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Predictive Current Control for an Induction Motor

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Abstract—This paper presents a Predictive Current Control (PCC) strategy applied to an Induction Motor (IM) drive. In contrast to conventional vector control, where the inverter is not taken into account by the controller, the PCC considers the state of the inverter as a discrete control variable. Based on a simplified state space model of the IM and the inverter, the proposed control scheme calculates the state vector evolution direction in the d- and q-reference frame for all possible switching states of the inverter. The switching state which minimizes a given cost function is selected and is applied during an adapted duration which is calculated for each computation cycle. As the control requires the knowledge of the instantaneous rotor fluxes and in order to improve the control robustness, a reduced-order extended high gain observer is proposed for estimation of rotor fluxes and inverse rotor time constant. The simulation results validate the observer. The controller is implemented on a 5.5kW IM drive with a Digital-Signal-Processor (DSP) on a DSpace1103 board. Experimental results show the effectiveness and the performances of the proposed control.

Keywords—Predictive current control; induction motor; inverter; high gain observer.

I. INTRODUCTION

In AC-drive systems, fast current and torque responses are necessary. The development of high performance controls for AC-machine drives has motivated considerable attention in recent years. Many studies are reported for current controls [1-3].

The main objective of the current control is to ensure the tracking of the desired stator currents in a transient interval as short as possible. There are different strategies for current controllers. The main ones including linear control, hysteresis control, and predictive control are discussed in [4]. Among them, a widely used scheme for high performance is the predictive control. The method presented [5] and [6] uses Model Predictive Control (MPC) theory to determine the optimal set of switching states with a prediction horizon of 3, but the real-time constraint is great due to the complexity of MPC algorithm. The approach presented here consists in designing an extended observer allowing online estimation of the rotor fluxes and the stator pulsation. Indeed, the motor parameters, notably the rotor resistance value, can change with temperature. The incertitude on parameters induces estimation errors which can deteriorate the control quality. In order to achieve better system dynamic performance and robustness, the approach proposed in this paper consists in designing an extended observer allowing online estimation of the rotor fluxes and the inverse rotor time constant. Simulation studies show the feasibility of the approach. Experimental results are carried out on a real induction motor driver with a Digital-Signal-Processor for the proposed predictive current control.

II. MODELS

The IM is classically modelled by continuous state space equations written in the d-q rotor flux reference frame.

\[ \dot{X} = A(\omega_s, \omega_r) X + BU \]  

with

\[ X = \begin{bmatrix} \Phi_{rd} & \Phi_{rq} & I_{sd} & I_{sq} \end{bmatrix}^T \] \[ U = \begin{bmatrix} V_{sd} & V_{sq} \end{bmatrix}^T \]

\[ A(\omega_s, \omega_r) = \begin{bmatrix} -\sigma_r & \omega_r - \omega_s & \sigma L_m & 0 \\ -\omega_s & -\sigma_r & 0 & \sigma L_m \\ \sigma \beta & \beta \omega_r & -\lambda & \omega_s \\ -\beta \omega_s & \beta \sigma_r & -\omega_s & -\lambda \end{bmatrix} \]

\[ B = \begin{bmatrix} 0 & 0 & \frac{1}{\sigma L_r} & 0 \\ 0 & 0 & 0 & \frac{1}{\sigma L_r} \end{bmatrix} \]
TABLE I. INVERTER SWITCHING STATES

<table>
<thead>
<tr>
<th>j</th>
<th>0</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
<th>6</th>
<th>7</th>
</tr>
</thead>
<tbody>
<tr>
<td>$u_A$</td>
<td>0</td>
<td>1</td>
<td>1</td>
<td>0</td>
<td>0</td>
<td>0</td>
<td>1</td>
<td>1</td>
</tr>
<tr>
<td>$u_B$</td>
<td>0</td>
<td>0</td>
<td>1</td>
<td>1</td>
<td>1</td>
<td>0</td>
<td>0</td>
<td>1</td>
</tr>
<tr>
<td>$u_C$</td>
<td>0</td>
<td>0</td>
<td>0</td>
<td>1</td>
<td>1</td>
<td>1</td>
<td>1</td>
<td>1</td>
</tr>
</tbody>
</table>
The proposed predictive control requires the knowledge of the rotor fluxes which are not usually measurable in practice. An observer for estimation of the rotor fluxes is necessary. As previously mentioned, the control quality depends on the model accuracy. A variation of the rotor resistance (which varies with temperature) can induce a performance degradation of the system. So an extended observer which allows an on-line estimation of fluxes and inverse rotor time constant \( r \) is proposed. As currents are measured, they can be extracted from the state vector of the observer. The extended reduced order state space equation (7) is used.

\[
\begin{align*}
\dot{X}_r &= f_r(X_r) + g_r(X_r,U_r), \\
\dot{y}_r &= h_r(X_r)
\end{align*}
\]

\[
X_r = \begin{bmatrix} \Phi_{rd} & \Phi_{rq} & \sigma_r \end{bmatrix} = \begin{bmatrix} x_1 & x_2 & x_3 \end{bmatrix}^T
\]

\[
U_r = \begin{bmatrix} I_{rd} & I_{rq} \end{bmatrix}^T
\]

\[
y_r = \begin{bmatrix} \Phi_{rdp} & \Phi_{rqp} \end{bmatrix}^T
\]

\[
f_r(x_r) = \begin{bmatrix} -x_3 & (\omega_q - \omega_p)x_2 \\
-(\omega_p - \omega_q)x_2 & x_2x_3 \\
0
\end{bmatrix},
\]

\[
g_r(X_r,U_r) = \begin{bmatrix} L_{nr}x_3u_{r1} \\
L_{nr}x_3u_{r2} \\
0
\end{bmatrix}
\]

As the system (7) is nonlinear, a high gain nonlinear observer \([10]\) is realized.

\[
\dot{\hat{X}}_r = f_r(\hat{X}_r) + g_r(\hat{X}_r)U_r + G(\hat{X}_r,U_r,y_r)(y_r - h_r(\hat{X}_r)) \tag{8}
\]

Unlike linear observers, the gain matrix \( G(\hat{X}_r,U_r,y_r) \) is not a constant but a nonlinear function of \( \hat{X}_r \), \( U_r \), and \( y_r \). \( y_r \) is obtained from current and the stator voltage measurements by solving the differential equations (9).

\[
\begin{align*}
\frac{d\Phi_{rdp}}{dt} &= \frac{L_r}{L_{nr}}(V_{rd} - R_dI_{rd}) - \frac{\sigma L_r}{L_{nr}} \frac{dI_{rd}}{dt} - \omega_p \Phi_{rd}, \\
\frac{d\Phi_{rqp}}{dt} &= \frac{L_r}{L_{nr}}(V_{rq} - R_qI_{rq}) - \frac{\sigma L_r}{L_{nr}} \frac{dI_{rq}}{dt} + \omega_p \Phi_{rqp} \tag{9}
\end{align*}
\]

The matrix \( G(\hat{X}_r,U_r,y_r) \) is designed as follows so that the error dynamic is asymptotically stable.

With this transformation the state equation (7) is the sum of a linear term plus a non linear one. Furthermore the outputs are linear functions of the new state \( Z_r = (z_{r1}, z_{r2}, z_{r3})^T \) (11).

\[
\begin{bmatrix} \dot{z}_{r1} \\ \dot{z}_{r2} \\ \dot{z}_{r3} \end{bmatrix} = \begin{bmatrix} A_1 & 0_{2,1} & 0 \\ 0_{1,2} & A_2 & 0 \\ 0_{1,2} & C_2 & A_2 \end{bmatrix} \begin{bmatrix} z_{r1} \\ z_{r2} \\ z_{r3} \end{bmatrix} + \begin{bmatrix} 0 \\ \phi_1(Z_r,U_r) \\ \phi_2(Z_r,U_r) \end{bmatrix} \tag{11}
\]

\[
A_1 = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix}, \quad A_2 = 0, \quad C_1 = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, \quad C_2 = 1
\]

\[
\phi_1(Z_r,U_r) = \frac{\omega_p - \omega_q}{z_{r1}}z_{r3} - \frac{z_{r2}}{z_{r1}} \left[ \frac{\omega_p - \omega_q}{z_{r3}} - \frac{z_{r2}}{z_{r3}} \frac{L_{nr}u_{r3}}{z_{r1}} \right]
\]

\[
\phi_2(Z_r,U_r) = -\frac{\omega_p - \omega_q}{z_{r1}}z_{r3} - \frac{z_{r2}L_{nr}u_{r3}}{z_{r1}} \tag{12}
\]

In this way, the dynamic system (12) is an exponential observer for the system (11), where \( \Lambda \) is defined in (13).

\[
\dot{\hat{Z}}_r = A_r(\hat{Z}_r) + \phi_r(\hat{Z}_r,U_r) + \Lambda^v K(y_r - C_r Z_r) \tag{12}
\]

\[
\Lambda = \begin{bmatrix} T_1 & 0 & 0 \\ 0 & T_2^2 & 0 \end{bmatrix} \quad \text{with} \quad T_1 > 0 \tag{13}
\]

IV. REDUCED ORDER EXTEND HIGH GAIN OBSERVER

Figure 2. PCC principle for IM driver
TABLE II. PARAMETERS OF THE INDUCTION MOTOR

<table>
<thead>
<tr>
<th>P = 5.5 kW</th>
<th>U = 220 V</th>
<th>I = 20.2 A</th>
<th>p = 2</th>
</tr>
</thead>
<tbody>
<tr>
<td>f = 50 Hz</td>
<td>( \Omega = 1420 \text{ rpm} )</td>
<td>( J = 0.248 \text{ kg N m}^2 )</td>
<td>( d = 0.05 \text{ N m s rad}^{-1} )</td>
</tr>
<tr>
<td>( R_r = 1 \Omega )</td>
<td>( R_s = 1.179 \Omega )</td>
<td>( L_r = 0.1197 \text{ H} )</td>
<td>( L_s = 0.116 \text{ H} )</td>
</tr>
</tbody>
</table>

\( K \) is a gain matrix which is chosen that \( (A_t - KC_r) \) is Hurwitz. The dynamic of observer (12) can be adjusted through \( K \) and \( \hat{T}_{12} \).

From (10) to (12), going back to the original system of coordinates, an observer for system (7) is then given by (14).

\[
\dot{\hat{x}} = f(\hat{x}) + g(\hat{x})u + \left[ \frac{\partial G(\hat{x})}{\partial \hat{x}} \right]^{-1}\Lambda^{-1}K\left( y - h(\hat{x}) \right) \tag{14}
\]

with \( \frac{\partial G(x)}{\partial x} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & -x_{r3} & (\omega_s - \omega_r) - x_{r1} \\ 0 & 1 & 0 \end{bmatrix} \)

This Jacobian matrix is invertible if \( x_{r1} = \Phi_{rd} \neq 0 \).

V. SIMULATION RESULTS

In order to verify the feasibility of the proposed high gain observer, the simulation on SIMULINK from Mathwork has been carried out for a 5.5 kW induction motor. The high gain observer is implanted in a S-function using C language.

For the hybrid control, a first order Taylor expansion is retained to approximate the model (4). A second or third order expansion can be developed for the simulation, but it will increase the complexity and the computation duration for real-time implementation.

The maximum application time \( \tau_{max} \) has been limited to 100 ms which can guarantee the rectilinearity of state trajectories. The minimum application time \( \tau_{min} \) is set to 10 \( \mu \)s.

The current references are generated by a speed control loop. A discrete-time PI controller determined by pole assignment is used. The closed-loop dynamic corresponds to a discrete-time first order with a time constant of 0.1 s.

The nominal parameters of the induction motor are given in the Tab. II. The rotor flux references are fixed to nominal value (1.14 \text{ Wb}) for \( \Phi_{rd} \) and 0 \text{ Wb} for \( \Phi_{rq} \).

In order to evaluate the observer performances and effectiveness, the comparisons between the observed state variables and the simulated ones have been realized for several operating conditions.

Fig. 3 to 6 show the simulation results for a step input of the speed reference \( \Omega^\# \), from 0 to 500 rpm. In order to verify the inverse rotor time constant tracking, the simulation is realized with 50% variation of the nominal rotor resistance \( (R_r = 1.5R_{nom}) \).

One can see that the estimated values of fluxes (Fig. 4) and inverse rotor time constant (Fig. 5) converge very well to their simulated values.

Current ripples can be noted on Fig. 6. This is because the predictive current control applies only one converter configuration by cycle. As there are only seven possible configurations, the corresponding state vectors could not reach exactly the reference point. When the state is close to the reference point, as \( \tau \) is limited to \( \tau_{min} \), the state vector could then oscillate around the reference point. The smallest the \( \tau_{min} \) value, the lowest the current ripple.
VI. EXPERIMENTAL RESULTS

The experiment study was conducted with the equipment pictured in Fig. 7.

The IM used is the same as for simulations. A commercial 15kW three-phase inverter, three LEM current sensors and a 2000-pulse incremental encoder are used.

The control algorithm is implemented in C language on a DSpace DS1103 board. The digital I/O port is used to control the configuration of the inverter. A FPGA interface is added to perform dead times (set to 5μs) in inverter legs. At the moment of the paper redaction, the proposed high gain observer is not yet implemented for real-time operation. So the fluxes and the stator pulsation are estimated by the classical way using nominal parameters. The maximum and minimum times of application are kept as for the simulations.

Firstly the rotor is locked in order to show torque dynamic without the influence of speed.

Experimental results in Fig. 8 correspond to a transient response from a negative current reference \( I_{sq} = -16 \) A to a positive reference \( I_{sq} = 16 \) A while \( I_{sd} \) is set to 10 A, \( \Phi_{rd} = 1.14 \) Wb and \( \Phi_{rq} = 0 \) Wb. This experiment corresponds to a torque reference step from -37Nm to 37Nm (Fig. 9) which is equivalent to a nominal electromagnetic torque inversion for this machine. It can be seen that the steady-state operation is reached without any overshoot neither for \( I_{sd} \) nor for \( I_{sq} \). Moreover, the time response is lower than 700μs.

Secondly the speed control loop is added. The discrete-time PI controller used is the same as for simulations. Fig.10 corresponds to an evolution of the motor speed from -500rpm to 500rpm for a load torque of about 5 Nm. The speed dynamic is respected but it does not correspond to a first order dynamic. This can be explained by the mechanical model error due to parameter incertitude and frictions.

The transient evolution of the currents in the d-q reference frame (Fig. 11) shows that the step change of speed produces a change of the current \( I_{sq} \) from -2.5 A to 20 A. The current \( I_{sq} \) is maintained at 10 A without any cross-coupling effect. Current ripples can be found as on simulation.

Due to the PI speed controller, the torque reference overtakes the rated torque during the transient operation. Then one can see over currents during this time interval.

During steady state operation, phase current shapes are almost sinusoidal with low-level ripples.

VII. CONCLUSION

In this paper, a predictive current control applied to an induction motor has been presented and validated on an
experimental test bench. The fast dynamic performance is proved. A new reduced order high-gain observer is proposed to estimate the rotor fluxes and the inverse rotor time constant in order to compensate some parameter variations. The observer has been validated on simulation. This shows its feasibility and effectiveness. It can be noted that the proposed control requires high performance hardware for real-time implementation. The switching frequency is not fixed. These drawbacks can be suppressed by choosing more than one converter configuration (multi-step predictive current control) in a fixed switching frequency. Further work will be carried out on multi-step PCC with observer implementation on real-time.

REFERENCES


