

1 **Abstract**

2 Laboratory tests were conducted to investigate the effect of wetting-drying (W-D)
3 cycles on the initiation and evolution of cracks in clay layer. Four identical slurry
4 specimens were prepared and subjected to five subsequent W-D cycles. The water
5 evaporation, surface cracks evolution and structure evolution during the W-D cycles
6 were monitored. The effect of W-D cycles on the geometric characteristics of crack
7 patterns was analyzed by image processing. The results show that the desiccation and
8 cracking behaviour was significantly affected by the applied W-D cycles: the
9 measured cracking water content θ_c , surface crack ratio R_{sc} and final thickness h_f of
10 the specimen increased significantly in the first three W-D cycles and then tended to
11 reach equilibrium; the formed crack patterns after the second W-D cycle were more
12 irregular than that after the first W-D cycle; the increase of surface cracks was
13 accompanied by the decrease of pore volume shrinkage during drying. In addition, it
14 was found that the applied W-D cycles resulted in significant rearrangement of
15 specimen structure: the initially homogeneous and non-aggregated structure was
16 converted to a clear aggregated-structure with obvious inter-aggregate pores after the
17 second W-D cycle; the specimen volume generally increased with increasing cycles
18 due to the aggregation and increased porosity. The image analysis results show that
19 the geometric characteristics of crack pattern were significantly influenced by the
20 W-D cycles, but this influence was reduced after the third cycle. This is consistent
21 with the observations over the experiment, and indicates that the image processing can
22 be used for quantitatively analyzing the W-D cycle dependence of clay desiccation
23 cracking behaviour.

24

25 **Keywords:** wetting-drying cycle; clay layer; desiccation crack; aggregate formation;
26 image processing; crack pattern

1 Introduction

2 The formation of desiccation cracks on soil surface due to loss of water is a common
3 natural phenomenon, and can significantly affect the soil performance in various
4 geotechnical, agricultural and environmental applications. For example, a cracked soil
5 is more compressible than an intact one at the same water content and the overall
6 mechanical strength is weakened due to the presence of cracks (Morris et al., 1992).
7 The size (width, length and depth), tortuosity, spatial distribution and connectivity of
8 cracks govern the rate and the velocity at which solutes and microorganisms are
9 transported in the soil, and thus control the dispersal of substances in soil (Horgan and
10 Young, 2000). Most importantly, the soil hydraulic properties are directly controlled
11 by the desiccation crack networks (Chertkov and Ravina, 1999; Chertkov, 2000).
12 Many previous studies have indicated that the hydraulic conductivity of cracked soils
13 is several orders of magnitude greater than that of intact soils (Boynton and Daniel,
14 1985; Albrecht and Benson, 2001). This issue is therefore a major concern in design
15 and construction of low permeability structures as clay buffers and barriers for nuclear
16 waste isolation, liners and covers for landfill, etc.

17 Over the past decades, a number of field studies and laboratory experiments have
18 been undertaken to investigate the initiation and propagation of desiccation cracks in
19 soils (Corte and Higashi 1960; Kleppe and Olson, 1985; Morris et al., 1992; Konrad
20 and Ayad, 1997; Miller et al., 1998; Velde, 1999; Nahlawi and Kodikara, 2006; Tang
21 et al., 2008; Tang et al., 2010). However, these investigations have been largely
22 qualitative and most are limited in the description of desiccation cracking phenomena.
23 More recently, techniques for quantifying the main features of the crack patterns have
24 evolved from direct field measurement to more sophisticated analysis by image
25 processing (Miller et al., 1998; Velde, 1999; Vogel et al., 2005). Image analysis has
26 proved to be a powerful tool by which several geometric and morphologic parameters
27 such as crack width, length, area, angle and their distribution characteristics can be
28 determined effectively. In addition, some modelling and theoretical studies on
29 desiccation cracking have also been conducted (Abu-Hejleh and Znidarčić, 1995;
30 Ayad et al., 1997; Konrad and Ayad, 1997; Chertkov and Ravina, 1998; Chertkov,
31 2000; Chertkov, 2002; Deng and Shen, 2006; Péron, 2008; Péron et al., 2009a).
32 However, as soil is a highly complex material, the desiccation cracking behavior is
33 governed by a large number of factors including mineral composition, clay content,
34 relative humidity, temperature, layer thickness, boundary conditions etc. (Fang, 1997;
35 Albrecht and Benson, 2001; Nahlawi and Kodikara, 2006; Rodríguez et al., 2007;
36 Tang et al., 2007; Tang et al., 2008; Tang et al., 2010). It is therefore difficult to
37 propose a rational model to describe this complex phenomenon with a reasonable
38 number of parameters. The essential mechanism of desiccation cracking is still not
39 well understood today and the prediction of cracks initiation and the associated crack
40 network propagation also faces several challenges.

41 It is recognised that the soil in-situ is subject to diurnal changes and seasonal rainy
42 and sunny weather, and undergoes periodical wetting-drying (W-D) cycles. Several
43 studies have been performed to investigate the effect of wetting and drying on soil

1 physical properties (Rao et al., 2001; Alonso et al., 2005; Nowamooz et al., 2009,
2 Tang et al. 2011). However, the relationship between W-D cycles and desiccation
3 cracking behaviour is still not clearly understood. In this study, the effect of W-D
4 cycles on cracking behaviour was investigated by subjecting a group of initially
5 saturated clay layers to five W-D cycles. The initiation and evolution of cracks on the
6 specimen surface during the cycles were monitored. The geometric characteristics of
7 surface crack patterns are described and quantified through image processing and the
8 mechanisms involved are discussed.

10 **Material and methods**

11 *Material*

12 The Romainville clay was used in this investigation. The physical properties are
13 presented in Table 1. This clay is a lagoonal-marine deposit which is part of the Paris
14 Basin Tertiary (Oligocene) formations. It is widely distributed over the eastern region
15 of Paris, and has been considered responsible for the large amount of damages to
16 buildings due to the swelling-shrinkage and cracking phenomenon. Various studies
17 have been undertaken to analyse the hydro-mechanical behaviour of the clay under
18 weather effects such as W-D cycles (Audiguier et al., 2007; Laribi et al., 2008;
19 Geremew et al., 2009; Tang et al., 2009a; Tang et al., 2009b). However, little attention
20 has been paid to the effect of W-D cycles on the desiccation cracking behaviour.

22 *Test methods*

23 The air-dried Romainville clay was crushed and sieved at 2 mm. Saturated slurry
24 specimens were prepared by mixing the crushed powder with distilled water at a water
25 content of approximately 170 % (g g^{-1}) (Note that all the given water contents of the
26 tested specimens in the next sections is 'gravimetric' water content, unless otherwise
27 specified). A desired quantity of slurry was then poured into glass cups (117 mm in
28 diameter). To remove entrapped air bubbles in the slurry, these cups were placed on a
29 vibration device for 5 minutes. Finally, the cups were sealed with plastic membrane
30 and left for at least 3 days. The final settled layer thickness was about 10 mm.

31 Four parallel specimens were prepared and dried at constant room temperature
32 (25 ± 1 °C, 50 ± 5 % of relative humidity) until the weight of specimen was stabilized,
33 i.e., the first W-D cycle was completed. The subsequent wetting was started by
34 pouring distilled water directly into the glass cups. During this wetting process,
35 sufficient water was provided to ensure full submergence of the specimen and no
36 mixing was applied. The glass cups were again sealed with plastic membrane to
37 prevent water evaporation. After three days, the specimens were exposed to room
38 conditions to be dried again. This procedure was repeated and finally a total of five
39 W-D cycles was applied.

40 The schematic set-up used in this study is illustrated in Fig. 1. In order to measure
41 the variation of water content during drying, the specimen was placed on a balance

(with an accuracy of 0.01 g) to monitor the weight. A digital camera was fixed above the specimens to capture the surface image during wetting and drying cycles in different time steps. Fig. 2 presents a typical crack pattern taken during the first drying path. With the application of image processing, the surface crack ratio (R_{sc}) or crack intensity factor CIF (Miller et al., 1998), defined as the ratio of the area of cracks to the total initial area of specimen, was determined to quantify the cracking extent during drying. At the end of each W-D cycle, other geometric parameters - the number of intersections per unit area N_{int} , number of crack segments per unit area N_{seg} , mean crack length L_{av} , mean crack width W_{av} and mean clod area A_{av} - were also determined from the final crack patterns. Note that the crack length was determined by calculating the length of the mid-axis of crack segment between two intersections. For this purpose, a skeletonising operation (Gonzalez and Woods, 2002) was initially performed by repeatedly removing pixels from the boundaries of cracks until they are reduced to single-pixel-wide skeletons. The crack width was sampled in orthogonal direction and the shortest distance between the crack boundaries was calculated. The clods are surrounded by cracks, and their areas are defined as the pixel number of the regions. All these parameters were obtained by applying the software CIAS which was developed by our research group. More details can be found in Liu et al. (2008) and Tang et al. (2008). Eight clods were selected from each specimen in the end of each drying period to determine their thickness using calliper, and the mean value is regarded as the final thickness of specimen layer.

In order to investigate the volume shrinkage behaviour of specimens during drying, four other identical specimens were prepared following the same procedure described above. During the first drying path, small clods were taken from the specimens in different time steps to determine their water contents θ and density ρ . The clod volume used for the density determination was measured by immersing it in a non-wetting hydrocarbon liquid. Then the void ratio e and the corresponding degree of saturation S_r of specimens can be determined using the following equations:

$$e = \frac{\rho_s(1 + 0.01\theta)}{\rho} - 1 \quad (1)$$

$$S_r = \frac{\theta\rho_s}{e} \quad (2)$$

where ρ_s is the density of the solid phase of the Romainville clay, equal to 2.79 Mg m⁻³ (Table 1).

Results

Evaporation, shrinkage and cracking process

The measured water content θ at various times t during the first drying path for the four separate specimens are shown in Fig. 3 (desiccation curve). Two distinct evaporation stages can be indentified: a constant evaporation stage during which water content decreases linearly with time; and a subsequent falling evaporation stage

1 during which water loss slows down gradually until the residual water content of
2 about 4.3 % is reached.

3 The determined shrinkage curve (e versus θ) is presented in Fig. 4, from which two
4 transition points between linear and exponential phases can be determined - the air
5 entry (AE) point and the shrinkage limit (SL) point (Stirk, 1954; Boivin et al., 2004;
6 Groenevelt and Grant, 2004; Cornelis et al., 2006; Chertkov, 2007). The water
7 contents at the point of AE and SL are approximately 18% and 12%, respectively.
8 After desiccation cracks appear on the surface of the specimen, the surface crack ratio
9 R_{sc} at different water content θ was determined by image processing, and the result is
10 also plotted in Fig. 4 as the cracking curve (R_{sc} versus θ). This indicates that the water
11 content at the onset of cracking ranges from 38 to 43%, which is much higher than the
12 AE value. Therefore the specimens are still fully saturated as cracking occurs. During
13 the initial stage, the R_{sc} increases rapidly with decreasing water content and
14 decreasing pore volume. However, with further drying, the increment of R_{sc} slows
15 down once the water content is close to AE point ($\theta = 18\%$). After the SL ($\theta = 12\%$) is
16 reached, the R_{sc} approaches a relative steady value of 14.6-15.8 % for the four
17 separate specimens.
18

19 *Cracking water content, final surface crack ratio and layer thickness*

20 During drying, when the first crack is observed on the specimen surface, the
21 corresponding water content is herein defined as the cracking water content θ_c . Fig. 5
22 shows the determined θ_c of the four specimens during each drying path. It indicates
23 that θ_c increases rapidly during the first three drying paths, and does not change
24 significantly during the subsequent fourth and fifth drying paths. For instance, the
25 mean value of θ_c of the four specimens during the first drying path is 40.5%;
26 increasing to 76.1% during the third drying path, whereas the mean value of θ_c during
27 the fifth drying path is 80.2%, only 1.2% higher than the fourth drying path.

28 After each W-D cycle, the final surface crack ratio R_{sc} and the mean final thickness
29 h_f were also determined and are presented in Fig. 6 and Fig. 7 respectively. Similar to
30 θ_c , the final mean value of R_{sc} and h_f of the four specimens also increase quickly in
31 the first three W-D cycles, while the increment rate slows down in the subsequent
32 cycles.
33

34 *Geometric parameters of crack pattern*

35 Quantitative analysis of the crack pattern is important when studying clay cracking.
36 Indeed, the geometric parameters are helpful in evaluating the hydro-mechanical
37 properties of the clay-water system. They are also related to the variation of the
38 stress-strain state and may provide a way to investigate the essential mechanisms of
39 cracking. In addition, the crack propagation behavior and the geometric characteristics
40 of the crack pattern reflect the material plasticity and mineral compositions. Perrier et
41 al. (1995) indicated that if the real structure features of crack pattern can be
42 determined, the soil response to wetting and drying can be predicted.

1 Table 2 summarizes the mean values of the geometric parameters which were
2 determined from the final crack patterns after each W-D cycle, the corresponding
3 standard deviation (SD) are also presented. It is found that the mean values of all the
4 parameters in the first three cycles are much more variable than that in the subsequent
5 cycles. For N_{int} and N_{seg} , they reach the maximum value after the second cycle and
6 decrease after the third cycle. After that, N_{int} and N_{seg} increase slightly with further
7 increase of W-D cycles. Moreover, the ratio of $N_{\text{seg}}/N_{\text{int}}$ is greater than 1.5 and less
8 than 2 for all the cycles, indicating that, three or four crack segments sharing one
9 intersection, is the dominant outline of the crack pattern. For L_{av} , the maximum and
10 the minimum values are 8.43 mm and 7.57 mm respectively after the first and second
11 cycle. It is between 8.07 and 8.22 mm after the third cycle and no obvious trend can
12 be observed. For W_{av} , the minimum value is 1.01 mm that is observed after the first
13 cycle; it reaches a maximum value at 1.86 mm after the third cycle and decreases
14 slightly in the subsequent cycles. Based on the obtained values of L_{av} and W_{av} , it can
15 be deduced that most of the formed cracks in the first drying cycle are slim and
16 threadlike. For A_{av} , the maximum value is 1.18 cm² observed after the first cycle. It
17 generally decreases with increasing cycles and finally stabilizes at 0.65 cm²,
18 indicating that the clods become smaller due to fragmentation. These results indicate
19 that the geometric and morphologic characteristics of crack patterns are significantly
20 influenced by W-D cycles, but the influence intensity declines after the third cycle.
21 Moreover, the corresponding SD of the determined parameters generally decreases
22 with increasing cycles, indicating that the initial densities, sizes or dimensions of the
23 crack elements show significant variability but become more homogeneous under the
24 effects of W-D cycles.

26 Visual observations and discussion

27 *Crack pattern and structure evolution after W-D cycles*

28 Fig. 8 presents the typical crack pattern after each W-D cycle. It indicates that the
29 specimen surface was split to separate clods by the crack networks. After the first
30 W-D cycle (Fig.8 (a)), the shapes of the clods are relatively regular and most of the
31 clods are close to quadrangles or pentagons; the crack segments are smooth and
32 generally perpendicular to each other. This is consistent with the observations of
33 Vogel et al. (2005) and Peron et al. (2009b), and can be explained using the maximum
34 stress release criterion and crack propagation criterion (Lachenbruch, 1962; Morris et
35 al., 1992).

36 After the second W-D cycle (Fig. 8 (b)), the shapes of the separated clods are more
37 irregular and the crack segments are more jagged than that observed in Fig. 8 (a). The
38 second W-D cycle also caused dramatic aggregate formation from the initially
39 non-aggregated structure. The formed clods were degraded significantly and a large
40 number of inter-aggregate pores can be observed.

41 Figs. 8 (c), (d) and (e) indicate that the geometric and morphologic characteristics
42 of the crack patterns are similar to each other after the third, fourth and fifth W-D

1 cycle. This observation is consistent with the quantitative results of the geometric
2 parameters in Table 2. In the tests of Yesiller et al. (2000) and Tang et al. (2008), most
3 cracks after the second and third W-D cycles were found to be situated at the same
4 locations as that after the first W-D cycle. However, this was not evident in this study
5 when comparing Figs. 8 (a), (b) and (c). This can be attributed to the heterogeneous
6 aggregated-structure formed during the wetting process. Many weak zones were
7 created, which significantly control the start positions of cracks during the subsequent
8 drying period (Yong and Warkentin, 1975).

9 Based on the results of surface crack ratio R_{sc} and layer thickness h_f shown in Figs.
10 6 and 7, the final total volume of the dried clods (without the cracks) as well as the
11 increment of porosity after each W-D cycle can be calculated. It is found that, after the
12 fifth cycle, the porosity of the clods increases by approximately 21%. This is
13 consistent with the findings of the previous studies on remolded and natural soils
14 (Sartori et al., 1985; Pires et al., 2008), and can be explained by the progressive
15 increase in pore volume and the average diameter of the pores with the increase of
16 W-D cycles (Geremew et al., 2009).

18 *Crack pattern evolution and aggregate formation during wetting*

19 A time series of 6 images is shown in Fig. 9 to illustrate the evolution of surface
20 cracks and aggregate formation process during the second wetting path. For reasons of
21 simplicity and clarity, only the white marked area in Fig. 8 (a) is presented. Fig. 9 (a)
22 shows the initial morphology of desiccation crack pattern taken from Fig. 8 (a). Figs.
23 9 (b) and (c) indicate that injecting water led to immediate collapse of the clods: the
24 clods were broken down into several small aggregates. Meanwhile, some new
25 micro-cracks induced by wetting appeared on the specimen's surface.

26 Notably, the collapse or destruction firstly occurred on the clods edges, especially
27 on the corner positions (circled zones in Fig. 9 (b)). This is because rapid hydration
28 firstly occurred at these less stable positions, and the previous cracks provided free
29 spaces for clay swelling.

30 Upon further wetting, the original desiccation cracks tend to be increasingly narrow
31 due to the filling of the exfoliated aggregates from the clods as well as the volume
32 swelling of the clods. Fig. 9 (d) shows that the original desiccation cracks were fully
33 closed after about 2.5 min wetting. However, there were more and more new
34 micro-cracks induced by wetting. These new cracks are mainly resulted from the
35 differential swelling pressures and the inner stresses during the wetting process of the
36 clods. Fig. 9 (d) also shows that the specimen surface is not as flat and smooth as its
37 initial state, but is 'heaved' along the trace of the original desiccation crack segments,
38 as quadrangle marked in Figs. 9 (c)-(e). This is because the high swelling potential of
39 the clay minerals was constrained so that the clods jostle against each other.

40 Comparison between Fig. 9 (e) and Fig. 9 (f) shows that the surface morphologies
41 are similar to each other. The edges of the aggregates are clear and the
42 wetting-induced new cracks can still be identified even after a long time (72 hours)
43 has elapsed. However, in the test of Tang et al. (2008), the aggregates breakdown into

1 individual fine particles and the new cracks were completely closed after a short
2 wetting time of 2 hours. This can be attributed to the different clay fractions in the
3 studied materials. For Romainville clay, the clay fraction is 79 %, which is 57%
4 higher than Xiashu clayey soil used by Tang et al. (2008). The dispersion of
5 aggregates was therefore prevented by the strong bonds between clay particles.

6 Pictures of the specimen subjected to the third wetting path are presented in Fig. 10.
7 The observations are slightly different from the second wetting process (Fig. 9). After
8 water was poured into the glass cup, clods degraded rapidly and some small aggregate
9 plates floated on the water surface (Fig. 10 (a)). About 1.5 min later, the original
10 desiccation cracks were fully closed (Fig. 10 (b)); after a period of 72 h wetting, all
11 the clods were broken down and a large amount of individual aggregates can be
12 observed (Fig. 10 (c)). However, no new micro-cracks or “jostle effects” were
13 observed, as in the second wetting path (Fig. 9).

14 During the fourth and fifth wetting paths, no significant difference was observed as
15 compared to the third wetting path, and as a result, no pictures are presented.

17 *Effect of W-D cycles on cracking water content*

18 Fig. 5 demonstrates that the W-D cycles result in significant increase in cracking
19 water content θ_c . Moreover, near 90% of the increase occurs in the first three cycles.
20 Previous studies indicate that cracking occurs when the tensile stress induced by the
21 developed suction exceeds the tensile strength of the specimen (Corte and Higashi,
22 1960; Morris et al., 1992; Miller et al., 1998; Péron et al., 2009b). The effects of W-D
23 cycles on this cracking behaviour can be explained by considering the specimen fabric,
24 as follows:

25 i) during W-D cycles, volume shrinkage and cracking would result in irreversible
26 fabric changes, decrease of specimen integrity and increase of weak zones in
27 specimen (Yong and Warkentin, 1975). As a result, the specimen tensile strength was
28 reduced, promoting specimen cracking at a higher θ_c upon the subsequent drying;

29 ii) the multiple W-D cycles gave rise to an increase in material heterogeneity as
30 discussed in the above sections. For instance, after the first W-D cycle, the initial
31 homogenous structure was changed to aggregated-structure during the subsequent
32 W-D cycles (Fig. 8). Due to the non-uniform distribution characteristics of aggregate
33 sizes and inter-aggregate pore sizes, the tensile stresses developed during subsequent
34 drying cycles would be also non-uniform and can easily be concentrated at defects
35 with lower tensile strength. Weinberger (1999) and Tang et al. (2008) have observed
36 that cracks first initiated at surface defects, and emphasized that the surface defects
37 can trigger or promote crack initiation due to shrinkage distortion of the surrounding
38 medium and tensile stress concentration.

39 Note that because of the difficulty in drying tests, there has been no experimental
40 data concerning the actual value of the local water content at the moment of crack
41 initiation. The commonly measured water content in the laboratory is a mean value
42 and can not completely reflect the moisture distribution characteristics in localised
43 positions. To reduce the test error, the simplest way is to prepare an initially relatively

1 homogenous specimen with a limited thickness – thus thin layer (10 mm thick) slurry
 2 specimens were prepared in this study. Generally, the physical, hydraulic and
 3 mechanical properties of the specimen vary permanently with moisture changes
 4 during drying. In order to better understand the intrinsic mechanism of desiccation
 5 cracking, future studies should also take into account some dynamic factors such as
 6 evaporation rate, suction development rate, volume shrinkage rate and tensile strength
 7 development rate, in addition to the critical water content θ_c .

9 *Equilibrium state during multiple W-D cycles*

10 Based on all the results shown in Figs. 5 (θ_c), 6 (R_{sc}), 7 (h_f) and Table 2, it can be
 11 concluded that the cracking behaviour reached a relative equilibrium state after the
 12 specimens were subjected to the third cycle. This conclusion is also supported by the
 13 observations shown Fig. 8: no significant difference can be observed for the crack
 14 patterns after the third, fourth and fifth W-D cycle. Presumably the rearrangement of
 15 specimen fabric diminishes and finally ceases after certain a number of W-D cycles.

16 Previous studies on this subject also confirmed that there is an equilibrium state
 17 during multiple W-D cycles, but the corresponding numbers of cycles depend on
 18 material nature especially the clay fraction. Generally, clayey soils with high plasticity
 19 need more W-D cycles to reach the equilibrium state than silty or sandy soils
 20 (Al-Wahab and EI-Kedrah, 1995; Yesiller et al. 2000; Omid et al., 1996).

22 **Conclusions**

23 Desiccation and cracking behaviour of clay layers from a slurry state upon five
 24 wetting-drying (W-D) cycles were investigated through laboratory experiments. The
 25 process of water evaporation, surface cracks evolution, structure evolution and
 26 volume shrinkage behaviour were monitored and have been discussed here. The
 27 geometric characteristics of crack pattern after each W-D cycle were quantitatively
 28 analyzed by image processing. The following conclusions can be drawn:

29 (1) during the first drying path, the water evaporation process is composed of two
 30 stages: a constant rate zone and a subsequent decreasing rate zone; the increase of
 31 surface crack ratio R_{sc} during drying was accompanied by progressive pore volume
 32 shrinkage, and the R_{sc} reached stabilization as the water content reached the shrinkage
 33 limit; the final crack pattern was dominated by polygonal clods and smooth crack
 34 networks;

35 (2) during the second wetting path, the poured water resulted in rapid collapse of
 36 clods, and the desiccation cracks formed in the previous drying path were quickly
 37 closed; meanwhile, a large number of new micro-cracks induced by wetting appeared
 38 on the specimen surface that divided the clods into smaller aggregates, and a typical
 39 aggregated-structure was developed and significantly intensified the specimen
 40 heterogeneity; moreover, the second wetting path led to significant rearrangement of
 41 clay particles and modification of the pore network; these processes are generally
 42 irreversible and drastically influence the desiccation cracking behaviour during the

1 subsequent drying path;

2 (3) after the second drying path, since the specimen homogeneity decreased, the
3 shapes of the clods were more irregular and the crack segments were more jagged
4 than that observed after the first drying path; the clods showed clear
5 aggregated-structure with a large amount of inter-aggregate pores; the bonds between
6 the formed aggregates were broken quickly in the third wetting path and no new
7 micro-cracks were induced;

8 (4) an equilibrium state can be reached after a certain numbers of W-D cycles; for
9 the tested Romainville clay, it was observed that the rearrangement of specimen fabric
10 or structure reached an apparent state of equilibrium after the third W-D cycle: before
11 that, the measured cracking water content θ_c , final surface crack ratio R_{sc} and layer
12 thickness h_f increased significantly with increasing cycles, but after, the effects of
13 W-D cycles on the cracking behaviour and the cracking pattern became insignificant;

14 (5) image processing provided useful information on the geometric characteristics
15 of crack patterns. The effect of W-D cycle on desiccation and cracking behaviour can
16 therefore be quantitatively described through these specific parameters.

17 Generally, field soils are very complex and conditioned by a large number of
18 variables. Cracking is a 3D phenomenon and the patterns are usually composed of
19 irregular polygonal shapes. Quantification of a 3D crack pattern is a much more
20 challenging task than the 2D process described in this investigation. However, it is
21 believed that the findings of this laboratory experiment are helpful for better
22 understanding the interrelationship between the sequence of seasonal processes and
23 the evolution of soils or mud properties. In addition, as multiple W-D cycles can result
24 in possible changes in clay structure and cracking behaviour, the hydraulic and
25 mechanical properties of this type of materials must depend on the number of W-D
26 cycles. Further attention should therefore be paid to the engineering fields where
27 swelling clays are involved.

28

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39

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1 **Tables**

2

3 **Table 1 Physical properties of Romainville clay**

Physical properties	Values
Density of the solid phase	2.79 Mg m ⁻³
Liquid limit	77 %
Plastic limit	40 %
Plasticity index	37 %
USUC ^a classification	CH
Clay (<2μm)	79 %
Clay composition	Illite and smectite
Specific surface area	340 m ² /g

4 a-Unified Soil Classification System

5

6 **Table 2 Mean values of crack quantitative parameters and the**
 7 **corresponding standard deviation (SD) after each wetting-drying cycle**

After each wetting-drying cycle	N_{int} (cm ⁻²)	SD of N_{int}	N_{seg} (cm ⁻²)	SD of N_{seg}	L_{av} (mm)	SD of L_{av}	W_{av} (mm)	SD of L_{av}	A_{av} (cm ²)	SD of L_{av}
First	1.09	0.17	1.78	0.12	8.43	4.50	1.01	0.63	1.18	1.20
Second	1.52	0.12	2.45	0.19	7.57	3.75	1.52	0.49	0.78	0.56
Third	1.37	0.08	2.13	0.11	8.12	3.42	1.86	0.42	0.69	0.53
Fourth	1.43	0.05	2.16	0.08	8.07	3.31	1.74	0.38	0.65	0.53
Fifth	1.44	0.07	2.22	0.05	8.22	2.75	1.73	0.37	0.65	0.49

8 **Figure captions**

9 Fig. 1 Schematic drawing of set-up

10 Fig. 2 A typical desiccation crack pattern of specimen during the first
11 drying path

12 Fig. 3 Desiccation curves of the specimens during the first drying path

13 Fig. 4 Variation of surface crack ratio R_{sc} and void ratio e with water
14 content θ during the first drying path

15 Fig. 5 Cracking water content θ_c of the specimens during each drying path

16 Fig. 6 Surface crack ratio R_{sc} after each W-D cycle

17 Fig. 7 Mean thickness h_f of specimen layer after each W-D cycle

18 Fig. 8 Typical desiccation crack patterns after each W-D cycle (pictures
19 were taken from the same specimen)

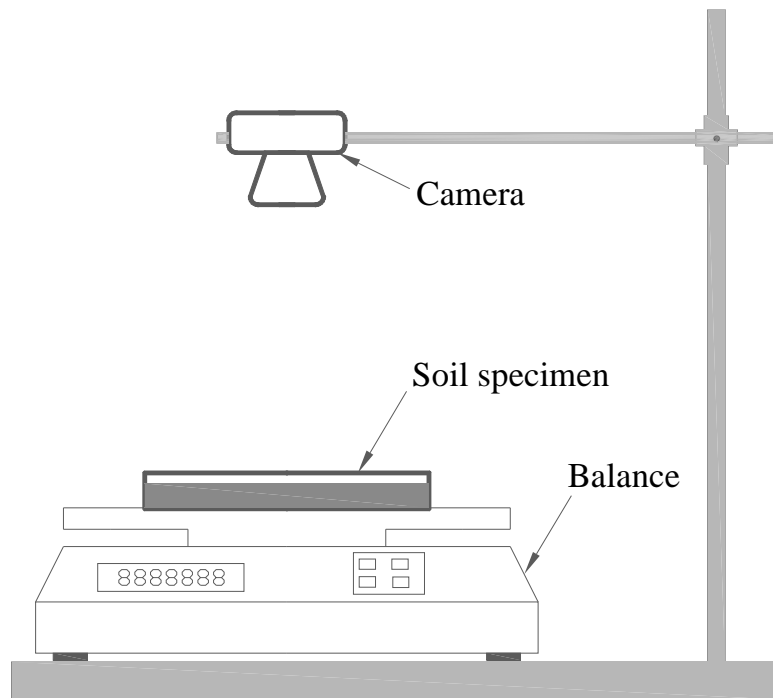
20 Fig. 9 Evolution of crack pattern during the second wetting path

21 Fig. 10 Evolution of surface cracks during the third wetting path

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24 **Figures**



25

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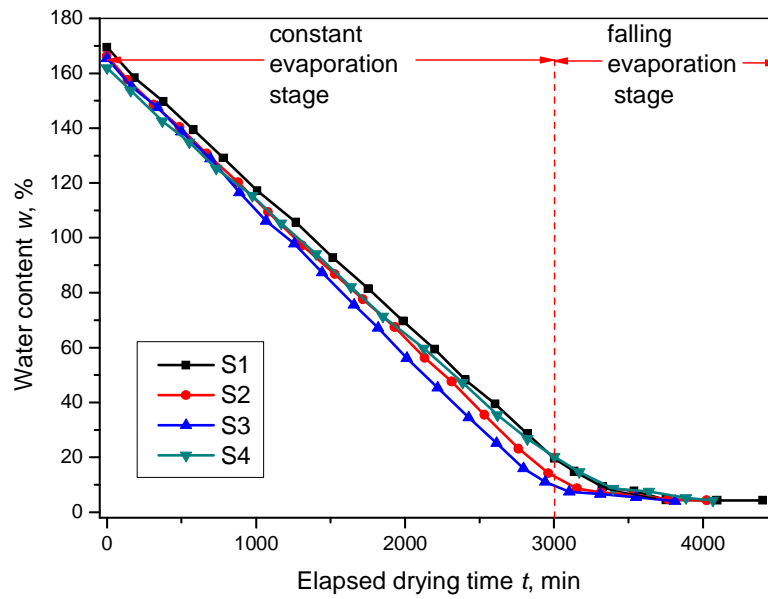
Fig. 1 Schematic drawing of set-up

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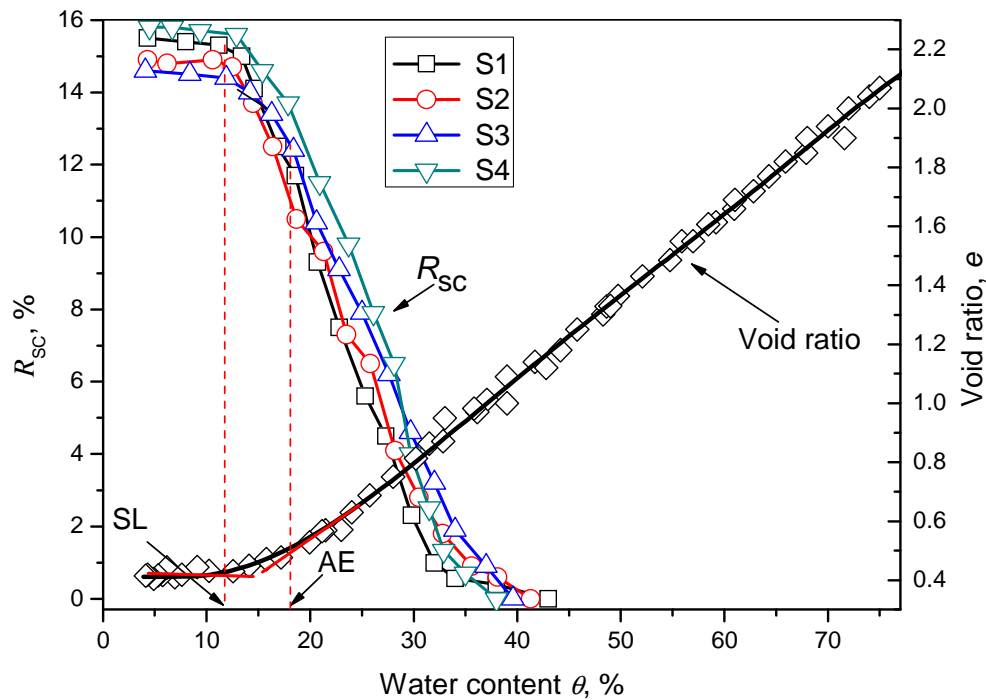
29 Fig. 2 A typical desiccation crack pattern of specimen during the first
30 drying path



31

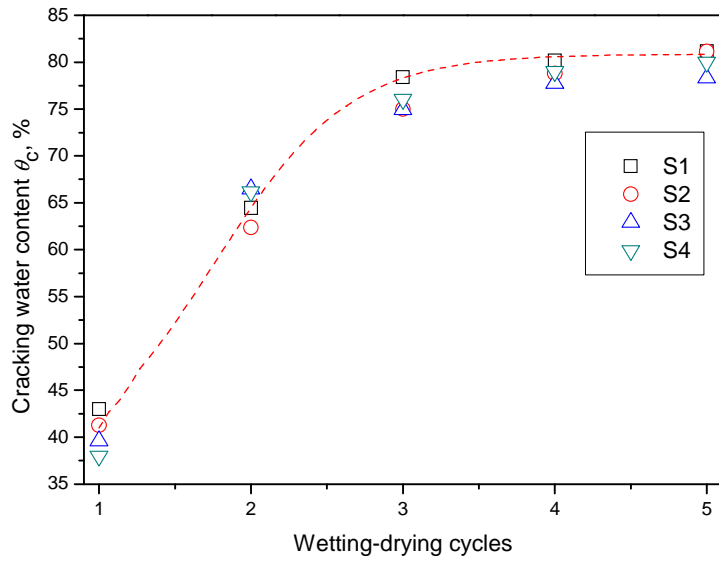
32 Fig. 3 Desiccation curves of the specimens during the first drying path

33

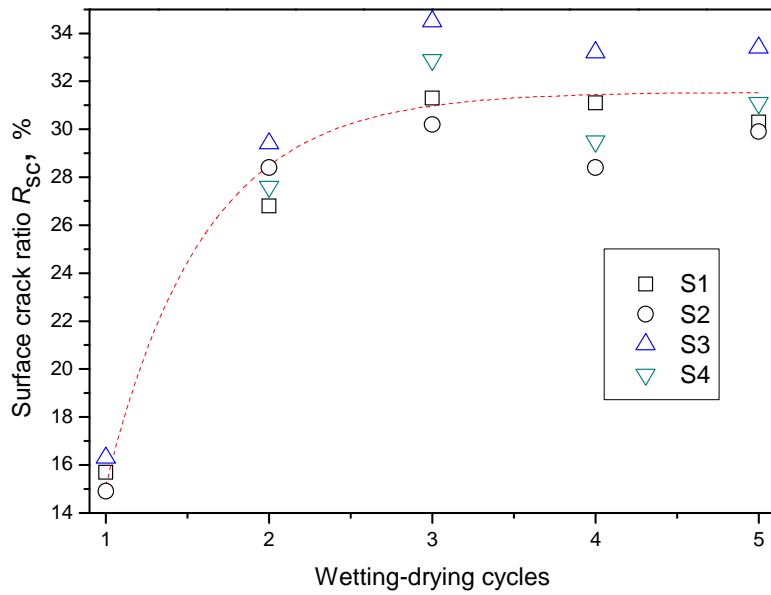


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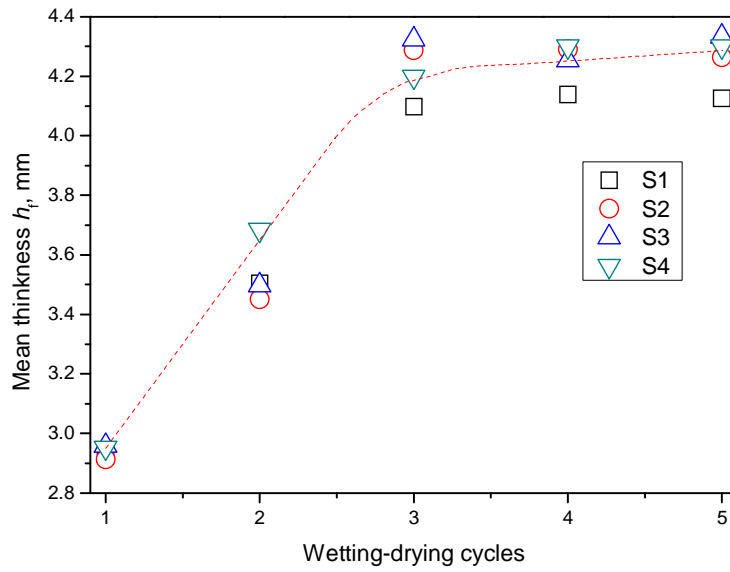
35 Fig. 4 Variation of surface crack ratio R_{sc} and void ratio e with water36 content θ during the first drying path



39 Fig. 5 Cracking water content θ_c of the specimens during each drying path

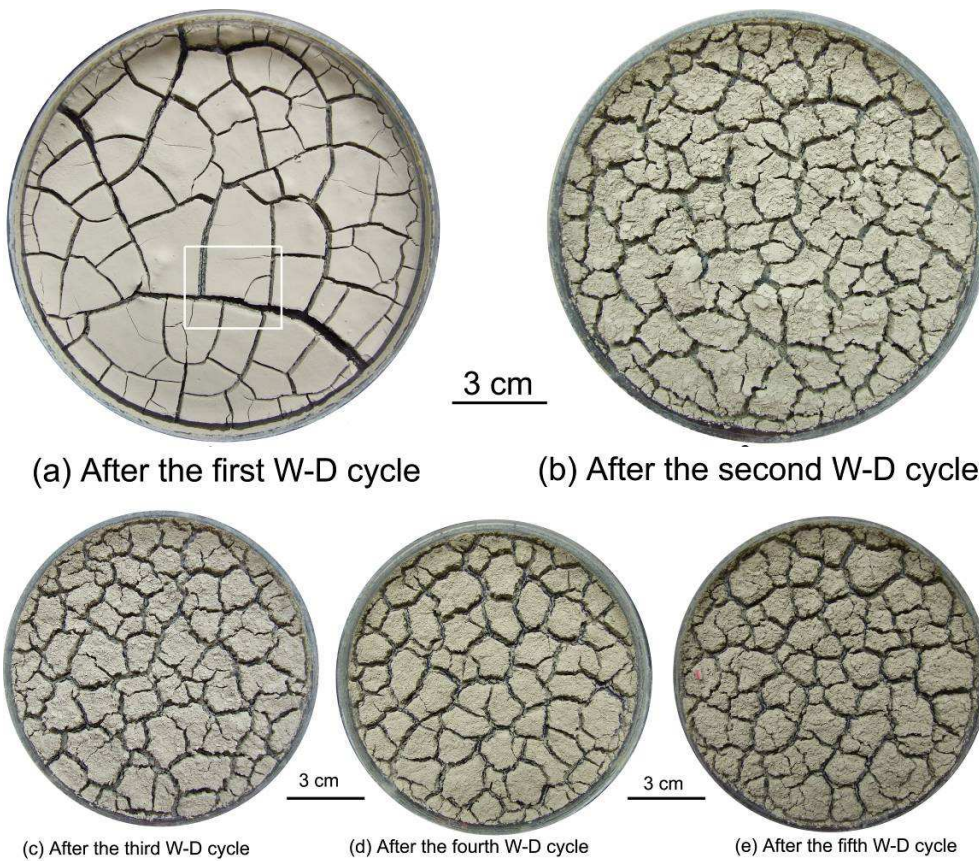


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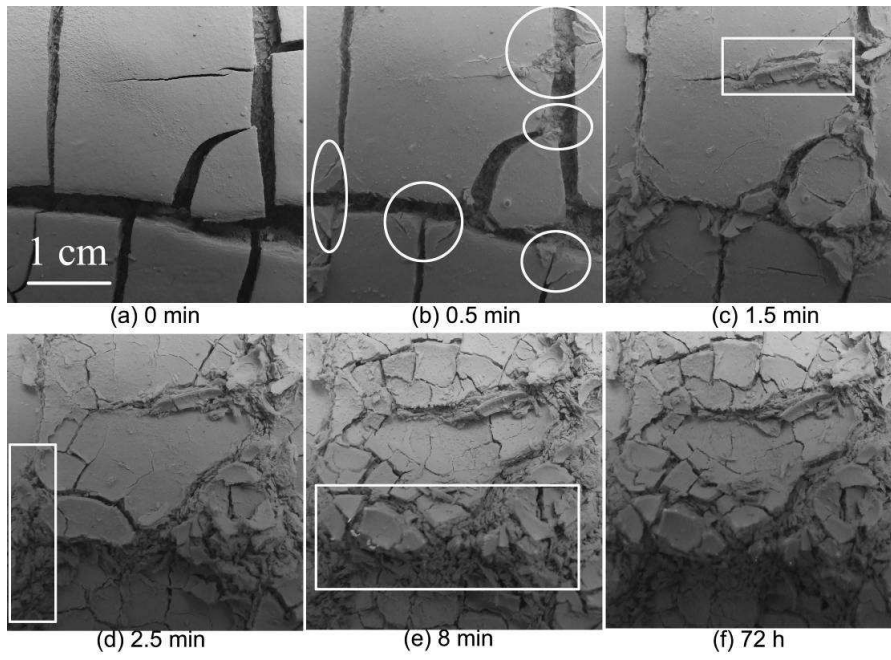


Fig. 9 Evolution of crack pattern during the second wetting



Fig. 10 Evolution of surface cracks during the third wetting path