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Singularity Analysis of Zero-Torsion Parallel Mechanisms

Sébastien Briot and Ilian A. Bonev, *Member, IEEE*

Abstract—This paper presents the singularity analysis of four 3-DOF symmetric zero-torsion parallel mechanisms. These mechanisms are composed of three identical legs ending with a spherical joint that is constrained to move in one of three equally spaced plane intersecting at one line. The computation of the singularity loci is based on the degeneracy of the system of screws applied on the platform by the legs. The whole study is based on the use of a special orientation representation, previously introduced under the name of Tilt-and-Torsion angles. This representation is briefly introduced. Then the interdependence between the Cartesian coordinates of the general class of parallel mechanisms is derived. Finally, the singularity loci are derived and the size of the workspace taking into account all singular configurations is shown.

I. INTRODUCTION

FOR the last few decades, parallel mechanisms are increasingly being used and studied. Even if most works on parallel mechanisms were focused on 6-degrees-of-freedom (DOFs) mechanisms (mainly hexapods), recently, more interest has been paid to mechanisms with less than 6 DOFs. The most popular of these mechanisms belong undoubtedly to the group of 3-DOF symmetric parallel mechanisms whose mobile platform is attached to three identical legs via spherical joints (Fig. 1). The legs constrain the centers of the spherical joints to move in three equally spaced vertical planes intersecting at a common line. These mechanisms will be referred to as 3- $[PP]S$ ones¹.

There is abundant literature on this group of mechanisms, studying their kinematics, singularity analysis and design. For example, a 3- $\underline{PPS}$ parallel mechanism was proposed in [1] (Fig. 1a), the 3- $\underline{RPS}$ architecture (Fig. 1b) was analyzed in [2-6], two different 3- $\underline{PRS}$ designs were studied in [7] (Fig. 1c) and [8] (Fig. 1d), the latter design being best known through the *Z3 Head* by DS Technologie [9], and finally a 3- $\underline{RRS}$ robot was investigated in [10]. Of all these publications, only [3] seems to identify the exact nature of the interdependence of the orientation parameters and its geometric significance. To fill this important gap, the second author studied the kinematic geometry of 3- $[PP]S$ parallel mechanisms and showed clearly their motion pattern [11].

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¹ It is common to denote parallel mechanisms by using the symbols P , R , and S , which stand respectively for prismatic, revolute and spherical joint. When a joint is actuated, its symbol is underlined. In this paper, we also use $[PP]$ to denote any combination of joints that allows 2-DOF planar motion.

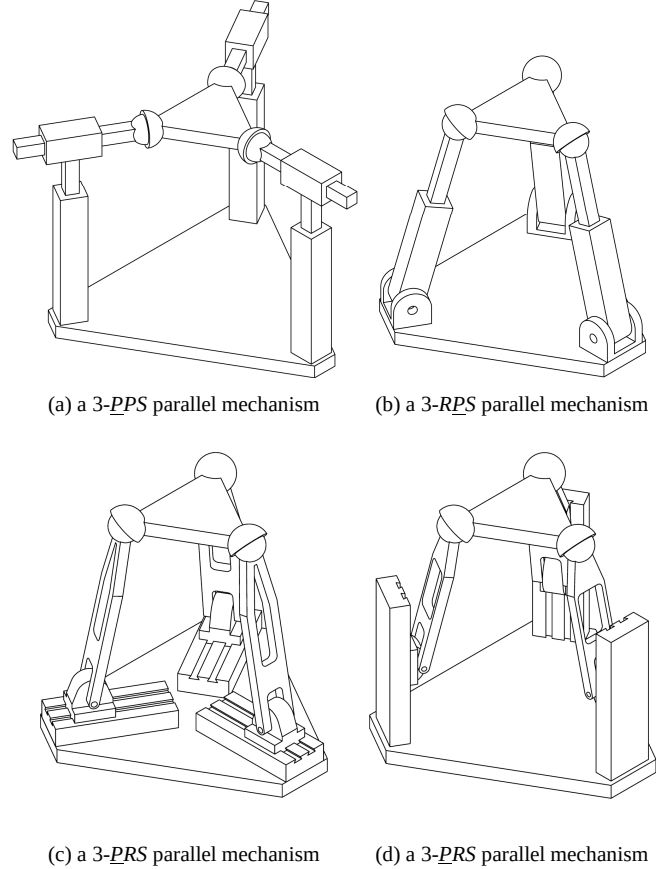


Fig. 1. Examples of 3-DOF 3- $[PP]S$ parallel mechanisms

In this paper, we use a special orientation representation to obtain simplified relations for the singularity analysis of these mechanisms. This orientation representation was recently applied to the derivation of the closed-form direct kinematics of the mechanisms shown in Fig. 1(a-c)[12]. It was shown that this representation considerably simplify the expressions of the direct kinematics of such mechanisms. Thus, in the next section, we describe briefly this orientation representation and use it in Section 3 to derive the simple interdependence between the orientation angles and the position of the platform of a general 3- $[PP]S$ parallel mechanism. Then, in Section 4, we present the expression of the singularity loci of four 3- $[PP]S$ parallel mechanisms, namely the 3- $\underline{PPS}$ design (Fig. 1a), the general 3- $\underline{RPS}$ design (Fig. 1b), and two common 3- $\underline{PRS}$ designs (Fig. 1c and 1d). We also analyze the size of the singularity-free workspace of these structures, as a function of the design parameters, taking into account all singular configurations. Finally, conclusions are drawn in Section 5.

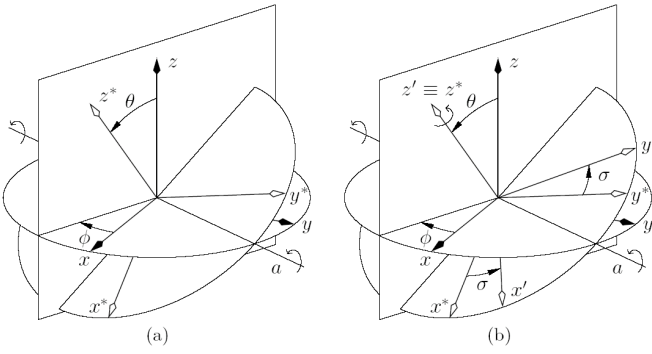


Fig. 2. The successive rotations of the T&T angles: (a) tilt, (b) torsion

II. ORIENTATION REPRESENTATION

A novel three-angle orientation representation, later called the *Tilt-and-Torsion (T&T) angles*, was proposed in [13] in 1999, in conjunction with a new method for computing the orientation workspace of symmetric spatial parallel mechanisms. It was shown that the T&T angles take full advantage of a mechanism's symmetry. These angles were also independently introduced in [14] and [15] in 1999. Later, it was found out that the angles had been proposed in [16] in 1984 under the name *halfplane-deviation-twist* angles. The author of that reference proposed the set due to its indisputable advantages in modeling the limits of human body joints. Yet, again in 1999, these angles were proposed independently in [17] as a new standard in modeling angular joint motion, and particularly that of the spinal column's vertebra. These angles are also used for computer animation of articulated bodies, known as the *swing-and-twist* representation. In [11], the advantages of the T&T angles in the study of spatial parallel mechanisms were further demonstrated. It was shown that there is a class of 3-DOF mechanisms that have always a zero torsion, that we now call *zero-torsion parallel mechanisms*. Furthermore, it was demonstrated in [18] and [19] that the workspace and singularities of symmetric spherical parallel mechanisms are best analyzed using the T&T angles.

The T&T angles are defined in two stages—a tilt and a torsion. This does not, however, mean that only two angles define the T&T angles but simply that the axis of tilt is variable and is defined by another angle. In the first stage, illustrated in Fig. 2a, the body frame is tilted about a horizontal axis, a , at an angle θ , referred to as the *tilt*. The axis a is defined by an angle ϕ , called the *azimuth*, which is the angle between the projection of the body z' axis onto the fixed xy plane and the fixed x axis. In the second stage, illustrated in Fig. 2b, the body frame is rotated about the body z' axis at an angle σ , called the *torsion*.

For space limitations, we will omit the otherwise quite interesting details of the derivation process (see [11]), and write directly the resulting rotation matrix of the T&T angles, which is

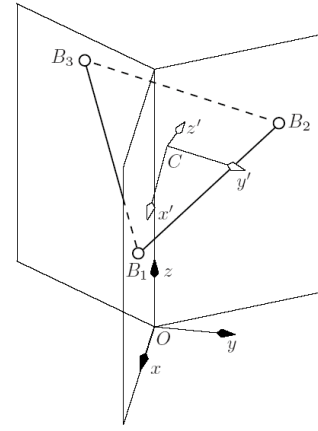


Fig. 3. Kinematic geometry of a general 3-[PP]S parallel mechanism

$$\mathbf{R}(\phi, \theta, \sigma) = \begin{bmatrix} c_\phi c_\theta c_{\sigma-\phi} - s_\phi s_{\sigma-\phi} & -c_\phi c_\theta s_{\sigma-\phi} - s_\phi c_{\sigma-\phi} & c_\phi s_\theta \\ s_\phi c_\theta c_{\sigma-\phi} + c_\phi s_{\sigma-\phi} & -s_\phi c_\theta s_{\sigma-\phi} + c_\phi c_{\sigma-\phi} & s_\phi s_\theta \\ -s_\theta c_{\sigma-\phi} & s_\theta s_{\sigma-\phi} & c_\theta \end{bmatrix}, \quad (1)$$

where $c_\phi = \cos \phi$, $s_\phi = \sin \phi$, $c_\theta = \cos \theta$, $s_\theta = \sin \theta$, $c_{\sigma-\phi} = \cos(\sigma-\phi)$ and $s_{\sigma-\phi} = \sin(\sigma-\phi)$.

One of the properties of three-angle orientation representation is that a given orientation can be represented by at least two triplets of angles. In our case, the triplets $\{\phi, \theta, \sigma\}$ and $\{\phi \pm \pi, -\theta, \sigma\}$ are equivalent. To avoid this and the representational singularity at $\theta = \pi$ (which is hardly achieved by any parallel mechanism), we set the ranges of the azimuth, tilt, and torsion as, respectively, $\phi \in (-\pi, \pi]$, $\theta \in [0, \pi)$, and $\sigma \in (-\pi, \pi]$. Then, probably the most valuable property of the T&T angles is that for the ranges just defined, the angles (ϕ, θ, σ) can be represented in a cylindrical coordinate system (r, ϕ, h) through a one-to-one mapping. In other words, any orientation (except a $\theta = \pi$ one) corresponds to a unique point within a cylinder in the cylindrical coordinate system, and vice versa. The reason is that the T&T representational singularity at $\theta = 0$ is of the same nature as the singularity of the cylindrical coordinate system occurring at zero-radius ($r = 0$).

III. KINEMATIC GEOMETRY OF 3-[PP]S PARALLEL MECHANISMS

As already mentioned, each leg of a 3-[PP]S parallel mechanisms has a 2-DOF planar chain, followed by an S joint. The vertical planes in which the three equidistant S joints move are intersecting at a common line at 120° (Fig. 3). Now, let $O - xyz$ be the base reference frame, such that its z axis coincides with the common line of the three planes, and its x axis lies in the plane of leg 1.

For brevity, let the three equidistant S joint centers, denoted by B_i , lie on a circle of radius 1, i.e.,

$$\mathbf{r}'_{CB_1} = [1, 0, 0]^T, \quad (2)$$

$$\mathbf{r}'_{CB_2} = [\cos(2\pi/3), \sin(2\pi/3), 0]^T, \quad (3)$$

$$\mathbf{r}'_{CB_3} = [\cos(4\pi/3), \sin(4\pi/3), 0]^T, \quad (4)$$

where $\mathbf{r}'_{CBi}$ are the vectors along CB_i expressed in the mobile frame $C - x'y'z'$. We, then, express the coordinates of these three points in terms of the coordinates of the platform center, x, y, z , and the three T&T angles:

$$\mathbf{r}_{OB_i} = \mathbf{R}\mathbf{r}'_{OB_i} + \begin{bmatrix} x \\ y \\ z \end{bmatrix} = \begin{bmatrix} x_{OB_i} \\ y_{OB_i} \\ z_{OB_i} \end{bmatrix}, \quad (5)$$

where $\mathbf{R}$ is the rotation matrix defined by (1) (in this paper, $i = 1, 2, 3$). Then, we write the three linear equations that constrain the S joint centers in the three vertical planes:

$$y_{OB_1} = 0, \quad (6)$$

$$\cos(2\pi/3)y_{OB_2} - \sin(2\pi/3)x_{OB_2} = 0, \quad (7)$$

$$\cos(4\pi/3)y_{OB_3} - \sin(4\pi/3)x_{OB_3} = 0, \quad (8)$$

Since z is obviously an independent coordinate, it is of no surprise that, after substitution of y_{OB_1} , x_{OB_2} , y_{OB_2} , x_{OB_3} , and y_{OB_3} from (5), none of the above three equations contains that variable:

$$y + q_{1,3} = 0, \quad (9)$$

$$-\frac{\sqrt{3}}{2}x - \frac{1}{2}y + q_{2,3} = 0, \quad (10)$$

$$\frac{\sqrt{3}}{2}x - \frac{1}{2}y + q_{3,3} = 0, \quad (11)$$

where $q_{1,3}$, $q_{2,3}$, and $q_{3,3}$ are functions of the three T&T angles. Therefore, in order to have a solution for x and y , the three linear equations must be linearly dependent. Obviously, any two of these equations are linearly independent. Hence, for any feasible orientation of the mobile platform, there is a unique solution for $\{x, y\}$.

Let $\mathbf{Q}$ be the coefficient matrix for the above three equations, i.e.,

$$\mathbf{Q} = \begin{bmatrix} 0 & 1 & q_{1,3} \\ -\frac{\sqrt{3}}{2} & -\frac{1}{2} & q_{2,3} \\ \frac{\sqrt{3}}{2} & -\frac{1}{2} & q_{3,3} \end{bmatrix}. \quad (12)$$

For these equations to be linearly dependent, the matrix $\mathbf{Q}$ should be singular, i.e.,

$$\det \mathbf{Q} = \frac{3\sqrt{3}}{4} \sin \sigma (\cos \theta + 1) = 0. \quad (13)$$

Disregarding $\theta = \pi$, (13) leads us to the only remaining possibility: $\sigma = 0$ or $\sigma = \pi$. If we substitute $\sigma = 0$ or $\sigma = \pi$ in (9–11), and solve any two of them, we obtain the following for the feasible motion of the mobile platform center:

$$x = \delta \frac{1}{2} \cos 2\phi (\cos \theta - 1), \quad (14)$$

$$y = -\delta \frac{1}{2} \sin 2\phi (\cos \theta - 1), \quad (15)$$

where $\delta = 1$ for $\sigma = 0$ and $\delta = -1$ for $\sigma = \pi$. These two modes of operation are separated by a *constraint singularity*, which

occurs at $\theta = 0$. Indeed, as shown in [20], constraint singularities generally separate the different modes of operation of constrained parallel mechanisms. While both modes exist in theory, in practice the tilt angle θ will be quite limited, and the actual prototype will be confined to operate in only one of the modes. Furthermore, in practice, the mode $\sigma = \pi$ is hardly realizable. Therefore, for any practical 3-[PP]S parallel mechanism, $\sigma = 0$.

Let us now analyze the singularity loci of several examples of 3-[PP]S parallel mechanisms.

IV. SINGULARITY LOCI OF 3-[PP]S PARALLEL MECHANISMS

Among the abundant literature devoted to 3-[PP]S mechanisms, only a few papers deal with the subject of singularities [5, 6, 21, 22]. Among these papers, references [5, 6] present the singularity analysis of a 3-RPS structure. However, in both papers, the obtained expressions are numerous and complicated due to the use of general Euler angles and are basically not exploitable. Reference [21] presents a short singularity analysis of the 3-PPS structure, but gives no expressions characterizing the singular configurations. Finally, reference [22] presents a geometric approach to finding Type 2 singularities of three-legged parallel mechanisms.

In this section, we will analyze the Type 2 singularities of four 3-[PP]S parallel mechanisms, namely the 3-PPS design, proposed in [1] (Fig. 1a), the general 3-RPS design (Fig. 1b), and the two 3-PPS designs proposed in [7] and [8] (Fig. 1c and 1d). To realize this analysis, we will study the degeneracy of a 6-dimensional matrix composed of the screws applied on the platform by the moving legs and will give for the first two mechanisms (the 3-PPS and the 3-RPS) simple analytical expressions characterizing the singularity loci obtained by the use of the T&T angles. We will show for the other two mechanisms that the singularity loci can be represented by a polynomial of high order (of degree 24). Moreover, for each mechanism, the maximal reachable workspace taking into account the singular configuration will be represented as a function of the design parameters.

A. Singularity Loci of 3-PPS Parallel Mechanisms

Referring to Fig. 4, the directions of the actuated prismatic joints are vertical, while the directions of the passive prismatic joints are horizontal.

Each leg applied two screws $\mathbf{R}_{i1}$ and $\mathbf{R}_{i2}$ on the platform. Thus, as shown on Fig. 4, for this manipulator, $\mathbf{R}_{i1}$ and $\mathbf{R}_{i2}$ are two forces located at point B_i and directed along the vertical axis z and perpendicular to the plane of the legs, respectively. The system of screws degenerates if the determinant of matrix $\mathbf{J}$, of which the lines are composed of the coordinates of the screws $\mathbf{R}_{ij}$ ($j = 1, 2$), vanishes. After simplification, this determinant can be written as:

$$\det \mathbf{J} = \frac{27}{8} \cos \theta (1 + \cos \theta), \quad (17)$$

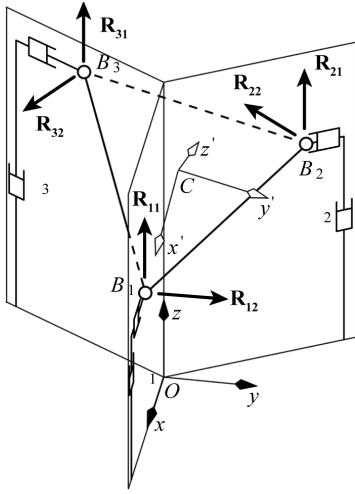


Fig. 4. Schematics of a 3-PPS parallel mechanism

Disregarding $\theta = \pi$, (13) leads us to the only remaining possibility for Type 2 singularities: $\theta = \pm\pi/2$.

Thus, for any 3-PPS parallel manipulator, the workspace is bounded by the orientation $\theta = \pm\pi/2$ of the platform, for any altitude z and angle ϕ .

B. Singularity Loci of 3-RPS Parallel Mechanisms

As shown in Fig. 5, for this mechanism, $\mathbf{R}_{i1}$ and $\mathbf{R}_{i2}$ are two forces located at point B_i , the first directed along the line A_iB_i and the second perpendicular to the plane of the legs. The system of screws degenerates if:

$$\det \mathbf{J} = c_2 \cos^2(3\phi) + c_1 \cos(3\phi) + c_0 = 0, \quad (18)$$

where c_0 , c_1 and c_2 depend on angle θ , on the altitude z of the center of the platform and on the radius R_b of the circumcircle of the base,

$$\begin{aligned} c_2 &= \frac{27}{16} z (1 + \cos \theta) (\cos \theta - 1)^3, \\ c_1 &= -\frac{27}{64} s_\theta (c_\theta - 1) (c_\theta (-c_\theta^2 + 3c_\theta + 1) + z^2 (12c_\theta + 8R_b + 4)) \\ &\quad - \frac{27}{64} s_\theta (c_\theta - 1) (2R_b (c_\theta + 1) (-c_\theta + 4R_b - 1) - 3) \\ c_0 &= -\frac{27}{32} z (c_\theta + 1) (-c_\theta (-c_\theta^2 - 4c_\theta + 3) + 4c_\theta z^2) \\ &\quad - \frac{27}{32} z (c_\theta + 1) (4R_b (c_\theta - 1) (c_\theta + 2R_b)) \end{aligned}$$

Therefore, it is quite simple to find the exact expression of the singularity loci expressing angle ϕ as a function of the other parameters:

$$\phi = \frac{1}{3} \cos^{-1} \left(\frac{-c_1 \pm \sqrt{c_1^2 - 4c_2 c_0}}{2c_2} \right) + \frac{2n\pi}{3}, \quad n = 0, 1, 2 \dots \quad (19)$$

Fig. 6 shows an example of singularity loci in the workspace of a 3-RPS parallel mechanism with $R_b = 1.3$ for $z = 1$. We can now analyze the size of the workspace represented by the maximal reachable angle θ for any angle ϕ as a function of the altitude of the platform and of the design parameters R_b (Fig. 7).

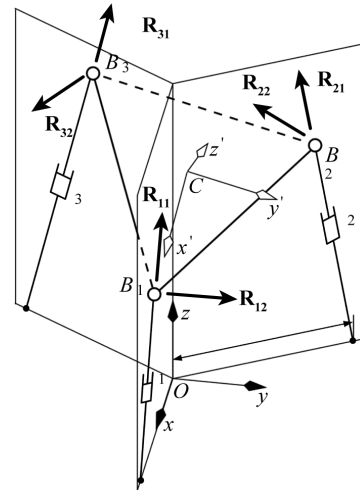


Fig. 5. Schematics of a 3-RPS parallel mechanism

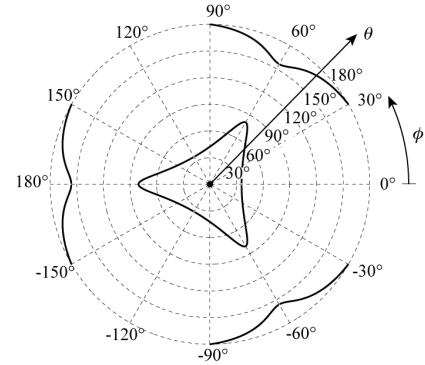


Fig. 6. Singularity loci in the workspace of a 3-RPS parallel mechanism with $R_b = 1.3$ for $z = 1$

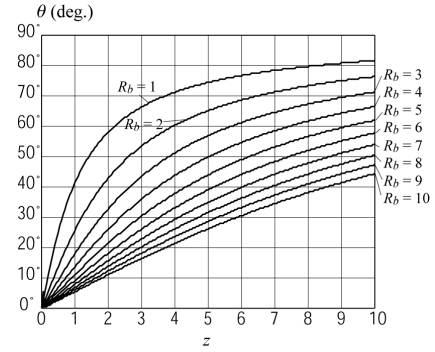


Fig. 7. Maximal reachable angle θ for any angle ϕ

The approach used to compute the maximal reachable angle θ can be described as follows. First, we fix the design parameter R_b and discretize the variable space $\{z, \phi, \theta\}$. Then, for a given set of variables $\{z, \phi\}$ and starting from $\theta = 0$, we observe the evolution of the sign of the determinant of matrix $\mathbf{J}$ when θ is varying. We met a singularity if, between two values of θ , the sign of $\det \mathbf{J}$ varies. Thus, we stop the procedure and retain the value θ_m of angle θ just before crossing the singular configuration. Then, we redo this algorithm for another value of angle ϕ . When this procedure has been realized for any angle ϕ , we

find the minima of the angles θ_m , plot it on Fig. 7 and execute another time the entire algorithm.

Thus, it can be observed that the size of the workspace increases with the altitude of the platform and decrease with the value of R_b .

C. Singularity Loci of 3-RPS Parallel Mechanisms

As for the previous mechanism, $\mathbf{R}_{i1}$ and $\mathbf{R}_{i2}$ are two forces located at point B_i , the first directed along the direction of the leg and the second perpendicular to the plane of the legs. The system of screws degenerates if:

$$\det \mathbf{J} = A_1 \Gamma_2 \Gamma_3 + A_2 \Gamma_1 \Gamma_3 + A_3 \Gamma_1 \Gamma_2 + B_1 \Gamma_1 + B_2 \Gamma_2 + B_3 \Gamma_3 + C = 0 \quad (20)$$

for the mechanism of Fig. 1c, with

$$A_1 = A(\phi) = \frac{9}{8}(c_\phi - 1)(c_\phi + 1)(c_\theta - 1)(c_\theta + 1)(z - c_\phi s_\theta),$$

$$A_2 = A(\phi - 2\pi/3), A_3 = A(\phi + 2\pi/3),$$

$$B_1 = B(\phi) = -\frac{9}{64}c_\phi(1 - 4c_\phi^2 - 7c_\theta + 4c_\phi^2 c_\theta) \\ (4c_\phi^2 s_\theta^3 + 4c_\phi z s_\theta^2 + 3c_\theta^2 + 4z^2 s_\theta - 3s_\theta)$$

$$B_2 = B(\phi - 2\pi/3), B_3 = B(\phi + 2\pi/3),$$

$$C = -\frac{27}{32}c_\theta(c_\theta + 1)(-s_\theta^3 c_{3\phi} - 3s_\theta^2 z + 4z^3),$$

$$\Gamma_1 = \pm\Gamma(\phi), \text{ where } \Gamma(\phi) = 2\sqrt{L^2 - z^2 + 2c_\phi s_\theta z - c_\phi^2 s_\theta^2}$$

$$\Gamma_2 = \pm\Gamma(\phi - 2\pi/3), \Gamma_3 = \pm\Gamma(\phi + 2\pi/3),$$

and,

$$\det \mathbf{J} = D \Delta_1 \Delta_2 \Delta_3 + E_1 \Delta_2 \Delta_3 + E_2 \Delta_1 \Delta_3 + E_3 \Delta_1 \Delta_2 + F_1 \Delta_1 + F_2 \Delta_2 + F_3 \Delta_3 = 0 \quad (21)$$

for the mechanism of Fig. 1d, with

$$D = -\frac{27}{6}c_\theta(c_\theta + 1),$$

$$E_1 = E(\phi) = \frac{9}{64}s_\theta c_\phi(-4c_\phi^2 - 7c_\theta + 4c_\phi^2 c_\theta + 1) \\ (-4c_\phi^2 c_\theta + c_\theta + 4c_\phi^2 - 3 + 2R_b)$$

$$E_2 = E(\phi - 2\pi/3), E_3 = E(\phi + 2\pi/3),$$

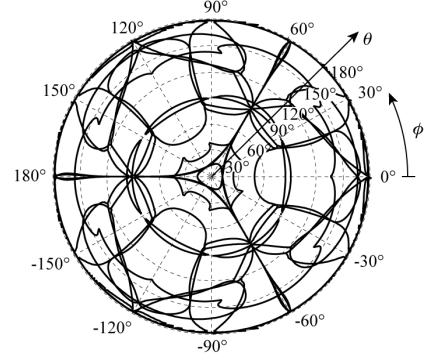
$$F_1 = F(\phi) = \frac{9}{4}s_\theta^2 s_\theta^2(4c_\phi^4(c_\theta^2 - 2c_\theta + 1) \\ + c_\phi^2(-5c_\theta^2 + 8c_\theta + 2R_b c_\theta - 2R_b - 3) \\ + c_\theta^2 - 2R_b c_\theta + R_b^2)$$

$$F_2 = F(\phi - 2\pi/3), F_3 = F(\phi + 2\pi/3),$$

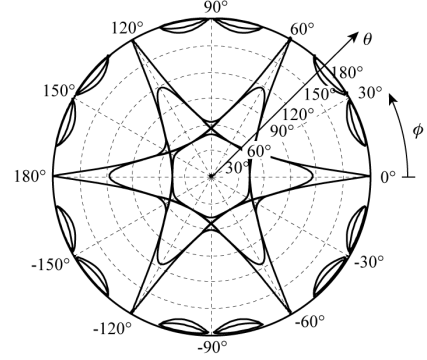
$$\Delta_1 = \pm\Delta(\phi), \text{ where}$$

$$\Delta(\phi) = (4L^2 + 3\sqrt{3} + (16\sqrt{3} - 28)c_\phi^4 - (16(\sqrt{3} + R_b) - 30 \\ - 8\sqrt{3}R_b)c_\phi^2 + (12 - 2\sqrt{3})R_b + 4R_b^2 - 39/4)^{1/2}$$

$$\Delta_2 = \pm\Delta(\phi - 2\pi/3), \Delta_3 = \pm\Delta(\phi + 2\pi/3).$$

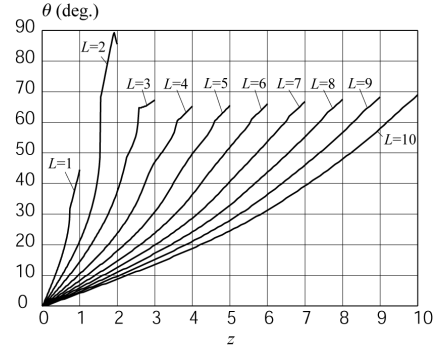


(a) for the mechanism of Fig. 1c, for $L = 1.3$ and $z = 0.5$

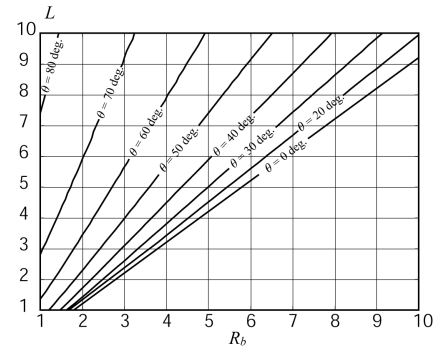


(b) for the mechanism of Fig. 1d, for $L = 1$ and $R_b = 1.3$

Fig. 8. Singularity loci in the workspace of the 3-PRS parallel mechanisms under study



(a) for the mechanism of Fig. 1c



(b) for the mechanism of Fig. 1d

Fig. 9. Maximal reachable angle θ for any angle ϕ

In these expressions, Γ_i and Δ_i are radicals depending on the working mode (solution of the inverse kinematics) of the mechanism. Thus, Type 2 singularity loci are much more complicated to determine due to the existence of these terms.

Indeed, to eliminate all radicals in the equation $\det \mathbf{J}$, the latter should be rearranged and squared three times, using a similar method as that proposed in [23] for the 3-RRR planar parallel robot. The equation resulting after these operations corresponds to all eight working modes.

Since this procedure cannot be performed symbolically, we firstly assign random integer values to the coefficients θ , R_b , L , and z . Then, we eliminate the radicals by rearranging terms and squaring three times the equations. Finally, as the system is symmetrical, it is possible to rearrange the obtained polynomial in $\cos \phi$ and $\sin \phi$ into a polynomial in $\cos 3\phi$. Finally, it can be observed that the obtained polynomials are of degree 16 for the mechanism of Fig. 1c, and of degree 24 for the mechanism of Fig. 1d.

Fig. 8 shows examples of singularity loci in the workspace of the 3-PRS parallel mechanisms under study.

Finally, we analyze the size of the singularity-free workspace represented by the minimum of all maximal reachable angles θ for any angle ϕ , without reaching a singularity, as a function of the altitude of the platform and of the design parameters R_b and L (Fig. 9a and 9b). We use an algorithm similar to that used for the 3-RPS parallel mechanism. It can be observed that:

- for the mechanism of Fig. 1c, the size of the singularity-free workspace increases with the altitude of the platform; moreover, for L close to 2 and for a high altitude z , the value of angle θ reaches 90° .
- for the mechanism of Fig. 1d, the size of the singularity-free workspace increases when L increase and R_b decrease; moreover, for R_b close to 1, the value of angle θ reaches 80° .

V. CONCLUSIONS

We presented in this paper yet another example of the advantages of using Tilt-and-Torsion angles for the analysis of 3-DOF zero-torsion parallel mechanisms. In particular, we proposed, for the first time, simple expressions for the singular configurations of four different zero-torsion mechanisms, namely a 3-PPS design, the general 3-RPS design, and two 3-PRS design. Furthermore, we analyzed the maximal singularity-free workspace of these mechanisms as a function of their design parameters. It should now be clear that so-called zero-torsion parallel mechanisms must be analyzed using Tilt-and-Torsion angles only.

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