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DUAL MODE, MULTIPLE ELECTRODES QUARTZ SENSOR

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ABSTRACT

We present a method to design the electrodes shape of contoured BAW resonators intended to serve as temperature compensated force sensors. Those are based on simultaneous operation on two families of modes: fast shear B-mode and slow shear C-mode. Use of anharmonic modes instead of main overtone ones provides the possibility of spatial separation of vibrating areas, each mode being driven by separated pairs of electrodes. Electronic circuitry is greatly simplified and force deriving is straightforward.

KEYWORDS: *BAW resonator, anharmonic modes, force sensor.*

1. INTRODUCTION

High frequency bulk acoustic waves piezoelectric resonators are used as frequency-output sensors for direct measurement of force or related quantities such as acceleration or pressure. By applying a compressional diametrical force on a classical round resonator, a frequency shift is to be noticed depending on force orientation.

The performances of such sensors on wide temperature ranges are generally limited by their frequency-temperature sensitivity, even when the crystals are realized in (quasi) thermally-compensated cuts. A way to avoid this limitation is to use the quartz as its own temperature sensor to compensate the residual variation of frequency due to temperature change. This can be done by operating the resonator at two resonant modes of different families (B and C) and by extracting the useful information from the two frequencies of modes. The treatment is simplified if the corresponding transfer matrix is quasi-diagonal.

Then one mode must be essentially sensitive to the force, while the other must be essentially sensitive to the temperature. Electronic operation can be achieved by using a single pair of electrodes systems and appropriate filtering. In that case, main overtone modes, so-called (n,0,0) and belonging to different thickness-propagation families (B and C) are systematically used. The use of a pair of anharmonic modes offers a better way with superior optimization, since, in that case, one can efficiently connect the two oscillators to separate electrode systems on the sensing resonator, which greatly simplifies the design of the electronics. This can be achieved if the vibration amplitudes of the two modes are mainly located in separate regions in the plane of the resonator.

We present here a method for designing the shape of electrodes derived from the knowledge of modes patterns corresponding to given mode family, overtone number and rank of anharmonic. These ones are obtained experimentally by using X-ray. Then data is employed in association with the analytical model of Stevens and Tiersten [10] to get the precise amplitude distribution of mechanical displacement for the design of electrodes and to compute the force sensitivity of the sensor [3], [8].

Practical application was made for a plano-convex SC-cut where the C-mode is thermally quasi-compensated and B mode has a fairly linear frequency-temperature slope. If the applied force has a certain azimuth angle then the force sensitivity of the B mode will be insignificant compared to that of the C mode.

Taking advantage of spatial symmetry properties of well-chosen pair of modes (for instance using C-mode (3,0,1) and B-mode (3,1,0)) leads to a dual-mode design which virtually eliminates the intermodulation between the two oscillator signals, while keeping the transfer matrix as nearly diagonal as possible.

2. VIBRATION AMPLITUDE MODELLING

In figure 1, (x'_1, x'_3) represent the local coordinates of the modes rotated by the angle $\psi_n^{(i)}$ with respect to the resonator system of axis (X_1, X_3) .

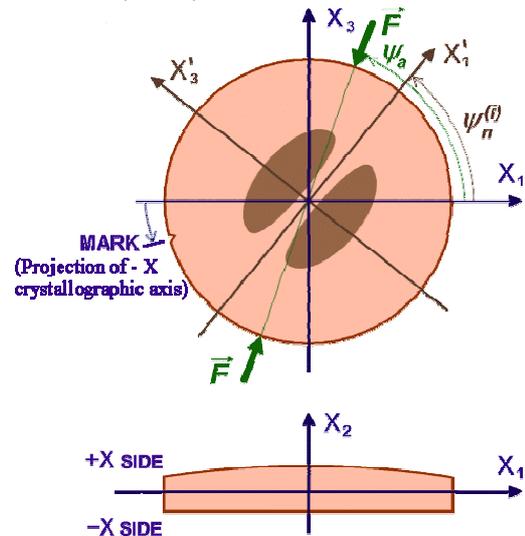


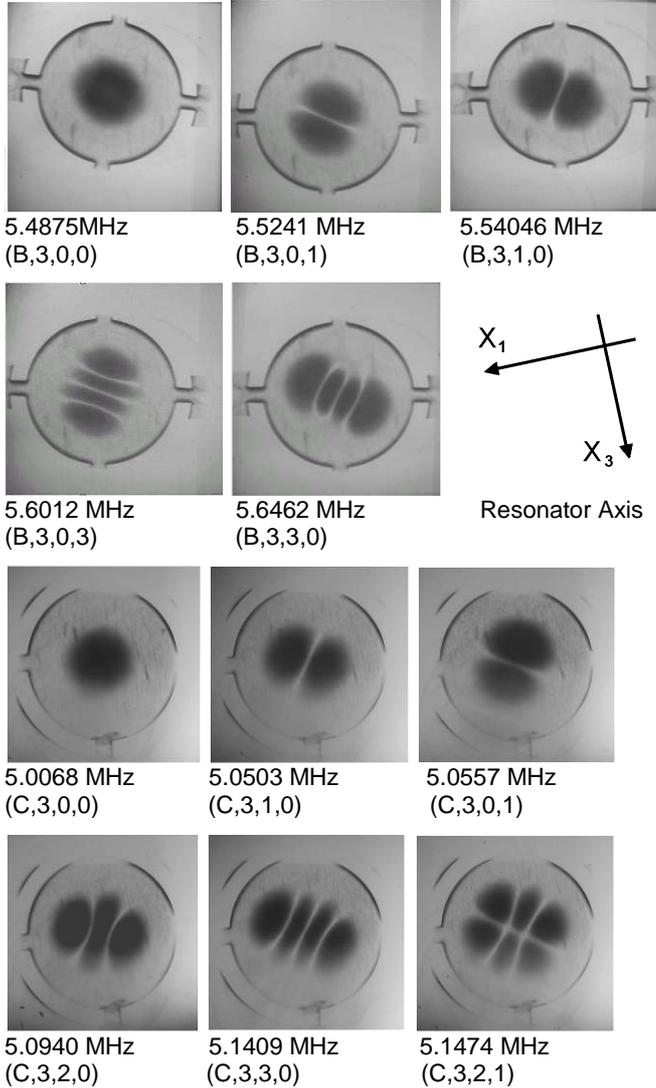
Figure 1. Contoured resonator geometry.

According to Stevens and Tiersten theory [10], [2] the normalized distribution of vibration amplitude is given by:

$$u_{nmp}^{(i)}(x'_1, x'_3, x_2) = H_m\left(\sqrt{\alpha_n^{(i)}} x'_1\right) \cdot H_p\left(\sqrt{\beta_n^{(i)}} x'_3\right) \cdot \sin \frac{n\pi x_2}{2h} \cdot e^{-\frac{\alpha_n^{(i)} x_1'^2 + \beta_n^{(i)} x_3'^2}{2}}$$

where:

- $i = B$ or C is the type of shear (fast or slow);
- $n = 1, 3, 5, \dots$ is the overtone number while m and p describe the vibration rank along X'_1 and X'_3 axis;
- H_m, H_p are Hermite polynomials ($H_0(x) = 1, H_1(x) = 2x, H_2(x) = 4x^2 - 2$ etc.);
- $2h$ is the thickness of the resonator;
- $\alpha_n^{(i)}$ and $\beta_n^{(i)}$ are constants that depend on the material, on the cut, on the type of shear, on the overtone n and on the curvature radius R , which govern the shape of the mode [2]. Values $\alpha_n^{(i)}, \beta_n^{(i)}$ and $\psi_n^{(i)}$ of are derived from experimental data (topographies and resonant frequencies).



Figures 2. X-rays topographies on a 5 MHz resonator.

An extensive series of X-ray topographies (XRT) were first performed on a 5 MHz multielectrode resonator to investigate experimentally the modes shapes and orientation angles.

Most representative mode patterns are shown in figures 2.

According to Lewis [7], the motional resistance R_1 is computed from integrals over the resonator volume:

$$R_1 = \frac{1}{Q\omega_{nmp}} \cdot \frac{\int_V c_{ijkl} S_{ij}^{nmp} S_{kl}^{nmp} dV}{\left(\int_V e_{kij} E_k^S S_{ij}^{nmp} dV \right)^2}$$

Where S_{ij}^{nmp} is the dynamic deformation depending on u_{nmp} of the mode and E_k^S is the static electric field in the resonator when a unity voltage is applied between the electrodes. Q is the quality factor of the resonator.

3. MULTIELECTRODE DESIGN

The criteria for a proper anharmonic modes multielectrode structure design are diverse and subject to tradeoff between them:

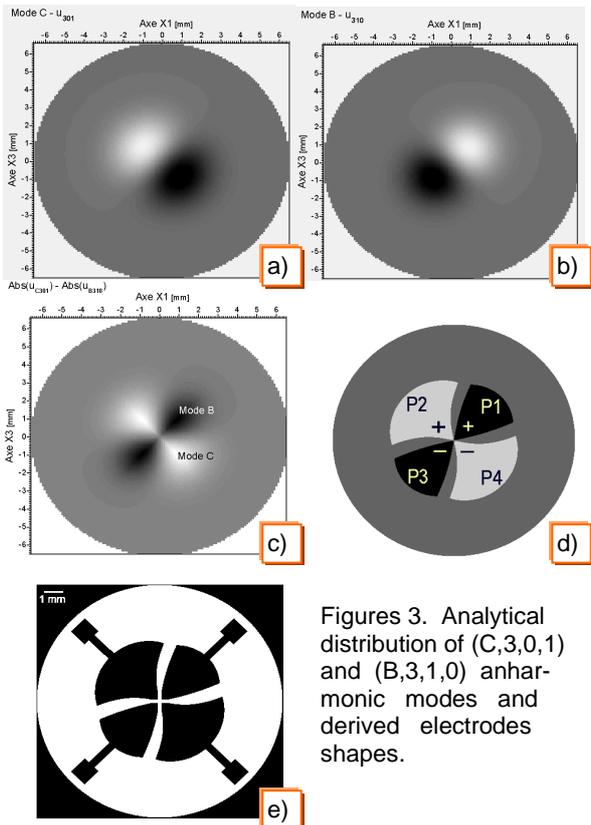
- nodal lines of thickness shear modes of different families must be as much orthogonal as possible;
- selected modes have to have low anharmonic ranks, provided that higher ranks give too complex distribution shapes;
- electrode shape must electrically excite as much as possible the selected anharmonic mode according with Lewis formula[7] but also to suppress unwanted others;
- electrode area must be taken into account, knowing that increasing the surface will increase the static capacitance C_0 while lowering the surface will diminish the mode amplitude;
- electrodes must be sufficiently spatially separated to avoid coupling capacitance between them.

First, we need to compute analytically the distribution of vibration amplitude of selected anharmonic modes pair. Several choices are possible; in our case selected pair was (C,3,0,1) and (B,3,1,0) – figures 3.a and 3.b respectively. The design steps included an algorithm to calculate the difference of modulus amplitudes $|u_{301}^C| - |u_{310}^B|$, which is represented on figure 3.c. The area covered by electrodes must satisfy the following conditions imposed to vibration amplitude:

- 1) $|u_{310}^B| > k \cdot |u_{301}^C|$ and $|u_{310}^B| \geq lev$ for B-mode electrode pairs,
- 2) $|u_{301}^C| > k \cdot |u_{310}^B|$ and $|u_{301}^C| \geq lev$ for C-mode electrode pairs,

where k is a called a separation factor and lev is the minimum level factor. Using Lewis formula, the motional resistance of mode is calculated. Proper values are: $k = 1.5$ and $lev = 10\%$ of peak amplitude. The resulted electrode shape is represented in figure 3.d. Electrode pairs P1 and P3 connected in antiparallel will drive the (B,3,1,0) mode while (C,3,0,1) mode will be excited by the electrodes P2 and P4. Final picture of electrodes plus associated connection pads is shown in figure 3.e.

Several multielectrode samples were constructed from quartz SC-cut blanks of 13.2 mm diameter, 0.7 mm thickness and 300mm curvature radius. Electrodes were made of gold on a chrome buffer by using photolithography technique. Selected (C,3,0,1) and (B,3,1,0) modes frequencies are located at 7.2947 MHz and 7.975 MHz respectively, as can be seen from the spectrums (figures 4-5, frequencies marked by circle). Quality factors in air range around 200,000.



Figures 3. Analytical distribution of (C,3,0,1) and (B,3,1,0) anharmonic modes and derived electrodes shapes.

All other modes present lower or equal admittances than selected ones. Unwanted modes of the highest amplitude are (B,3,0,1) and (C,3,1,0), which are separated by ~ 700 kHz from the selected modes and may be further filtered with passive components. Much lower amplitudes present the modes (B,3,0,3), (B,3,3,0), (C,3,0,3) and (C,3,3,0). Due to the fact that opposite pairs of electrodes are driven in antiparallel, ranks of anharmonic of even numbers such as (C,3,2,0) or (B,3,2,0) are completely suppressed. X-ray topographies of selected modes were performed and are shown on figure 6.

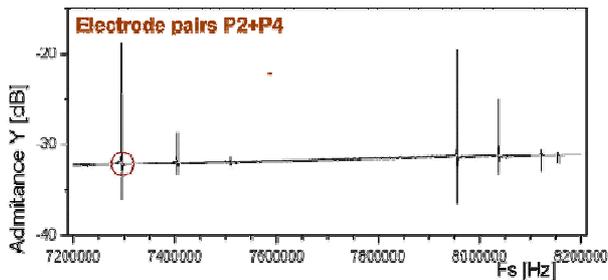


Figure 4. Admittance spectrum. Electrode pair for (C,3,0,1).

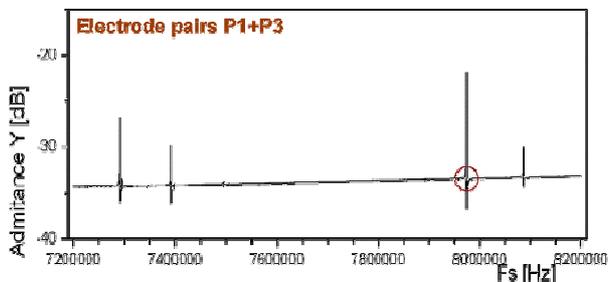
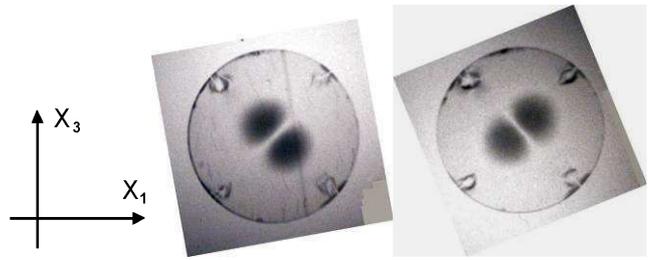


Figure 5. Admittance spectrum. Electrode pair for (B,3,1,0).



Figures 6. XRT on (C,3,0,1) and (B,3,1,0).

4. SENSOR TRANSFER FUNCTION

For SC-cut, B-mode is a thermometric one and was fitted under a 2nd order polynomial (figure 7) while the C mode is quasi-compensated, being described by cubic parabola (figure 8). Force sensitivity is linear up to 95 % of its crushing load [8].

$$\Delta f_B = f_B - f_{B0} = b_1 t + b_2 t^2 + S_{FB} F$$

$$\Delta f_C = f_C - f_{C0} = c_1 t + c_2 t^2 + c_3 t^3 + S_{FC} F$$

$f_{B0}=7977560$	$b_1=-203.126$	$b_2=-0.22721$	---
$f_{C0}=7294625$	$c_1=10.0365$	$c_2=-0.11365$	$c_3=3.541E-4$
[Hz] at 273.15 K	[Hz/K]	[Hz/K ²]	[Hz/K ³]

As seen from figure 9 where the Ratajski force sensitivity coefficients K_f [8], [3] are represented vs. ψ_a (angle of applied force). For a azimuth angle of $\psi_a = 75^\circ$ the force sensitivity S_{FB} of (B,3,1,0) mode is negligible while the force sensitivity S_{FC} of (C,3,0,1) mode is close to maximum.

$$S_{FB} = \frac{\Delta f_B}{\Delta F} \cong 0 \ll S_{FC} = \frac{\Delta f_C}{\Delta F} \cong -14.95 \text{ Hz/N}$$

Mode (B,3,1,0)

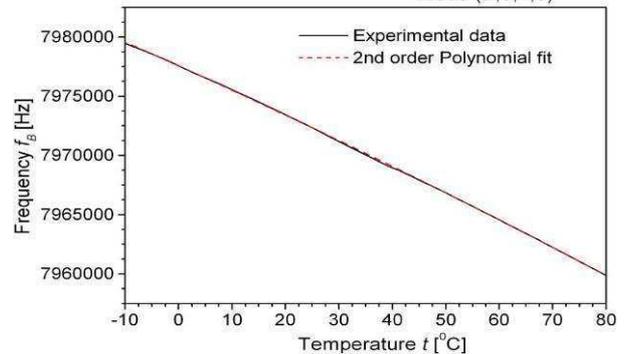


Figure 7. Frequency-Temperature Characteristic of (B,3,1,0).

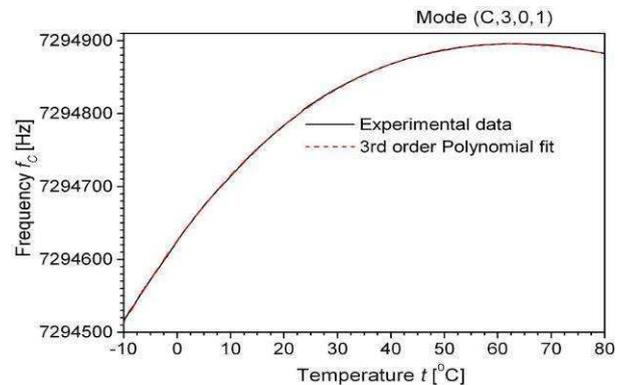


Figure 8. Frequency-Temperature Characteristic of (C,3,0,1).

5. CONCLUSIONS

This approach efficiently combines the designing effort on the crystal resonator and driving electronics in order to make dual-mode multiple electrodes sensors competitive in comparison with the more complicated sensors electronically discriminated dual-mode sensors relying on a single pair of wires. Using two independent low-cost oscillators connected to a microcontroller, a precise measurement system of force is implemented.

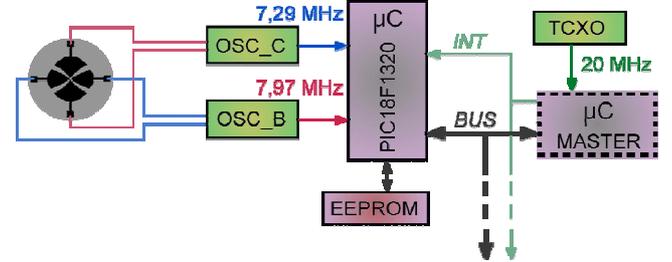


Figure 12. Digital processing circuit block diagram.

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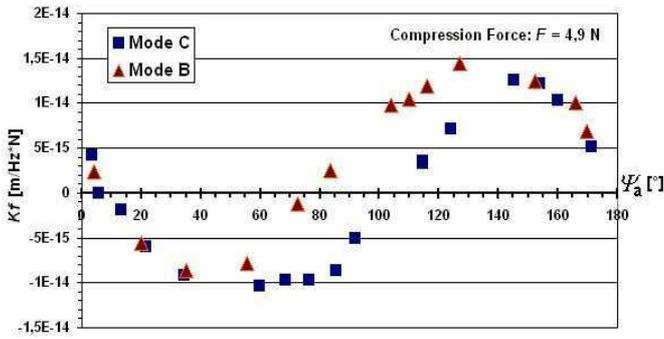


Figure 9. Force sensitivity coefficients K_f of (C,3,0,1) and (B,3,1,0) modes w.r.t. azimuth angle ψ_a .

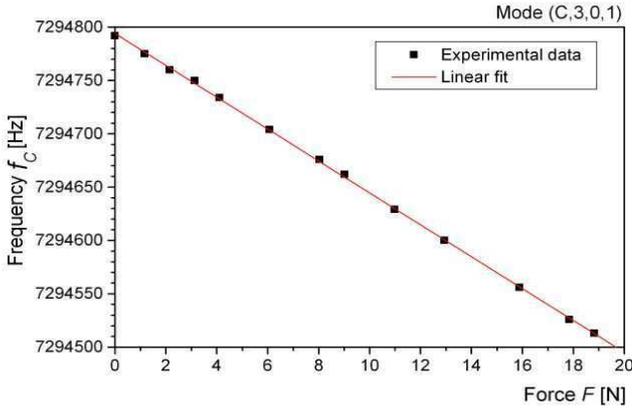


Figure 10. Frequency-Force Characteristic at $\psi_a = 75^\circ$.

For example, an azimuth error of $\pm 2^\circ$ leads to a non-zero S_{FB} that finally causes the errors: $\delta_t = -0,004^\circ\text{C}$ on temperature measurement and $\varepsilon_F = 0.33\%$ force relative error. Temperature t value is obtained from the B-mode frequency:

$$t = \frac{-b_1 - \sqrt{b_1^2 + 4b_2 \cdot \Delta f_B}}{2b_2}$$

Then, the force transfer function results from the above temperature formula and the C-mode frequency. A plot of the function depending on frequency variations is shown in figure 11.

$$F = \frac{1}{S_{FC}} (\Delta f_C - c_1 t - c_2 t^2 - c_3 t^3)$$

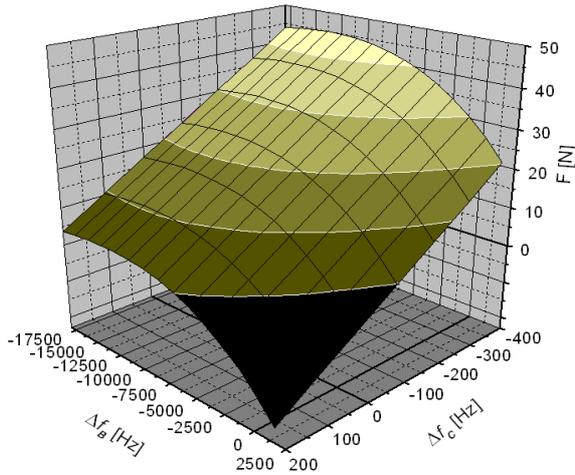


Figure 11. Force-frequencies transfer funct. $F = (\Delta f_B, \Delta f_C)$