 580               | 7                                      | 0.77                | 0.76           | 8.9                 | 4.0                 | 12.9                | 0.9               | 9.0  | 1.9        |
|                 |      | ,               | 31-4  | 370                                       | 580               | 7                                      | 0.75                | 0.71           | 14.4                | 6.4                 | 8.3                 | 0.3               |      |            |
|                 |      |                 | 31-5  | 370                                       | 520               | 5                                      | 0.41                | 0.61           | 7.0                 | 4.0                 | 5.7                 | 0.2               |      |            |
| 28              | 460  | 5/6             | 28-1  | 20  | 610               | 14                                     | 0.96                | 0.84           | 31.5                | 9.1                 | 34.7                | 0.9               | 39.6 | 3.3        |
|                 |      |                 | 28-2  | 200                                       | 430               | 6                                      | 0.31                | 0.77           | 6.1                 | 3.0                 | 42.6                | 1.7               |      |            |
|                 |      |                 | 28-3*<br>28-5   | $\begin{array}{c} 200 \\ 300 \end{array}$ | 610<br>610        | $\frac{12}{10}$                        | $0.95 \\ 0.94$      | $0.76 \\ 0.81$ | $81.1 \\ 25.0$      | $\frac{25.6}{8.8}$  | $\frac{44.5}{30.4}$ | $0.4 \\ 0.9$      |      |            |
|                 |      |                 | 28-6*   | $\frac{300}{350}$                         | 610               | 9                                      | 0.94 $0.99$         | $0.81 \\ 0.78$ | $\frac{25.0}{7.8}$  | $\frac{0.0}{2.9}$   | $36.4 \\ 36.1$      | 3.6               |      |            |
| 27              | 455  | 0/3             | 20-0  | 300                                       | 010               | 9                                      | 0.55                | 0.10           | 1.0                 | 2.5                 | 30.1                | 5.0               |      |            |
| $\frac{2}{25}$  | 443  | $\frac{3}{4}/4$ | 25-3  | 350                                       | 610               | 9                                      | 0.93                | 0.81           | 20.9                | 7.9                 | 25.4                | 0.9               | 25.0 | 0.2        |
|                 |      | -/ -            | 25-2  | 350                                       | 610               | 9                                      | 0.92                | 0.76           | 9.2                 | 3.5                 | 25.1                | 1.9               |      |            |
|                 |      |                 | 25-7*   | 430                                       | 610               | 7                                      | 0.78                | 0.70           | 10.9                | 4.9                 | 24.8                | 1.3               |      |            |
|                 |      |                 | 25-5*   | 200                                       | 610               | 12                                     | 0.94                | 0.82           | 18.5                | 5.8                 | 24.5                | 1.0               |      |            |
| 24              | 424  | 3/4             | 24-1*   | 350                                       | 610               | 9                                      | 0.92                | 0.75           | 17.7                | 6.7                 | 24.9                | 1.0               | 23.4 | 0.8        |
|                 |      |                 | 24-4  | 20  | 350               | 6                                      | 0.62                | 0.76           | 3.6                 | 1.8                 | 22.9                | 3.0               |      |            |
| വ               | 410  | 0./2            | 24-6*   | 250                                       | 610               | 11                                     | 0.93                | 0.76           | 25.5                | 8.5                 | 22.4                | 0.6               |      |            |
| 23              | 418  | 0/3             | 01.1  | 400                                       | 610               | -                                      | 0.74                | 0.67           | 99.6                | 19.6                | 17.0                | 0.4               | 140  | 0.4        |
| 21              | 406  | 2/3             | $\begin{array}{c} 21\text{-}1 \\ 21\text{-}2 \end{array}$ | $\frac{490}{390}$                         | $\frac{610}{610}$ | 5<br>8                                 | $0.74 \\ 0.89$      | $0.67 \\ 0.72$ | $\frac{23.6}{31.7}$ | $\frac{13.6}{13.0}$ | $17.2 \\ 13.1$      | $0.4 \\ 0.3$      | 14.8 | 2.4        |
| 20              | 401  | 0/2             | 21-2  | 330                                       | 010               | O                                      | 0.03                | 0.12           | 31.1                | 15.0                | 10.1                | 0.5               |      |            |
| 18              | 388  | $\frac{3}{4}$   | 18-1  | 310                                       | 520               | 7                                      | 0.36                | 0.76           | 5.8                 | 2.6                 | 10.7                | 0.5               | 8.5  | 2.0        |
| 10              | 500  | 0/1             | 18-3  | 370                                       | 580               | 8                                      | 0.86                | 0.78           | 9.4                 | $\frac{2.0}{3.9}$   | 5.7                 | 0.4               | 0.0  | 2.0        |
|                 |      |                 | 18-5*   | 130                                       | 280               | 6                                      | 0.33                | 0.75           | 4.0                 | 2.0                 | 12.1                | 0.7               |      |            |
| 12              | 310  | 4/4             | 12-2  | 20  | 580               | 17                                     | 0.90                | 0.78           | 14.6                | 3.8                 | 7.7                 | 0.4               | 7.3  | 0.3        |
|                 |      |                 | 12-3  | 220                                       | 550               | 11                                     | 0.84                | 0.76           | 8.1                 | 2.7                 | 6.8                 | 0.5               |      |            |
|                 |      | 7               | 12-4  | 340                                       | 520               | 6                                      | 0.48                | 0.65           | 4.3                 | 2.1                 | 8.1                 | 0.6               |      |            |
| 67              | 005  | 0/1             | 12-6  | 220                                       | 550               | 11                                     | 0.84                | 0.74           | 18.7                | 6.2                 | 7.1                 | 0.2               |      |            |
| 07<br>06        | 265  | 0/1             | 06.0  | 400                                       | 610               | -                                      | 0.00                | 0.00           | 20.0                | 170                 | 0.0                 | 0.0               | 60   | 0.7        |
| 06              | 245  | 3/4             | 06-2<br>06-3*   | 490                                       | $\frac{610}{610}$ | $\begin{array}{c} 5 \\ 10 \end{array}$ | $0.82 \\ 0.92$      | 0.69           | $\frac{29.8}{28.2}$ | 17.2                | 8.0<br>6.7          | 0.2               | 6.8  | 0.7        |
|                 |      |                 | 06-4*   | $\frac{300}{460}$                         | 610               | 6                                      | $0.92 \\ 0.85$      | $0.61 \\ 0.65$ | $\frac{28.3}{21.7}$ | $10.0 \\ 10.9$      | $\frac{6.7}{5.4}$   | $0.1 \\ 0.1$      |      |            |
|                 |      |                 | 00-4  |   |                   |  |                     |                |                     |                     |                     |                   |      | 4.4        |
| 05              | 240  | 2/9             | 05-4  | 20  | 49∩               | 10                                     | 0.35                | (1.74          | フラ                  | na                  | IX 6                | I G               | 15.7 | 4 4        |
| 05              | 240  | 2/2             | $\begin{array}{c} 05\text{-}4 \\ 05\text{-}2 \end{array}$ | $\frac{20}{200}$                          | $\frac{490}{520}$ | 10<br>9                                | $0.35 \\ 0.55$      | $0.74 \\ 0.74$ | $\frac{2.5}{3.1}$   | $\frac{0.9}{1.2}$   | $18.6 \\ 13.5$      | $\frac{1.9}{1.8}$ | 15.7 | 4.4        |

Table 2: Paleointensity results of Neskaupstadur section

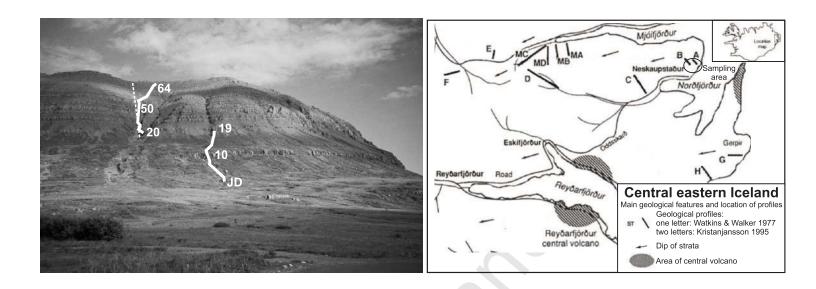
| Site       | Alt. | n/N      | Sample                | $T_{min}$ | $T_{max}$ | N  | f    | g    | q    | w    | $F_i$ | $\sigma F_i$ | F    | $\sigma F$ |
|------------|------|----------|-----------------------|-----------|-----------|----|------|------|------|------|-------|--------------|------|------------|
| 03         | 233  | 2/4      | 03-1                  | 20        | 550       | 12 | 0.58 | 0.86 | 10.9 | 3.4  | 13.6  | 0.6          | 16.1 | 2.7        |
|            |      | •        | 03-5*                 | 430       | 610       | 7  | 0.87 | 0.69 | 16.4 | 7.3  | 17.8  | 0.7          |      |            |
| 02         | 229  | 3/4      | 02-4*                 | 100       | 580       | 16 | 0.94 | 0.78 | 25.3 | 6.8  | 53.2  | 1.5          | 48.7 | 2.8        |
|            |      | ,        | 02-5*                 | 310       | 550       | 8  | 0.91 | 0.73 | 12.6 | 5.1  | 46.9  | 2.5          |      |            |
|            |      |          | 02-7                  | 370       | 580       | 7  | 0.87 | 0.78 | 23.0 | 10.3 | 44.7  | 1.3          |      |            |
| $_{ m ja}$ | 217  | 4/4      | ja-1                  | 460       | 610       | 6  | 0.91 | 0.60 | 14.2 | 7.1  | 20.8  | 0.8          | 20.4 | 0.6        |
|            |      | ,        | ja-2*                 | 490       | 610       | 5  | 0.78 | 0.56 | 48.3 | 27.9 | 20.4  | 0.2          |      |            |
|            |      |          | ja-3                  | 460       | 610       | 6  | 0.91 | 0.62 | 12.6 | 6.3  | 22.2  | 1.0          |      |            |
|            |      |          | ja-4                  | 490       | 610       | 5  | 0.86 | 0.57 | 14.4 | 8.3  | 18.2  | 0.6          |      |            |
| jb         | 214  | 4/4      | jb-1                  | 200       | 610       | 12 | 1.00 | 0.84 | 7.0  | 2.2  | 24.8  | 3.0          | 22.8 | 1.9        |
| -          |      | •        | $\mathrm{jb}	ext{-}2$ | 430       | 610       | 7  | 0.95 | 0.68 | 29.5 | 13.2 | 23.2  | 0.5          |      |            |
|            |      |          | jb-3                  | 490       | 610       | 5  | 0.88 | 0.57 | 14.8 | 8.6  | 18.0  | 0.6          |      |            |
|            |      |          | jb-4                  | 250       | 430       | 5  | 0.33 | 0.69 | 7.5  | 4.3  | 28.5  | 0.9          |      |            |
| $_{ m jc}$ | 209  | 4/4      | jc-1*                 | 20        | 610       | 14 | 0.99 | 0.77 | 26.7 | 7.7  | 15.0  | 0.4          | 14.3 | 1.0        |
|            |      |          | jc-3                  | 20        | 550       | 12 | 0.82 | 0.64 | 7.2  | 2.3  | 14.6  | 1.1          |      |            |
|            |      |          | $ m jc	ext{-}4$       | 460       | 610       | 6  | 0.74 | 0.68 | 8.8  | 4.4  | 10.7  | 0.6          |      |            |
|            |      |          | jc-5*                 | 250       | 490       | 7  | 0.40 | 0.80 | 4.7  | 2.1  | 16.6  | 1.2          |      |            |
| $_{ m jd}$ | 199  | 4/4      | jd-3*                 | 490       | 610       | 5  | 0.70 | 0.67 | 20.8 | 12.0 | 19.1  | 0.4          | 22.0 | 1.4        |
|            |      |          | jd-4                  | 250       | 550       | 9  | 0.84 | 0.81 | 32.5 | 12.3 | 22.4  | 0.5          |      |            |
|            |      |          | jd-5                  | 20        | 350       | 6  | 0.37 | 0.78 | 3.7  | 1.8  | 21.9  | 1.7          |      |            |
|            |      | lla Harr | $_{ m jd}$ -6         | 490       | 610       | 5  | 0.88 | 0.67 | 10.4 | 6.0  | 26.4  | 1.5          |      | ,          |

Site denotes the flow number and Alt their altitude in the profile. The success rate n/N is the number of successful measured samples per site versus the number of treated specimen. The sample name is extended by a superscripted star in case of check corrected analysis.  $T_{min}$  and  $T_{max}$  give the temperature interval used for the paleointensity calculations. N gives the number of successive data points in the used interval, f gives the used fraction of the NRM, g the gap factor and q the quality factor. The weighting factor is denoted w.  $F_i$  and  $\sigma F_i$  give the paleointensity and its standard deviation for each single sample, F gives the weighted mean from the individual paleointensity measurements weighted with the quality factor q and the weighted standard deviation sigma F. If a site only contains two evaluable samples the minimum-maximum deviation was calculated instead of a weighted standard deviation.

Table 3 Paleodip and its direction. N denotes the number of flows used for the calcu-

| Group     | N  | Mean                    | $\alpha_{95}$ | k     | paleodip | paleodip  |
|-----------|----|-------------------------|---------------|-------|----------|-----------|
| (Sites)   |    | $\mathbf{D}/\mathbf{I}$ |               |       |          | direction |
| 1 (jd-05) | 9  | 229.6/-59.1             | 15.1          | 12.6  | 41       | 36        |
| 2 (11-14) | 3  | 62.2/72.3               | 10.3          | 144.0 | 15       | 107       |
| 3 (16-31) | 12 | 202.9/-68.6             | 6.0           | 53.0  | 34       | 14        |
| 4 (34-45) | 10 | 358.1/76.3              | 6.1           | 63.2  | 3        | 4         |
| 5 (50-62) | 8  | 233.8/-81.8             | 5.5           | 103.9 | 19       | 16        |
| Mean      |    |                         |               |       | 24.7     | 16.4      |

The dip direction of group 2 is printed italic, as only three sites contribute to the group mean direction. Therefore this result is assumed to be unreliable.



# 0.5 SP saturation envelope 0.2 SP-SSD 0.05 SP-SSD 0.05 SP-SSD 0.05 SD-MD PSD MD 0.01 1 2 3 5 10 B<sub>cr</sub>/B<sub>c</sub>

