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Streaming potential and permeability of saturated sandstones under triaxial stress: Consequences for electrotelluric anomalies prior to earthquakes

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Abstract. The streaming potential, due to fluid circulation in rock, was measured on saturated sediments (Fontainebleau sandstones). The electrokinetic coupling coefficient, which is the ratio of the streaming potential and the excess pore pressure, is proportional to the fluid resistivity. Additionally, for a fluid conductivity of 10^{-3} S/m, the electrokinetic coupling coefficient varies from 10 to 6642 mV/0.1 MPa for sample permeability in the range of permeabilities from 0.15×10^{-15} to 1220×10^{-15} m². The different values of the electrokinetic coupling coefficient have been explained by the effect of increasing surface conductivity which becomes nonnegligible compared to fluid conductivity for low permeability. When the sample is deformed under triaxial stress up to failure, the vertical permeability (along the principal stress) drops by about 0.20%/0.1 MPa when failure occurs. The typical variation of the electrokinetic coupling coefficient is a large increase beginning with the onset of the localization of the shear band at about 75% of the yield stress and stopping at the failure. This increase of the electrokinetic coupling coefficient is due to an increase of ζ potential in the shear zone when new surfaces are created and connected. Possible consequences of our results are given concerning the electrical fields which could appear during the preparation of an earthquake. It is shown that in some cases, self-potential anomalies reported in the deformed zone preceding an earthquake occurrence could be due to an increase of the electrokinetic coupling coefficient from 75% of the yield stress to rupture in the vicinity of one of the electrodes. Any variation of fluid resistivity or permeability in the vicinity of one electrode could change the electrokinetic coupling coefficient, inducing a surface electrokinetic potential anomaly. In regard to the interpretation of the electrokinetic effect which occurs at large distance from the epicenter, a larger electrokinetic potential anomaly could be measured between electrodes situated along a vertical fluid flow, for instance, in a shallow borehole. An electrokinetic potential anomaly up to 30 mV, for a fluid conductivity of 0.01 S/m and a rock permeability of 10^{-12} m², could be observed with a change of the underground water table level as slight as 50 cm (50 mbar). Moreover, if the permeability between the electrodes is increased by a factor of 8×10^3 , the electrokinetic coupling coefficient could be enhanced by a factor up to 650.

Introduction

Surface observations of self-potential (SP) anomalies have been reported from numerous tectonically active areas in the world. Electrotelluric precursors to earthquakes appear from a few minutes to several days before the seism and can be observed as far as 300 km from the epicenter, with an intensity ranging from 10 to 100 mV. The correlation of SP anomalies with earthquake occurrences has often been emphasized as a possible means for predicting earthquakes [Mizutani *et al.*, 1976; Corwin and Morrison, 1977; Ishido and Mizutani, 1981; Varotsos and Alexopoulos, 1984a, b].

SP anomalies can be produced by a streaming potential, as a consequence of fluid pressure gradients; by a thermoelectric potential, as a consequence of a temperature gradient; by a chemical potential, as a consequence of a chemical gradient; or by these effects possibly acting together. The

streaming potential effect in the crust may be a promising model to explain low-frequency electric and magnetic precursors to earthquakes. These electrokinetic effects may be produced by fluid percolation in the crust, driven by a pore pressure gradient related to precursory deformation. This model was first proposed by Mizutani *et al.* [1976], who assumed that dilatancy prior to earthquakes [Nur, 1972; Scholz *et al.*, 1973] enhances the permeability of the medium and allows the fluid to flow in the vicinity of the fault. Murakami *et al.* [1984] reported self-potential anomalies associated with an active fault, and anomalous time variations of the self-potential in the fractured zone of an active fault preceding the earthquake occurrence were measured [Miyakoshi, 1986]. Dobrovolsky *et al.* [1989] proposed a long-distance elastic effect inducing the fluid flow and an electrokinetic effect near the electrodes. Bernard [1992] proposed an electrokinetic model based on the triggering of fluid instabilities by strain perturbation. However, the long-distance effects are still controversial, as their observation requires the coincidence of very favorable circumstances to

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take into account a reasonable precursory strain and the fact that no coseismic electrical anomalies are observed. Recently, some evidence of streaming potential has been reported in a study of the electrical effect of the annual variation of the water saturation of rocks in an underground quarry [Morat *et al.*, 1992]. Electrokinetic effects were also proposed to explain the SP anomalies frequently observed in geothermal areas [Corwin and Hoover, 1979], or electrokinetic effects were used to monitor subsurface flow in geotechnical constructions [Merkler *et al.*, 1989].

Surface electrokinetic effects, calculated for several geometries and various pore pressure source distributions, only appear near lateral heterogeneities of conductivity, permeability, or generally of the streaming coupling coefficient C_s , which is the ratio between the electrokinetic potential and the excess pore pressure [Nourbehecht, 1963; Fitterman, 1978, 1979]. The study of this electrokinetic coupling coefficient and its variation prior to earthquakes is therefore essential to quantify electrotelluric effects better. Streaming potentials refer to the electrical signals produced when a fluid flows in a porous medium, and this effect can be quantified through experimental results. Few data of geophysical interest on streaming potential are available [Somasundaran and Kulkarni, 1973; Ishido and Mizutani, 1981; Massenet and Van Ngoc, 1985; Morgan *et al.*, 1989]. These experiments are done on crushed samples or capillaries at atmospheric pressure and could not reflect the behavior of natural rocks. We chose to measure the streaming potential on intact saturated sediments with a large range of permeabilities. As the spatial distribution of anomalies in electrotelluric potentials and geomagnetic variations is partly controlled by relative change in C_s , we must know how C_s is affected prior to an earthquake. Particularly, is the electrokinetic coupling coefficient affected during dilatancy? As the streaming potential is expected to be proportional to the fluid pressure gradient, how is it affected by changes of permeability? The streaming potential coupling coefficient C_s and the permeability have therefore been measured first on a series of undeformed sediments and then during the deformation of samples up to failure.

Electrokinetic Phenomena

Electrokinetic phenomena are due to the existence of an electric double layer formed at the solid/liquid interface. The currently accepted model of the rock/fluid interface is due largely to Stern [1924] [Ishido and Mizutani, 1981; Morgan *et al.*, 1989]. The double layer is made up of a layer of ions (the Helmholtz layer) adsorbed on the surface of the rock and of a diffuse mobile layer (the Gouy-Chapman zone) extending into the liquid phase. Figure 1 depicts the potential distribution: Φ_0 , Φ_h , and ζ are the potentials at distances from the surface of zero, H , and S , respectively. H is the distance to the beginning of the diffuse zone. S is referred to as the shear plane. Under all conditions the double layer as a whole is electrically neutral: the charge of the surface layer C_0 is equal to the sum of the charges in the diffuse zone (C_d) and in the Helmholtz layer (C_h), appropriate charge signs being taken into account.

When a fluid is made to flow through a porous medium, there will be an occurrence of a potential, the so-called streaming potential, across the sample, because of the relative motion between the solid and the liquid. The streaming

Figure 1. Scheme of the electrochemical solid/solution interface. Stern's model: C_0 is the charge density of the rock/fluid surface zone. Φ_0 is the surface potential. H is the plane between diffuse zone and adsorbed ions with a charge density C_h . S is the slipping plane with a corresponding ζ potential. Note that Φ_h and ζ can be positive or negative.

potential is just the reverse of electroosmosis. S is considered to be the closest plane to the surface on which fluid motion takes place. The potential on this plane is defined as the ζ potential, and it is the potential which is manifest in streaming potential measurements.

The Helmholtz-Smoluchowski equation is the relation governing the streaming potentials generated by fluids moving through porous media or capillaries [Overbeek, 1952; Nourbehecht, 1963]. In a porous medium the general relations between the electric current density I (A/m²), the fluid flow J (m/s), and the forces of $\text{grad } V$ and $\text{grad } P$ are

$$-I = \frac{\sigma_f}{FF} \text{grad } V - \frac{\epsilon \zeta}{\eta FF^\circ} \text{grad } P \quad (1)$$

$$-J = -\frac{\epsilon \zeta}{\eta FF^\circ} \text{grad } V + \frac{k}{\eta} \text{grad } P \quad (2)$$

where σ_f and ϵ are the electrical conductivity and the dielectric constant of the fluid, ζ is the zeta potential, η is the dynamic viscosity of the fluid, k is the permeability of the porous medium, FF° is the formation factor ($\sigma_{\text{fluid}}/\sigma_{\text{rock}}$) with a very high fluid conductivity when surface conduction is absent, FF is the formation factor for the fluid conductivity being studied (i.e., possibly with surface conductivity), P is the pressure of the fluid, and V is the potential. The first term on the right-hand side of (1) represents Ohm's law and the second term in (2) represents Darcy's law. In a steady state equilibrium the convection current (due to $\text{grad } P$) is balanced by the conduction current (due to $\text{grad } V$). Equating these currents leads to

$$C_s = \frac{\Delta V}{\Delta P} = \frac{\epsilon \zeta}{\eta \sigma_f} \frac{FF}{FF^\circ} \quad (3)$$

which is the Helmholtz-Smoluchowski equation [Dukhin, 1974].

ΔV is the generated potential and ΔP is the applied pore pressure difference. This equation implies that the currents are of equal magnitude and opposite flow along the same

Figure 2. Nonmagnetic triaxial pressure cell and sample assembly.

path. The ratio $\Delta V/\Delta P$ is called the streaming potential cross-coupling coefficient C_s or simply the coupling coefficient. When surface conductivity is absent, $FF = FF^\circ$, and we have $C_s = \varepsilon\zeta/\eta\sigma_f$. The ratio FF°/FF can be also expressed for a circular cross section pore of radius a as

$$\frac{FF}{FF^\circ} = 1 / \left(1 + \frac{2S_s}{a\sigma_f} \right) \quad (4)$$

where σ_f is the fluid conductivity and S_s is the surface conductance [Morgan *et al.*, 1989]. We can note that the smaller the pore radius is, the greater the surface conductivity is.

Experimental Procedure

High-Pressure Cell

The sample assembly is shown in Figure 2. The samples were cut in cylinders (25 mm in diameter and 50 mm long) and dried at 70°C in vacuum for 8 hours. Then they were saturated with distilled water. The samples were subjected to a gradually increasing deviatoric stress up to failure, with a confining pressure of 10 MPa. The variations of the streaming potential, of resistivity, and of permeability with deformation were measured. Each measurement required 20–40 min to reach a stable state. A typical experiment lasted 8–11 hours. We used a triaxial cell servocontrolled in displacement by an hydraulic press. The entire cell is amagnetic, and the mobile insulating piston is made of alumina and has a central circular hole (Figure 2). The deformation was measured by a displacement sensor. The deformation of the press was not negligible and was taken into account by a calibration. The variations of axial stress, confining pressure, and pore pressure are independent. The sample was isolated from the confining fluid by an insulating jacket. The flow circuit is connected, at both ends of the sample, to an upstream and a downstream reservoir volume, where two sensors monitor the fluid pressure. Different valves allow us to keep the flow circuit open or closed. Air was removed from the flow system. The fluid was made to flow through the sample in the axial direction at each triaxial state of stress in order to measure permeability and electrokinetic potential. The two electrodes are made of beryllium bronze with a hole in the center and two linked circular grooves allowing the

fluid to flow uniformly in the axial direction throughout the sample. The upper and lower electrodes are isolated from the conductive press and the cell by an insulating alumina piston and insulating pastille, respectively (Figure 2). The streaming potential and the resistance of the sample can not be measured at the same time, because the impedance meter disturbs the measurement of the streaming potential. The dielectric constant of the fluid is ε_{H_2O} at temperatures between 17°C and 24°C. The samples used were Fontainebleau sandstones (France), with a wide range of permeabilities. Using replicas method which produces resin casts of the pore space, we observed the porous medium of samples by electron microscope analysis. A resin is used to fill the pores, and the quartz grains are then dissolved with an acid. Different pore features have thus been shown.

Resistivity Measurement

The resistance of the sample was measured by an HP 4284A impedance meter at a frequency of 4 kHz to avoid polarizing the electrodes. The resistance of the different wires and connections is taken into account by the impedance meter. The confining fluid was checked to be nonconductive. The fluid present in the cylindrical hole of the insulating piston and insulating pastille is in contact with the sample and can provide a conduction path outside of the sample. The resistance R_w of this exterior conduction path was measured. The effect of R_w is to give a conduction path between the electrodes that is parallel with the conduction path through the sample. Thus the effective resistance between the electrodes R_m is $1/R_m = (1/R_s) + (1/R_w)$, where R_s is the resistance of the sample. The resistance of the sample, the resistivity of the fluid, and the streaming potential can not be measured simultaneously. During the experiment the resistance of the sample was measured just after the streaming potential measurement. We noted that the resistance of the sample changed when fluid was flowing through it. Fluid in the upstream reservoir has a constant resistivity of $2 \times 10^3 \Omega \text{ m}$ in most of the cases. After flowing through the sample, fluid is usually more conductive, and we assumed that fluid resistivity after flowing through the sample was closer to fluid resistivity in the sample than fluid resistivity in the upstream reservoir. The resistivity ρ_w of the fluid, which has flowed through the sample, was used for the calculation of R_w and was measured out of the cell using a conductivity cell at each triaxial state of stress, as soon as the flow was stopped. This procedure allowed us to consider the resistivity of the sample (ρ_s) and the resistivity of the fluid (ρ_w) approximately equal to those that were present during the streaming potential measurement.

Streaming Potential Measurement

The streaming potential was measured during fluid flow (when permeability is $> 10^{-15} \text{ m}^2$) by an HP 34401A voltmeter with an input resistance above $10^{10} \Omega$. The electrodes and the voltmeter were linked by coaxial wires, and the ground was connected to the press to avoid electrical noise. The lower electrode was connected to the ground of the streaming potential measurement. The resistance of the water in the insulating piston (R_w) is taken into account. Indeed, in this case, electrical current is no longer zero in the sample, and using the definition of electrokinetic coupling coefficient (equation (3)), the measured ΔV is related to the measured ΔP as

$$\frac{\Delta V}{\Delta P} = C_s / \left(1 + \frac{R_s}{R_w} \right). \quad (3')$$

Data were recorded, once per second, by a PC computer with an Institute of Electrical and Electronics Engineers interface. The flow could be reversed to measure the reverse streaming potential. The electrokinetic coupling coefficient was computed from the regression coefficient of five measurements. When permeability was less than 10^{-15} m^2 , the streaming potential was measured during the pressure gradient diffusion.

Permeability Measurement System

Steady state flow method. The flow system was kept open at atmospheric pressure near the downstream reservoir, and the fluid was made to flow through the sample with a manual pump near the upstream reservoir. The pressure gradient ΔP across the sample was kept at a constant value. The rate of fluid flow Q (m^3/s) through the sample was measured during steady state fluid flow. The permeability k is simply given by Darcy's law,

$$Q = (kA\Delta P)/(\eta L), \quad (5)$$

where A is the cross-sectional area of the sample perpendicular to the direction of the flow and L is its length. This method can be used to measure permeabilities greater than 10^{-16} m^2 . In all our experiments the fluid flow Q is proportional to the pressure gradient, and permeability values are computed from the regression coefficient determined from five measurements.

Transient flow method. The flow system is kept closed at the upstream and at the downstream reservoirs. A pressure pulse ΔP_0 (less than 10% the magnitude of the pore fluid pressure) is applied to the fluid reservoir connected to one end of the sample. The pressure gradient decay is then recorded in the fluid reservoirs at both ends of the specimen. *Brace et al.* [1968] analyzed the transient flow method and derived an expression for the pressure gradient as a function of time:

$$\Delta P(t) = \frac{2\Delta P_0 V_2}{V_1 + V_2} e^{-mt}, \quad (6)$$

where V_1 and V_2 are the upstream and downstream reservoir volumes ($V_1 = V_2 = 50 \times 10^{-6} \text{ m}^3$ in our experimental setup, large compared with the sample pore volume). A plot of the decay curve in terms of $\ln(\Delta P(t))$ versus time gives a straight line with a slope m , and the permeability k can be determined by

$$k = (m\eta\beta LV_1 V_2)/[A(V_1 + V_2)] \quad (7)$$

where β is the compressibility of the pore fluid ($0.42 \times 10^{-9} \text{ Pa}^{-1}$). This method can be used to measure permeabilities in the range 10^{-16} m^2 to 10^{-24} m^2 .

Results

We present streaming potential measurements on seven saturated samples of intact Fontainebleau sandstones with a large range of permeabilities.

Figure 3. Example of measurement of streaming potential ΔV during a typical experiment: pressure difference $\Delta P = 0.1 \text{ MPa}$ and fluid resistivity $600 \Omega \text{ m}$. This measurement has been done on sample F313, with permeability $k = 13 \pm 3 \times 10^{-15} \text{ m}^2$, under hydrostatic pressure conditions $p = 11.5 \text{ MPa}$.

Results on Undeformed Sediments

Streaming potential measurements. The streaming potential was first measured when the sample was subjected to a quasi-hydrostatic pressure of about 11.5 MPa: axial stress of $12 \pm 0.5 \text{ MPa}$ and confining pressure of $11 \pm 0.1 \text{ MPa}$. We present a typical measurement of the streaming potential when the permeability of the sample was measured using the steady state flow method (for all our samples except F82) and when the permeability was measured using the transient flow method (for F82). In all our experiments the permeability was measured along the axial stress. The effects of the surface conductivity and of the fluid conductivity on the streaming potential will be discussed. We always observed negative electrokinetic coupling coefficients; the reported values are the absolute values of the electrokinetic coupling coefficients.

A typical streaming potential ΔV at a given pressure difference ΔP is shown in Figure 3 when the permeability is measured by the steady state flow method (sample F313). The streaming potential appears when the pressure difference is applied and still remains as long as the pressure gradient is maintained. The streaming potential drops to zero when the fluid flow is stopped. The sign of the streaming potential changes when the fluid flow is reversed. For this example the resistivity of the fluid was $600 \Omega \text{ m}$. The streaming potential reaches about 300 mV (Figure 3) when the pressure difference is 0.1 MPa, leading to an electrokinetic coupling coefficient C_s of $540 \text{ mV}/0.1 \text{ MPa}$, taking into account the resistance of the fluid in the cylindrical hole of the piston (R_w).

The permeability of sample F82, $k = 0.15 \pm 0.05 \times 10^{-15} \text{ m}^2$, was measured by the transient flow method. In this case the streaming potential was measured during the pressure gradient diffusion (Figures 4a and 4b). The fluid pressure before the pressure pulse was 10.03 MPa. The fluid resistivity was $1250 \Omega \text{ m}$ for this example. The potential

Figure 4. (a) Pressure gradient diffusion as a function of time: $\Delta P(t)$ during the transient flow method. (top) Behavior of pore pressure at the end of the sample where ΔP is applied. (bottom) Behavior of pore pressure at the other end of the sample. (b) Evolution of the streaming potential during this diffusion of pressure gradient $\Delta V(t)$. These measurements have been done on F82 in hydrostatic pressure conditions $p = 11.5$ MPa, permeability $k = 0.15 \pm 0.05 \times 10^{-15} \text{ m}^2$, fluid resistivity $\rho_f = 1250 \text{ m}$.

changes from -65 to 24 mV (Figure 4b) when the pressure pulse is applied by increasing the pore pressure from 10.03 to 10.68 MPa (Figure 4a). This leads to a C_s of $13.7 \text{ mV}/0.1 \text{ MPa}$ (the resistance of the fluid in the cylindrical hole of the piston (R_w) was very large compared to the sample resistance). The evolution of the streaming potential with time is

$$\Delta V(t) = \frac{1}{\sigma_f} \int_{x_1}^{x_2} i_{\text{conv}}(t) dx \quad (8)$$

with $i_{\text{conv}}(t) = \sigma_f C_s \partial P(t) / \partial x$, where $x_2 - x_1$ is the length of the sample. If we assume that C_s is constant, then $\Delta V(t) = C_s \Delta P(t)$, the pressure gradient being constant along its length, although it varies with time [Brace *et al.*, 1968]. A typical measurement (Figures 4a and 4b) shows that ΔV decreases more rapidly than ΔP . A possible interpretation is that the electrokinetic coupling coefficient is not exactly constant during the experiment. It seems that there is no threshold of pressure gradient to produce a streaming potential, the measurement being possible if the signal is greater than the noise.

Effect of surface conductivity. To estimate the contribution of the surface conductivity, we measured the conductivity of the sample F313 ($k = 13 \pm 3 \times 10^{-15} \text{ m}^2$ during the entire experiment) as a function of fluid conductivity with different NaCl concentrations. The resistance of the sample was measured as soon as the flow was terminated. The conductivity of the sample as a function of fluid conductivity is shown in Figure 5.

The results lead to $FF^0 = 91$ when fluid conductivity is larger than $2 \times 10^{-3} \text{ S/m}$. For fluid conductivity below $\sigma_f = 2 \times 10^{-3} \text{ S/m}$ the conductivity of the sample is no longer proportional to the fluid conductivity. Our measurements are usually done with $\sigma_f = 10^{-3} \text{ S/m}$ and $FF = 61$, and we would have to multiply the "apparent" ζ potential by 1.5 if we wanted to have the "true" value of ζ for this sample (equation (3)).

The surface conductivity is the limit of the conductivity of the sample when fluid conductivity becomes very low. With the lowest fluid conductivity used in our measurements (Figure 5) being 10^{-3} S/m , the conductivity of the sample with this fluid allows us to overvalue the surface conductance: $S_s = 10^{-7} \Omega^{-1}$. For sandstones the pore radius is expected to be equal to 10^{-5} m . Then $2S_s/a = 2 \times 10^{-2} \text{ S/m}$ is larger than the fluid conductivity $\sigma_f = 10^{-3} \text{ S/m}$ for this sample, and the surface conductivity term is the major contributor to the streaming potential.

Effect of fluid conductivity. We measured C_s with different NaCl concentrations (Figure 6) with $pH = 5$ on the same sample F313. Different pore fluids were made to flow

Figure 5. Rock conductivity versus fluid conductivity measured on sample F313 in hydrostatic pressure conditions $p = 11.5$ MPa.

Figure 6. Electrokinetic coupling coefficient as a function of fluid resistivity for sample F313 in hydrostatic pressure conditions $p = 11.5$ MPa.

through the sample from the most resistive to the most conductive fluid, waiting to reach a constant fluid resistivity out of the cell at each measurement of the streaming potential. We observed electrical instabilities when fluid conductivity was higher than 10^{-2} S/m. The electrokinetic potential was no longer constant when pore pressure difference was constant and abnormal variations at higher frequency up to 50% of the signal were observed. We used distilled water to avoid these electrical instabilities. The high fluid resistivity used enhances the chemical reactions between the matrix and the fluid. Changes in fluid resistivity when the fluid was made to flow through the sample were noted outside the cell, particularly before the failure. These changes resulted from the interaction between the rock and the fluid, and this interaction was dependent on deformation and cracking. The coupling coefficient was found to be proportional to the resistivity of the fluid which allowed us to compute electrokinetic coupling coefficients at a given fluid conductivity. As ϵ and η are constant, we can deduce that the ζ potential is constant, in first approximation, with different salinities of fluid. Notice that for pure quartz $\zeta = -2.8 \times 10^{-2}$ to $2.5 \times 10^{-2} \log_{10} \rho_f$, it means $\zeta = -100$ mV for a fluid resistivity of $10^3 \Omega \cdot m$ and $\zeta = -50$ mV for a fluid resistivity of $10 \Omega \cdot m$ [Pride and Morgan, 1991]. Moreover, Ishido and Mizutani [1981] found that ζ potential was dependant upon chemistry of the pore fluid. Nevertheless, it seems that ζ potential is constant with different conductivities for this sample and in this range of fluid conductivity. The linear dependence of the streaming potential versus the pressure gradient shows that (3) is verified with the term $FF/(\sigma_f FF^\infty)$ constant.

Relation between the streaming potential, fluid flow, and permeability. The relation between the streaming potential and the driving pressure, at a stress of about 11.5 MPa, was examined first and is shown in Figure 7. For sample F82 the slope of the straight line results from 10 measurements of pressure gradients and streaming potentials by the transient flow method, in the range 0.12–0.80 MPa. The slopes of the straight lines for the other samples result from five to seven measures by the steady state flow method. The various

Figure 7. Streaming potential ΔV measurements with different applied driving pore pressures ΔP , on seven samples, in hydrostatic pressure conditions $p = 11.5$ MPa. Permeabilities range from $0.15 \pm 0.05 \times 10^{-15}$ to $1220 \pm 30 \times 10^{-15} \text{ m}^2$, corrected for a constant fluid resistivity $\rho_f = 10^3 \Omega \cdot m$. The streaming potential is proportional to the driving pore pressure. The electrokinetic coupling coefficient $\Delta V/\Delta P$ (in absolute value) varies from 10 ± 1 to 6642 ± 611 mV/0.1 MPa.

coupling coefficients were not measured with exactly the same fluid resistivity. As the coupling coefficients are proportional to the fluid resistivity, in first approximation they can be computed at a fixed fluid conductivity and then compared (Figure 7). There is a linear relation between the streaming potential and the driving pressure. It means that for a given sample the streaming potential is proportional to the flow rate of fluid. The coupling coefficient C_s , reported for a water resistivity of $10^3 \Omega \cdot m$, varies from 10 ± 1 to 6642 ± 611 mV/0.1 MPa.

For various samples (with $\epsilon = 7.04\text{--}7.18 \times 10^{-10}$ F/m, $\eta = 0.951\text{--}1.049$ mPa s, $\sigma_f = 10^{-3}$ S/m), large values of the streaming coupling coefficient are obtained for large permeabilities (Figures 7 and 8a). The streaming coupling coefficient shows a linear variation with permeability on log-log coordinates with a slope of 0.7 (Figure 8a). The different values observed for the coupling coefficient could be produced by the ζ potential variations. But the ζ potential is expected to be of the same order of magnitude for all these Fontainebleau sandstones because the mineralogy is nearly identical. The apparent dependence of the coupling coefficient on permeability could be mainly due to the surface conduction effect, as the smaller the permeability is, the smaller the pore sizes in sandstones are expected to be. If surface conductivity is enhanced by smaller permeabilities, the conduction current tends to increase. As the conduction current equilibrates the convection current (which is constant), the electrical gradient tends to decrease, and the streaming coupling coefficient is decreased. This study has shown, using replicas method, different porous features reported in Table 1. These samples do not contain clay and have comparable size quartz grains ranging between 100 and 300 μm . Moreover, it has been shown that the surface conductivity for sample F313 ($k = 13 \pm 3 \times 10^{-15} \text{ m}^2$) is not negligible compared with the fluid conductivity. In order

Figure 8. (a) Streaming coupling coefficient as a function of permeability. (b) Relation between the streaming potential and permeability at a constant fluid flow $Q = 10^{-7} \text{ m}^3/\text{s}$, calculated (solid line) with $\zeta = -21.9 \text{ mV}$, fluid conductivity $\sigma_f = 10^{-3} \text{ S/m}$, or measured (rectangles) for different samples.

to know the exact effect of surface conductivity and the corrected ζ potential, the rock conductivity as a function of the fluid conductivity should be measured for each sample, which is beyond the scope of this paper. Our purpose is not to calculate the exact value of ζ potential for each sample but to know how the coupling coefficient varies with permeability. The coupling coefficient varies when the permeability changes as shown in Table 1 and in Figures 7 and 8a. The effect of surface conductivity has been quantified using a capillary model to express surface conductivity as a function of surface conductance and hydraulic radius. Then hydraulic radius has been related to permeability using Carman-Kozeny's law and computed values of streaming coupling coefficient are a good approximation of measured values.

We can deduce from (3) and (5) the relation between the streaming potential, the fluid flow, and the permeability [Jouniaux and Pozzi, 1995]:

$$\Delta V = \frac{L \varepsilon \zeta Q F F^\circ}{A \sigma_f k F F^\circ} \quad (9)$$

Table 1. Porosity, Permeability, and Electrokinetic Coupling Coefficient on Undeformed Sandstones

	Porosity, %	Permeability, $\times 10^{-15} \text{ m}^2$	Electrokinetic Coupling Coefficient, mV/0.1 MPa
F82	4.3*	0.15 ± 0.05	10 ± 1
F17		4.9 ± 1.2	65 ± 5
F01		86 ± 2	310 ± 24
F44	13	287 ± 7	661 ± 53
F9IY	9.9†	180 ± 4	1166 ± 93
FK5	10	250 ± 5	4002 ± 320
F2	20‡	1220 ± 30	6642 ± 611

With a fluid resistivity of $10^3 \Omega \text{ m}$.

*Pore size 5–15 μm grain boundary porosity, important cementation.

†Pore size 10–30 μm grain boundary porosity, no cementation.

‡Pore size 30–50 μm large pores connected between poorly cemented grains.

The streaming potential ΔV increases if permeability decreases for a given fluid flow Q (the parameters L , A , ε , σ_f , and FF/FF° being constant), considering ζ constant. The dependence of ΔV at $Q = 10^{-7} \text{ m}^3/\text{s}$ and $\sigma_f = 10^{-3} \text{ S/m}$ with permeability k is shown in Figure 8b. The streaming potential ΔV shows a linear variation versus permeability on log-log coordinates of -0.18 slope with an average value of ζ of -21.9 mV (solid line). The difference between measurements (rectangles) and calculated variation (solid line) could be due to the different effects of surface conductivity, as explained above. The streaming potential is proportional to the fluid flow Q (with L , A , ε , ζ , σ_f , and FF/FF° constant) at a given permeability k , according to (9). We calculated the Darcian speed Q/A corresponding to the pore pressure gradient of $\Delta P = 0.1 \text{ MPa}$ for two samples. The samples F82 and F2 have a permeability of $0.15 \pm 0.5 \times 10^{-15} \text{ m}^2$ and $1220 \pm 30 \times 10^{-15} \text{ m}^2$, respectively. The deduced Darcian speed is 9.1 m/yr for F82 and 215 m/d for F2 which is higher than Darcian speeds in many geophysical contexts. The streaming potential as a function of Darcian speed depends on sample size, and we will not use this expression to predict the observed SP in the field. Note that electrokinetic coupling coefficient is independent of sample size and can be used for field measurements interpretation.

Results on Deformed Sediments

We present the behavior of the electrokinetic coupling coefficient and of permeability with deformation for three samples of Fontainebleau sandstones: F44, FK5, and F9IY. We first present the mechanical behavior, then the behavior of the electrokinetic coupling coefficient with deformation, and finally the behavior of permeability with deformation. The different features of the samples are reported in Tables 2 and 3. The effects of the deformation on these parameters for the three samples will be discussed, and we will try to explain the common features of the behavior of electrical properties and of permeability with deformation.

Mechanical behavior. The stress-strain curves for the samples F44, FK5, and F9IY are represented in Figures 9a, 9b, and 9c, respectively. The samples were subjected to an

Table 2. Principal Mechanical Features of the Samples F44, FK5, and F9IY

	Strain Rate, s^{-1}	Yield Stress, MPa	Deformation at Yield Stress, %	E , MPa
F44	9.5×10^{-7}	235	1.72	21,330
FK5	8.3×10^{-7}	260	1.52	28,870
F9IY	8.1×10^{-7}	249	1.50	27,450

E is the Young's modulus.

increasing hydrostatic pressure up to 10 MPa (point A). Then the axial pressure was gradually increased with a constant confining pressure of 10 ± 0.1 MPa. The average strain rate was between 8 and $9.5 \times 10^{-7} s^{-1}$. Failure occurred at a yield stress of about 250 MPa (point D). Young's modulus E , computed on the linear part of the curve, is between 21,000 and 29,000 MPa (Table 1).

Behavior of electrical properties with deformation. Previous studies on the same samples showed that electrical resistivity of the sample increases up to point C, which corresponds to 47%, 39%, and 40% of the yield stress for F44, FK5, and F9IY, respectively, and then decreases from point C to point D [Jouniaux *et al.*, 1992].

The variation of the coupling coefficient $\Delta V/\Delta P$, reported for a fluid resistivity of $10^3 \Omega m$, during the deformation of the samples F44, FK5, and F9IY is represented in Figures 10a, 10b, and 10c, respectively. The coupling coefficient decreases from point C to point L by 15.8% for F44, 45.2% for FK5, and 52% for F9IY. The coupling coefficient increases from point L to point D with a rate of 0.07–0.19%/0.1 MPa. The minimum value of the coupling coefficient, noted by point L, is obtained for a stress of 72–86% of the yield stress (Table 2).

Behavior of permeability with deformation. The permeability of the samples F44, FK5, and F9IY was measured by the steady state flow method, and its behavior with deformation is represented in Figures 11a, 11b, and 11c, respectively. First, the vertical permeability decreases (up to point C) by 0.007%/0.1 MPa, 0.013%/0.1 MPa, and 0.027%/0.1 MPa for F44, FK5, and F9IY (Figures 11a, 11b, and 11c). Then the permeability is changed by 0.0045%/0.1 MPa, –0.011%/0.1 MPa, and –0.014%/0.1 MPa for F44, FK5, and F9IY, respectively. Permeability dropped when failure occurred, with a rate of 0.017–0.020%/0.1 MPa (Table 3).

Discussion

Behavior of the Rock Resistivity with Deformation

Changes in the fluid resistivity for fluid that has flowed through the sample result from interaction between the rock and the fluid. Resistivity of the fluid often decreases from 50% of yield stress up to failure [Jouniaux, 1994]. A whiteish water was even sometimes observed just before the failure, denoting fine particles drained from the matrix. This effect can drastically affect the resistivity of the fluid up to 57% in some cases. These interactions are enhanced by our particular procedure of using a drained sample which is necessary to perform measurements of the streaming potential and of the permeability.

Variations of the sample resistivity are partly due to changes of the fluid resistivity. However, changes of the sample resistivity are mainly due to the closure of pores and subhorizontal microcracks (up to point C) and to the aperture of subvertical microcracks at the onset of dilatancy (from point C to point D) [Brace and Orange, 1968; Brace, 1975]. Indeed, the principal stress is always the vertical stress, and the increase of the deviatoric stress during the deformation induces the aperture of microcracks in the direction of the vertical stress. As a result the evolution of sample resistivity is the same in all our experiments, showing an increase up to point C and a decrease till the failure, although the magnitude of changes in fluid resistivity may be different [Jouniaux *et al.*, 1992; Jouniaux, 1994].

Studies done on Fontainebleau sandstones have shown brittle behavior [Darve, 1992] and an important dilatancy occurring at about 65% of the yield stress when the confining pressure is 10 MPa [Kondo *et al.*, 1991]. Point C, denoting the maximum resistivity of the rock during the deformation, occurs at 40–50% of the yield stress. These results are consistent with those of Brace and Orange [1968], who showed that maximum resistivity could occur before dilatancy detection.

Behavior of Permeability With Deformation

The changes of permeability are not similar for the three samples (Figures 11a, 11b, and 11c). At the beginning of the experiment, there is a path for the vertical fluid flow. First, the closure of pores and subhorizontal microcracks (up to point C) decreases the vertical permeability (Figures 11a, 11b, and 11c). Then the aperture of subvertical microcracks (from point C to point D) changes the permeability by increasing or decreasing it a little. The opened subvertical microcracks (after point C) do not strongly affect permeabil-

Table 3. Principal Features of the Behavior of Permeability and Electrokinetic Coupling Coefficient With Deformation

	Point A, $k \times 10^{-13}$ m^2	Point A C_s , mV/0.1 MPa	Point C, Percent of Failure	Point L, Percent of Failure	Increase Rate of C_s per 0.1 MPa From L to D, %	Decrease Rate of k at Failure per 0.1 MPa, %
F44	3.08 ± 0.08	531 ± 42	47	72	0.07	0.017
FK5	2.48 ± 0.06	4997 ± 399	39	86	0.13	0.020
F9IY	1.77 ± 0.04	1147 ± 92	40	73	0.19	0.020

Points A, C, L, and D refer to stress-strain curves given in Figures 9a, 9b, and 9c for samples F44, FK5, and F9IY, respectively. Increase rate of C_s and decrease rate of k are given for 0.1-MPa change in axial stress.

Figure 9. Axial stress-strain curve from triaxial deformation experiment to failure using a servocontrolled press in displacement. A indicates the point where samples were subjected to an increasing hydrostatic pressure up to 10 MPa, C indicates the point of maximum resistivity, L indicates the point of minimum electrokinetic coupling coefficient, D indicates the point of failure, E indicates Young's modulus computation point, F indicates the end of the first part of the weakening state, and percentages indicate percentages of strength. (a) Results for F44. (b) Results for FK5. (c) Results for F9IY.

Figure 10. Variation in electrokinetic coupling coefficient (in absolute value) with the axial strain from triaxial deformation experiment to failure. A indicates the point where samples were subjected to an increasing hydrostatic pressure up to 10 MPa, C indicates the point of maximum resistivity, L indicates the point of minimum electrokinetic coupling coefficient, D indicates the point of failure, F indicates the end of the first part of the weakening state, and percentages indicate percentages of strength. (a) Results for F44. (b) Results for FK5. (c) Results for F9IY.

ity, showing that they are not connected. The confining pressure is kept at a constant value (10 MPa) during the experiment to measure permeabilities at the same effective pressure (confining pressure minus pore pressure), as permeability depends on the effective pressure [Brace, 1980]. When failure occurs, the confining pressure often increases by about 1.5–5 MPa. Permeability is then measured when the confining pressure is restored to 10 MPa. Hence the drop of permeability is due to the failure and not to an increase of the effective pressure. In all our experiments a drop in permeability is observed when failure occurs. This drop of permeability at failure is about 0.020%/0.1 MPa. The grain sizes are reduced during the deformation. At the end of the experiment the connections between the main microcracks, used for the fluid flow, are probably filled with finely crushed particles, inducing the sealing of the main microcracks and preventing the fluid from flowing easily through the sample. Nevertheless, the permeability is not changed by a factor higher than 3 during the entire deformation.

Behavior of the Electrokinetic Coupling Coefficient with Deformation

A general trend of the behavior of the coupling coefficient is noticeable from point C to failure (point D). Changes in the electrokinetic coupling coefficient are not similar to changes of permeability. Hence the evolution of the electrokinetic coupling coefficient is not related to changes of the permeability (Figures 10 and 11). Our measurements do not allow us to quantify the pore sizes related to the permeability measured during the deformation. We can not estimate the behavior of the surface conductivity during the deformation. The important variation of the electrokinetic coupling coefficient (reported at a constant fluid conductivity) with deformation results in a decrease from point C to point L and an increase from point L to failure (point D) (Figures 10a, 10b, and 10c). Point L, representing 72–86% of the yield stress, may correspond to the onset of the localization of the shear band (it is the growth and the propagation of cracks in an area in which a rearrangement of the grains is observed), and this area will be the way for the future failure. This localization of failure is known to occur after the onset of dilatancy and before failure [Berthaud, 1993]. The important increase of the electrokinetic coupling coefficient from the localization of failure (point L) to failure (point D) is thought to be due to an increase of ζ potential in the shear band where new surfaces are created and connected. The ζ potential is enhanced in the shear zone, and the increase of the electrokinetic coupling coefficient is measured at the sample scale when new cracks are connected (point L) allowing fluid to flow through these new cracks. Also, the creation of a shear zone makes the sample macroscopically heteroge-

Figure 11. (opposite) Variation of permeability with axial strain from triaxial deformation experiment to failure. A indicates the point where samples were subjected to an increasing hydrostatic pressure up to 10 MPa, C indicates the point of maximum resistivity, L indicates the point of minimum electrokinetic coupling coefficient, D indicates the point of failure, F indicates the end of the first part of the weakening state, and percentages indicate percentages of strength. (a) Results for F44. (b) Results for FK5. (c) Results for F9IY.

neous. Charge separations may occur across the shear band in addition to the charge buildups at the ends of the sample.

Possible Consequences for Field Measurements

The major purpose of our study has been to measure representative values of the electrokinetic coupling coefficient under various conditions relevant to geophysical problems. We now give the possible consequences of our results for field measurements. The electrokinetic field due to fluid circulation can be measured horizontally by electrodes on the ground surface or vertically by electrodes buried at different depths.

Surface electrokinetic and magnetic anomalies have been computed in a layered Earth [Fitterman, 1978] and in a faulted half-space [Fitterman, 1979]. It has been shown that a boundary separating regions with different electrokinetic coupling coefficients, with a pressure in excess of hydrostatic at the electrokinetic coupling coefficient boundary, is required to develop a surface self-potential field due to subsurface fluid flow [Nourbehecht, 1963; Fitterman, 1979]. Moreover, these electrokinetic effects are proportional to $(C_1 - C_2)P$, where C_1 and C_2 are the electrokinetic coupling coefficients in region 1 and 2, respectively, and P is any pressure in excess of hydrostatic at the electrokinetic coupling coefficient boundary. Therefore these electrokinetic effects are changed if $(C_1 - C_2)$ or P is changed, leading to an electrokinetic potential anomaly.

In order to estimate changes of the difference between the electrokinetic coupling coefficients prior to an earthquake, we have to know the geophysical parameters influencing the electrokinetic coupling coefficient, especially those which could change during the mechanical process of preparation of an earthquake. Figure 12 shows the following (in absolute value). C is proportional to the fluid resistivity, as shown in Figure 6. C is inversely proportional to the fluid viscosity and depends thus on the fluid temperature and on the fluid nature. C is proportional to the ζ potential and depends on the nature of the rock and of the pore fluid chemistry. C decreases under the effect of the surface conductivity therefore by small pore sizes. C is thus lowered by low permeability and is enhanced by high permeability, as shown in Figure 7. C can increase by a factor up to 650 if permeability increases by a factor 8×10^3 . C depends on the applied deformation, especially between about 75% of the yield stress and the failure, as shown in (Figures 10a, 10b, and 10c).

We will try to give some applications of the effects of these parameters, especially during the preparation of an earthquake, first in order to measure surface self-potential anomalies in the deformed zone, then to measure these anomalies at large distances from the epicenter.

Measurement of Electrokinetic Potential Anomalies in Deformed Zone

Dilatancy is commonly assumed to occur prior to an earthquake in the vicinity of the fault, allowing fluid flow variations through the fault and acting as the boundary of the heterogeneity and its vicinity, one side acting as region 1, the other as region 2 (Figure 13a). The permeability could be enhanced and the electrokinetic coupling coefficient would increase, as the effect of surface conductivity would decrease. The deformation itself could change the rock/fluid

Figure 12. Schematic review of the physical parameters which have an influence on the electrokinetic coupling coefficient.

interaction. For instance, C could increase between about 75% of the yield stress and the failure at a rate up to 0.19% for 0.1 MPa of axial stress (Figures 10a, 10b, and 10c), using the effect of deformation on the electrokinetic coupling coefficient measured in our laboratory experiments. In order to measure the maximum of surface electrokinetic anomaly, it will be more convenient to measure the SP anomalies between an electrode buried where C is not changed, and an electrode near the site where a change of permeability is expected, dilatancy is expected, or a change of fluid conductivity is expected, assuming there is a fluid circulation through the fault separating the electrodes.

Miyakoshi [1986] reported SP anomalies at 3.2 km from the epicenter preceding an earthquake of $M = 5.6$, about 40 days and also 55 hours before the earthquake occurrence. The anomaly returned with the onset of the earthquake, reaching the initial level after 13 hours. The electrodes were fixed in an underground observation tunnel, and the maximum of the anomaly was 40 mV. He concluded that the anomaly was due to the change of the SP of the fractured fault rock in which one electrode was fixed, the other electrode being at a constant potential serving as a reference. Fluid was flowing through the Yamasaki fault, but this anomaly was not attributed to changes in the water migration through the fault on the basis of the time constant of the anomaly. Our measurements show that another interpretation can be proposed: the electrokinetic coupling coefficient of the rock near the electrode could be changed before the earthquake between about 75% of the yield stress and the rupture in the seismic zone. As the second electrode has

Figure 13. (a) Schematic view of fluid circulation and of lateral heterogeneity of electrokinetic coupling coefficient (C_1 and C_2) in the vicinity of a fault. (b) Schematic view of vertical fluid flow and lateral heterogeneity of electrokinetic coupling coefficient (C_1 and C_2) at large distances from the epicenter. V_1 and V_2 are the measured electric potentials. (c) Schematic view of vertical fluid flow at large distances from the epicenter, without lateral heterogeneity of electrokinetic coupling coefficient (C). V_1 and V_2 are the measured electric potentials.

shown a constant self-potential, one can suppose that it was buried in a rock with a constant coupling coefficient. Therefore the difference of the coupling coefficient could become greater, leading to an electrokinetic potential anomaly.

Measurement of Electrokinetic Anomalies at Large Distance From the Epicenter

Anomalies observed at large distances from the epicenter need a different interpretation. Indeed, electrokinetic currents produced in the deformed zone are expected to decrease very rapidly with the distance [Bernard, 1992]. Abrupt upheaval of underground water level is a phenomenon frequently observed postseismically. Large abnormal increases in water flow have been measured in springs and wells, beginning a few days after the seism, especially in major normal fault earthquakes, lasting 6–12 months, and observable at distances of the order of 50 km from the epicenter. Expelled water volumes were 0.2–0.5 km³ for the two earthquakes studied by Muir-Wood and King [1993] of magnitude 7 and 7.3. The mechanism of such a water expulsion is still controversial, but we can assume that there is ground-

water recharge during interseismic periods using the same mechanism. This recharge implies vertical fluid flows in shallow aquifers which could induce electrokinetic anomalies.

These anomalies will be detected at the surface, only if there is a lateral heterogeneity of the values of the electrokinetic coupling coefficient (Figure 13b). Electrokinetic potential anomalies will be proportional to vertical driving pore pressure. Hence any change of the vertical fluid flow could be detected prior to earthquakes. We must notice here that these surface measurements involve nonsaturated medium, and any computation and modeling in this case is beyond the scope of this paper.

Far from the epicenter when variations of the vertical fluid flow exist, the maximum of the electrokinetic effect will be measured between electrodes situated along the flow direction. In this case we assume that the ground is saturated. Thus the measurements will be similar to those made in the laboratory, and a lateral heterogeneity of the electrokinetic coupling coefficient is not needed (Figure 13c). The electric potential difference ΔV will be directly proportional to the vertical driving pore pressure, as shown in Figure 7, using the effect of permeability on the electrokinetic coupling coefficient measured in our particular laboratory experiments. Therefore an electrokinetic potential anomaly will be measured whenever the following occur. (1) The driving pore pressure is changed (equation (4)). Our measurements show that a streaming potential up to 30 mV, for a fluid conductivity of 0.01 S/m and a permeability of 10^{-12} m², could be produced by an underground water level change of 50 cm. Moreover, the streaming potential measurements could indicate when the water level change reverses, as the sign of the streaming potential will be reversed. (2) Fluid resistivity is changed, as the streaming potential is proportional to the fluid resistivity, assuming the driving pore pressure remains constant (4). (3) Permeability between the two electrodes is changed, inducing a different effect of surface conductivity (equation (4)). Our measurements show that if the permeability between the electrodes is increased by an amount of 8×10^3 , the streaming potential could be enhanced by a factor of 650 (Figure 7), assuming that the driving pore pressure remains constant.

Conclusion

Streaming potential was measured along the direction of fluid flow on saturated samples of intact Fontainebleau sandstones. Streaming potential ΔV is proportional to the driving pore pressure ΔP . For a fixed driving pore pressure, streaming potential is proportional to the fluid resistivity. Electrokinetic coupling coefficient varies from 10 to 6642 mV/0.1 MPa when permeability changes from 0.15×10^{-15} to 1220×10^{-15} m². This has been explained by the effect of surface conductivity which is not negligible compared with fluid conductivity when the permeability is reduced.

When the sample is deformed under triaxial stress up to failure, permeability is changed at the most by a factor 3. The electrokinetic coupling coefficient $\Delta V/\Delta P$ reported for a constant fluid conductivity of 10^{-3} S/m increases from the localization of the shear band up to failure. This increase of the electrokinetic coupling coefficient just before failure is due to an increase of ζ potential in the shear zone when new surfaces are created and connected.

Possible consequences of our results to investigate the

electric field which could appear during the preparation of an earthquake have been given. Self-potential anomalies observed in the deformed zone could be due to a large increase of the electrokinetic coupling coefficient from 75% of the yield stress to rupture. Far from the epicenter when variations of the vertical fluid flow exist in relation to an earthquake our measurements show that a vertical streaming potential of up to 30 mV could be induced by an underground water level change of 50 cm (for fluid conductivity 0.01 S/m and permeability 10^{-12} m²). As shown in this paper, the streaming potential is strongly dependent on the permeability. An increase of 8×10^3 in permeability would enhance streaming potential by a factor of 650. This result could explain the strong influence of the site on the intensity of seismo-electrical signals.

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