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CREEP BEHAVIOR OF ZIRCONIA FOAMS USED IN ELECTRICAL FURNACES
(2100 K - AIR)

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Abstracts - Some zirconia foams are used as heating element in electrical furnaces. Their creep behaviour has been investigated at high temperature and under low stress. Important visco-elastic behaviour has been observed. It is likely due to recrystallization, which is sensitive to the tetragonal-cubic phase transition and to the stress.

I - INTRODUCTION

Porous and dense zirconia based ceramics have been used for several years as heating element in electrical furnace /1/. The so-called zirconia furnace can be operated in air at 2100 K, for long periods. The aim of the present study is to investigate the creep behaviour of some new zirconia porous ceramics, such as zirconia foams (1) which are suitable as heating element. During the seventies, large grain dense ceramics (called ZGM) were used. More recently, porous ceramics made in Japan were preferred according to their thermal shock resistance, but their rough and inhomogeneous microstructure enhanced their brittleness. New materials were made by foam processing. They are much more homogeneous. The porosity lies in the range 0.25 - 0.71, so that it is very convenient to choose the electrical resistance and the thermal conductivity of the different parts of the heater (usually, three parts).

II - ELECTRICAL RESISTANCE

First of all, the electrical resistance of the zirconia foams was measured to check that they can be used as heater. The sample was an hollow cylinder: 20 mm inner

(1) Produced by Céramiques Techniques Desmarquest.
diameter, 31 mm outer diameter, 46.5 mm length. It was heated by a.c. current, and it has the same behaviour as a heater in the furnace. By this way one obtains the electrical resistance, or at least an average resistivity. The temperature is not uniform through a section of the sample, the temperature gradient can reach 180 K between the inner and the outer surface.

The figure 1 shows the experimental data. The activation energy is 1.2 eV, which is in good agreement with known values /2/. The electrical resistance roughly increases as the porosity increases from 0.29 to 0.71. Compared to the dense zirconia previously used, the electrical properties of the foams are suitable.

The application of zirconia foams in electrical furnaces involves the high temperature - low stress creep behaviour, in the temperature range 1500 - 2100 K, and at stress level lower than 2.0 MPa.

The creep curves show transient creep followed by stationary creep. Figure 2a shows the stationary creep rate as a function of the stress, at 1773 K for the samples A. It is likely stress power law, with the exponent n = 1.75 to 2.0. In figure 2b are given the data for sample B, between 1850 and 1950 K, a lower value

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**Fig. 1** - Electrical resistance of three zirconia foams (samples A).

### III - CREEP MEASUREMENT

Compression creep has been investigated at fixed temperature under constant stress. The sample sizes were 8 mm diameter, 15 mm height. The composition and porosity are given in Table I.

**Table I** - Sample details.

<table>
<thead>
<tr>
<th></th>
<th>Chemical composition, weight %</th>
<th>Porosity, %</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>ZrO₂</td>
<td>CaO</td>
</tr>
<tr>
<td>A1</td>
<td>91</td>
<td>3.9</td>
</tr>
<tr>
<td>A2</td>
<td>91</td>
<td>3.9</td>
</tr>
<tr>
<td>A3</td>
<td>91</td>
<td>3.9</td>
</tr>
<tr>
<td>B1</td>
<td>91</td>
<td>4.3</td>
</tr>
</tbody>
</table>

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of $n = 1.3$ is found. We should note that the precision of the stationnary creep rate data is rather low, due to the influence of the transient creep and some visco-elastic behaviour which is observed, as described in the following section. The value of $n$ indicates that the creep can be controlled by diffusion and grain sliding. A very important grain sliding is observed on the creep fractured samples. This is not surprising since the porosity is high. As a comparison, creep data of ZGM are given on figure 2. The zirconia foams exhibit higher creep resistance than the dense ZGM, in which there is probably a larger amount of silica.

![Stationary creep rate as a function of stress](image1)

(a) samples A, at 1773 K. (b) sample B, between 1850 and 1950 K. Creep rate of ZGM is given as a comparison.

On figure 3 are plotted the creep rate versus temperature at a stress equal to 1.0 MPa. An activation energy of around 180 kcal/mole is found, which is larger than the value found for dense zirconia.

![Arrhenius plot of the stationary creep rate](image2)

Fig. 3 - Arrhenius plot of the stationary creep rate.

![Visco-elastic behavior of sample A2 under cyclic stress.](image3)

Upper: stress versus time, Lower: strain versus time.

Fig. 4 - Visco-elastic behavior of sample A2 under cyclic stress.
IV - VISCO-ELASTIC BEHAVIOUR

At high temperature, for instance between 1750 and 1950 K, the zirconia foams exhibit a visco-elastic behaviour with very large strain. The same behaviour has been observed in dense ZGM samples above 1600 K. Figure 4 illustrates such a typical behaviour, under cyclic stress at 1973 K. The sample was already strained at $1.8 \times 10^{-7}$. Under load there is a transient creep, and when the sample is unloaded it appears a very important visco-elastic effect. The test was stopped because the last loading showed a tertiary creep, however the next unloading does not show a large permanent strain. The time constant of the effect is large: 1 to 10 minutes, and it is of the same order of magnitude than the last of the preceding creep. The visco-elastic behaviour appears more or less each time the stress value changes. The figure 5 gives an other illustration. In phase I, a transient creep is observed, followed by a stationary creep, more or less visible. In phase II, the stress was increased, no transient creep is seen. In phase III, a visco-elastic effect appears, as a creep rate which is zero at first and which increases to the stationary creep rate corresponding to the value of the stress. In phase IV, the stress is very low and the same behaviour as described before is observed. In phase V, the transient creep is seen again.

![Figure 5 - Creep curve and visco-elastic effects depending of loading and unloading.](image)

V - DISCUSSION

The temperature range at which the creep was studied corresponds to operating temperature of the zirconia furnace. This is the two-phase domain of the 4 w% calcia-zirconia (tetragonal-cubic). The microstructure of crept and uncrept samples were observed (figures 6a, b, c and d).

After tertiary creep a large number of cracks appears (see figures 6a and b). All the cracks are filled by small crystals, as seen on figure 6c, so the recrystallisation seems to be the principal factor for the tertiary creep and the creep fracture of these samples. The recrystallisation can start anywhere as seen in figure 6d. The presence of alumina in the ceramics could be responsible for the recrystallisation. The formation of calcium-aluminate can destabilize the zirconia /3/ however, all the grains which appear are zirconia and no aluminum is observed preferentially by EXAF on these grains and elsewhere. Moreover the creep resistance of the samples is high, even at 1950 K, thus it does not seem that a liquidus can be formed at this temperature as the phase diagram of calcia-alumina predicts it. The role of the stress during the recrystallisation and eventually the tetragonal-cubic phase transition is not clear at the present time.

The cracking of the samples is not necessarily dangerous for the application of the
foams, whenever the thermal shock resistance should be good and the loading of the samples is very low. However, the cracks can have an influence on the electrical resistance of the heater, and it is observed that the resistance of a heater increases slowly when the furnace is operated a very long time.

VI - CONCLUSION

Zirconia foams are suitable as materials for heating elements in electrical furnaces. Their electrical properties are convenient and also their creep resistance at high temperature and under low stress. During the creep measurements, important visco-elastic behaviour was observed, which seems to be related to a recrystallisation, and it would be associated to the tetragonal-cubic phase transition and to the stress level. The influence of the stress on the recrystallisation and the formation of cracks should be clarified by further investigation.
REFERENCES