

A Fully Equivalent Global Pressure Formulation for Three-Phase Compressible Flow

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Abstract: We introduce a new global pressure formulation for immiscible three-phase compressible flows in porous media which is fully equivalent to the original equations, unlike the one introduced in [5]. In this formulation, the total volumetric flow of the three fluids and the global pressure follow a classical Darcy law, which simplifies the resolution of the pressure equation. However, this global pressure formulation exists only for Total Differential (TD) three-phase data, which depend only on two functions of saturations and global pressure: the global capillary pressure and the global mobility. Hence we introduce a class of interpolation which constructs such TD-three-phase data from any set of three two-phase data (for each pair of fluids) which satisfy a TD-compatibility condition.

Key-words: Three-phase flow in porous media, global pressure.

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Une formulation des écoulements triphasiques en pression globale et totalement équivalente

Résumé : Nous introduisons une nouvelle formulation en pression globale pour les écoulements triphasiques immiscibles compressibles en milieu poreux. A la différence de [5], cette formulation est totalement équivalente aux équations physiques originales, mais elle permet toujours d'exprimer le flux volumétrique total des trois fluides à l'aide de la pression globale par une loi de Darcy classique, ce qui simplifie la résolution de l'équation en pression. Cette formulation n'existe cependant que pour des perméabilités triphasiques satisfaisant une condition de Différentielle Totale, qui ne dépendent plus que de deux fonctions des saturations et de la pression globale : la pression capillaire globale et la mobilité globale. C'est pourquoi nous introduisons une famille d'interpolation permettant de construire de telles perméabilités à partir de la connaissance de trois jeu de données diphasiques (un pour chaque paire de fluides) vérifiant une condition de compatibilité.

Mots-clés : Ecoulement triphasique en milieu poreux.

1 Introduction

The numerical simulation of three-phase immiscible compressible flows in porous media requires the knowledge of three-phase relative permeabilities and capillary pressures. In practice, experimental values for these data are available only on the boundary of the ternary diagram, i. e. for the three two phase flows corresponding to each pair of fluids. The three-phase relative permeabilities are then derived by interpolation from these sets of two-phase data (see for example [8]). The existence of various interpolation formula is in itself a sign that none of these formula is the ultimate truth.

We take advantage in this paper of this lack of experimental three-phase data, and introduce a new *class of TD-interpolations*, which is designed to simplify the numerical simulation of the flow by allowing the use of a *global pressure formulation*.

The global pressure reformulation of the original flow equation was introduced for incompressible two-phase flows in [3, 1], and generalized, under the approximation that the volume factors be evaluated at the new global pressure instead of the corresponding phase pressure, to *compressible* two and three-phase flows in [5]. For three-phase flows (both incompressible and compressible), the original global pressure formulation required that the three-phase relative permeabilities and capillary pressures satisfy a *Total Differential (TD)-condition*. An algorithm for the determination of such *TD-three-phase data* was given in [5] and implemented in [4, 7], but its complexity has limited the use of the global pressure in numerical simulation codes. Nevertheless, comparison with other approaches [6] show the computational effectiveness of this approach when it can be put to work, which may explain the current revival of interest for the global pressure : the approximation on the volume factors required in the original global pressure formulation of compressible flows has been lifted recently for two phase flows in [2] in an independantly work, and is lifted for three-phase flows in the present paper.

So we first show that, under an integral *Total Differential (TD)-condition* linking three-phase relative permeabilities and capillary pressures, the total volumetric flow of the three phases is governed by a single phase Darcy-like law for a *new global pressure* variable P . This new formulation is fully equivalent to the original three-phase compressible equations, in opposition to the formulation proposed in [5]. Three-phase relative permeabilities and capillary pressures which satisfy the TD-condition we be called *TD-three-phase data*.

Next we show that any collection of three two-phase data sets (defined on the boundary $\partial\mathbb{T}$ of the ternary diagram \mathbb{T}) which is the trace of some TD-three-phase data (defined on \mathbb{T}) satisfies necessarily a *TD-compatibility condition*.

Finally, we study the *TD-interpolation* of a collection of three two-phase data sets which satisfies the TD-compatibility condition : we show that TD-interpolation reduces to the choice of two functions over the ternary diagram (one global capillary pressure, to be defined in section 4, and one global mobility) which satisfy boundary conditions determined by the three given two-phase data sets. This is expected to make more easy the numerical determination of TD-three-phase data.

2 The three-phase immiscible compressible equations

Let the fluids be numbered in order of decreasing wettability, and denote by upper case letters S_j, P_j, \dots saturation and pressure distributions (function of the space and time variables x, t), and by lower case letters s_j, p_j, \dots saturation and pressure levels (real positive numbers). It will be convenient to use vector notations for the saturations :

$$\begin{cases} S = (S_1, S_3) & = \text{vector of saturation fields ,} \\ s = (s_1, s_3) & = \text{vector of saturation levels ,} \end{cases} \quad (1)$$

and to denote by \mathbb{T} and $\partial\mathbb{T}$ the ternary diagram and its boundary :

$$\begin{cases} \mathbb{T} & = \{s \text{ such that } 0 \leq s_j \leq 1, j = 1, 3, s_1 + s_3 \leq 1\} \\ \partial\mathbb{T} & = \{s \in \mathbb{T} \text{ such that } s_1 = 0 \text{ or } s_3 = 0 \text{ or } s_1 + s_3 = 1\} \end{cases} \quad (2)$$

2.1 Conservation laws :

For each phase $j = 1$ (water), 2 (oil), 3 (gas) one has :

$$\frac{\partial}{\partial t} \{ \phi(x, P_{\text{pore}}) B_j(P_j) S_j \} + \nabla \cdot \varphi_j = 0 \quad , \quad j = 1, 2, 3. \quad (3)$$

where:

$$\begin{cases} x & = \text{vector of spatial coordinates,} \\ \phi(x, p) & = \text{porosity at location } x \text{ and pressure } p, \\ P_{\text{pore}} & = \text{pore pressure, } \simeq P_1, P_2, \text{ or } P_3. \end{cases} \quad (4)$$

and where, for each phase $j = 1, 2, 3$:

$$\begin{cases} P_j & = P_j(x, t) & = \text{pressure,} \\ S_j & = S_j(x, t) & = \text{reduced saturation , } S = S_1, S_2, S_3 \\ & & 0 \leq S_j \leq 1, S_1 + S_2 + S_3 = 1, \\ \varphi_j & = \varphi_j(x, t) & = \text{volumetric flow vector at reference pressure.} \\ B_j(p_j) & = \rho_j(p_j) / \rho_j^{\text{ref}} & = \text{volume factor at pressure } p_j, \\ \text{where : } \rho_j(p_j) & = \text{density, (mass per unit volume) at pressure } p_j, \\ & \rho_j^{\text{ref}} & = \text{density at reference pressure,} \end{cases} \quad (5)$$

2.2 Muskat law :

The volumetric flow vector of each phase $j = 1, 2, 3$ at reference pressure is given by :

$$\varphi_j = -K(x) d_j(P_j) kr_j(S) (\nabla P_j - \rho_j(P_j) g \nabla Z) \quad (6)$$

where:

$$\begin{cases} K(x) & = \text{absolute permeability at location } x, \\ d_j(p_j) & = B_j / \mu_j = \text{phase mobility at pressure } p_j, \\ \mu_j(p_j) & = \text{phase viscosity at pressure } p_j, \\ kr_j(s) & = \text{phase relative permeability at saturation levels } s, \\ g & = \text{gravity constant ,} \\ Z(x) & = \text{depth of location } x. \end{cases} \quad (7)$$

2.3 Capillary pressure law :

$$\begin{cases} P_1 - P_2 &= P_c^{12}(S_1) , \\ P_3 - P_2 &= P_c^{32}(S_3) , \end{cases} \quad (8)$$

where:

$$\begin{cases} P_c^{12}(s_1) &= \text{water-oil capillary pressure at water saturation level } s_1, \\ P_c^{32}(s_3) &= \text{gas-oil capillary pressure at gas saturation level } s_3. \end{cases} \quad (9)$$

3 Classical resolution : “pressure equation”

The numerical resolution of equations (3)(6)(8) is usually done by solving one “pressure equation”, to be defined in the next section, with respect of one of the phase pressure, say P_2 , and two of the “saturation equations” (3), say with respect to S_1 and S_3 .

3.1 Forming the “pressure” equation :

Summing up the three conservation laws (3) gives :

$$\frac{\partial}{\partial t} \{ \phi(x, P_{\text{pore}}) \sum_{j=1}^3 B_j(P_j) S_j \} + \nabla \cdot q = 0 , \quad (1)$$

where q is the global volumetric flow vector:

$$q \stackrel{\text{def}}{=} \sum_{j=1}^3 \varphi_j = -K\lambda \{ \nabla P_2 + f_1 \nabla P_c^{12} + f_3 \nabla P_c^{13} - \rho g \nabla Z \} . \quad (2)$$

Here λ, f_1, f_3, ρ are the global mobility, the water and oil fractional flows and the global density expressed as function of the *oil pressure level* p_2 , using the capillary pressure laws (8) :

$$\lambda(s, p_2) = kr_1(s) d_1(p_2 + P_c^{12}(s_1)) + kr_2(s) d_2(p_2) + kr_3(s) d_3(p_2 + P_c^{32}(s_3)) \quad (3)$$

$$f_j(s, p_2) = kr_j(s) d_j(p_2 + P_c^{j2}(s_j)) / \lambda(s, p_2) , \quad j = 1, 3 , \quad (4)$$

$$f_2(s, p_2) = 1 - f_1(s, p_2) - f_3(s, p_2) , \quad (5)$$

$$\rho(s, p_2) = \sum_{j=1,2,3} f_j(s, p_2) \rho_j(p_j) . \quad (6)$$

In this approach, equations (1)(2) have to be solved for the oil pressure P_2 at each time step..

3.2 Difficulties :

Equation (1)(2) is not a classical pressure equation, because of the gradient of capillary pressure terms in (2), which makes its discretization delicate. Moreover, the individual phase pressures can be singular, as it is shown on figure 1, for a two-phase problem : the difference between water and oil pressure is the capillary pressure, whose derivative is infinite at residual saturations - hence the water and oil pressure cannot be both regular across a water-oil front. So the choice of P_2 as numerical unknown is likely to require a fine or adaptive mesh.

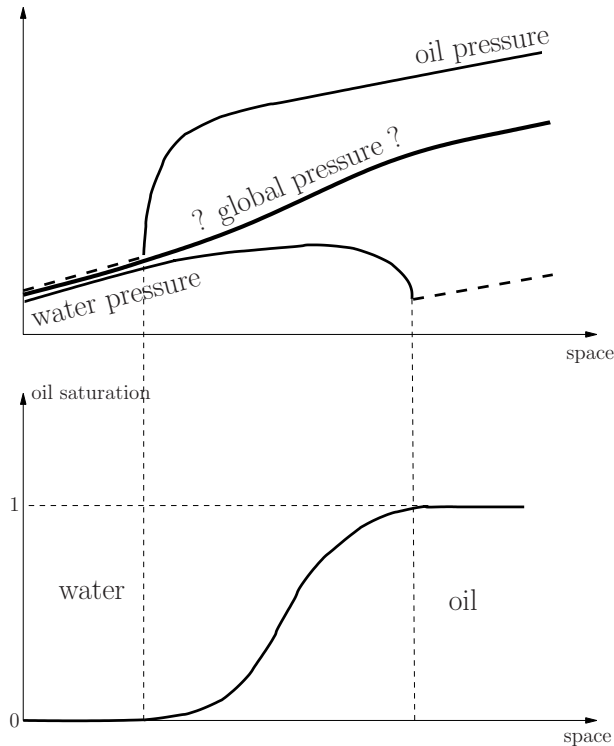


Figure 1: Behaviour of the individual phase pressure across a front

3.3 Let us have a dream ...

Could it be possible to find a “global pressure” field P such that :

- P is smooth, in opposition to the individual phase pressures,
- P governs the global volumetric flow of the three fluids :

$$q = -Kd\{\nabla P - \rho g \nabla Z\} , \quad (7)$$

where now d and ρ denote the global mobility and density at a global pressure level p - compare with equation (3)(6) :

$$d(s, p) \stackrel{\text{def}}{=} \lambda(s, p_2) \quad , \quad \rho(s, p) \stackrel{\text{def}}{=} \rho(s, p_2) , \quad (8)$$

(we have kept for simplicity the same notation for the global density as function of p_2 and p)

4 Searching for a global pressure P

Comparison of (2)(7) suggests to search for a new dependant *global pressure* variable P by setting :

$$P = P_2 + P_{cg}(S, P) \quad (1)$$

is satisfied. Notice that the computation of P from S, P_2 is required only for the determination of the initial global pressure distribution; after that, during the course of the computation, the numerical code knows only P , and it is P_2 which is computed from P and S using (1).

Hence a global pressure formulation will exist as soon as one can find a *global capillary pressure function* $s, p \rightsquigarrow P_{cg}(s, p)$ which satisfies the three conditions (5)(6)(8).

4.1 Satisfying condition (5) :

Condition (6) will constrain the global capillary pressure up to a constant, so we can fix its value at one point of the ternary diagram. Choosing :

$$P_{cg}(1, 0, p) = 0 \quad \text{for } P_{\min} \leq p \leq P_{\max} , \quad (9)$$

will imply the desired property (5) as it follows immediately from (19) below.

4.2 Satisfying condition (6) :

Taking successively $S_1(x, t) = \text{constant}$ and $S_3(x, t) = \text{constant}$ shows that (6) will be satisfied if and only if the global capillary function satisfies :

$$\begin{cases} \frac{\partial P_{cg}}{\partial s_1}(s, p) = f_1(s, p - P_{cg}(s, p)) \frac{dP_c^{12}}{ds_1}(s_1) , \\ \frac{\partial P_{cg}}{\partial s_3}(s, p) = f_3(s, p - P_{cg}(s, p)) \frac{dP_c^{32}}{ds_3}(s_3) , \end{cases} \quad (10)$$

for all $s \in \mathbb{T}$, $P_{\min} \leq p \leq P_{\max}$.

This relation implies that, if it exists, P_{cg} satisfies a differential equation along any smooth curve \mathcal{C} of \mathbb{T} . Hence the existence of a global capillary pressure function P_{cg} satisfying (10) amounts to the following *Total Differential (TD)* condition :

$$\begin{cases} \text{for any } s \in \mathbb{T}, P_{\min} \leq p \leq P_{\max} \text{ and any smooth curve } \mathcal{C} : [0, 1] \rightsquigarrow \mathbb{T}, \text{ such} \\ \text{that } \mathcal{C}(0) = (1, 0) , \mathcal{C}(1) = s, \text{ the solution of the differential equation :} \\ \frac{d\beta}{dt} = f_1(\mathcal{C}, p - \beta) \frac{dP_c^{12}}{ds_1}(\mathcal{C}_1) \mathcal{C}'_1 + f_3(\mathcal{C}, p - \beta) \frac{dP_c^{32}}{ds_3}(\mathcal{C}_3) \mathcal{C}'_3 , \beta(0) = 0 \\ \text{satisfies } \beta(1) = s \text{ independantly of } \mathcal{C}. \end{cases} \quad (11)$$

When this TD-condition is satisfied, the global capillary pressure satisfying (5)(6) is given by :

$$P_{cg}(s, p) = \beta(1). \quad (12)$$

An *alternative formulation of the TD-condition* is obtained by requiring that the second derivative $\partial^2 P_{cg} / \partial S_1 \partial S_3$ takes the same value when computed from either line of (10) :

$$\begin{cases} \text{There exists a function } s, p \rightsquigarrow P_{cg}(s, p) \text{ s.t. for all } s \in \mathbb{T} , P_{\min} \leq p \leq P_{\max} : \\ \frac{\partial}{\partial s_3} \left(f_1(s, p - P_{cg}(s, p)) \frac{dP_c^{12}}{ds_1}(s_1) \right) = \frac{\partial}{\partial s_1} \left(f_3(s, p - P_{cg}(s, p)) \frac{dP_c^{32}}{ds_3}(s_3) \right) . \end{cases} \quad (13)$$

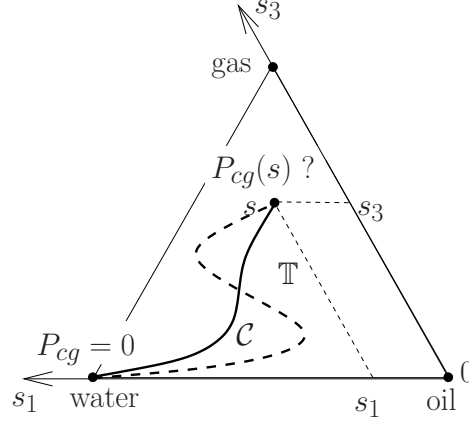


Figure 2: The Total Differential condition for three phase data : $P_{cg}(s, p)$ is required to be independant of the curve \mathcal{C} along which it is computed.

In the approximate global pressure formulation (see [5]), the P_{cg} terms were neglected in the right-hand sides of (10), and hence in (13). So condition (13) could be used to check whether a given set of three-phase data satisfied the TD-condition or not, and to construct fractional flow functions satisfying this condition [4]. This approach cannot be used anymore in the exact formulation given here, where the condition (13) begins with “there exists P_{cg} such that ...” : one has to resort to condition (11) to check if a given set of three-phase data satisfy the TD-condition, and to use a more direct - and hopefully simpler - approach for the construction of TD-three-phase data, which we describe now.

The TD-condition (11) or (13) has the effect of reducing the number of functions which can be chosen freely over the ternary diagram: instead three relative permeabilities kr_1, kr_2, kr_3 which are function of saturations (or equivalently two fractional flows f_1, f_3 and the global mobility λ which are function of saturations $s = (s_1, s_3)$ and oil pressure p_2), one can choose only in a global pressure formulation the *global capillary pressure* P_{cg} and the *global mobility* d which are function of saturation $s = (s_1, s_3)$ and global pressure p .

Based on (10) the fractional flows and relative permeabilities associated to P_{cg} and d are :

$$\nu_j(s, p) = \partial P_{cg} / \partial s_j(s, p) / dP_c^{j2} / ds_j(s_j) \quad , \quad j = 1, 3 \quad (14)$$

$$\nu_2(s, p) = 1 - \nu_1(s, p) - \nu_3(s, p) \quad (15)$$

$$kr_j(s, p) = \nu_j(s, p) d(s, p) / d_j(p - P_{cg}(s, p) + P_c^{j2}(s_j)) \quad j = 1, 3 \quad , \quad (16)$$

$$kr_2(s, p) = (1 - \nu_1(s, p) - \nu_3(s, p)) d(s, p) / d_2(p - P_{cg}(s, p)) \quad , \quad (17)$$

where we have used the notation ν_j for the fractional flows considered as *function of the global pressure* p . They are related to the fractional flows f_j as function of the oil pressure p_2 by:

$$\nu_j(s, p) = f_j(s, p - P_{cg}(s, p)) \quad , \quad j = 1, 2, 3 \quad . \quad (18)$$

4.3 Satisfying condition (8) :

Let now the three-phase data satisfy the TD-condition (11), $P_{cg}(s, t)$ be the global capillary pressure defined by (9)(11)(12), $s = (s_1, s_3) \in \mathbb{T}$, $P_{\min} \leq p \leq P_{\max}$ be given, and $\mathcal{C}^1 : t \rightsquigarrow (1 - t + ts_1, 0)$ and $\mathcal{C}^3 : t \rightsquigarrow (s_1, ts_3)$ be the curves shown in figure 3. The functions $\beta^j(t) = P_{cg}(\mathcal{C}^j(t), p)$, $j = 1, 3$ satisfy the differential equations (see (11)) :

$$\begin{cases} \frac{d\beta^1}{dt} = -f_1(1 - t + ts_1, 0, p - \beta^1) \frac{dP_c^{12}}{ds_1}(1 - t + ts_1)(1 - s_1), & \beta^1(0) = 0, \\ \frac{d\beta^3}{dt} = +f_3(s_1, ts_3, p - \beta^3) \frac{dP_c^{32}}{ds_3}(ts_3) s_3, & \beta^3(0) = \beta^1(1). \end{cases} \quad (19)$$

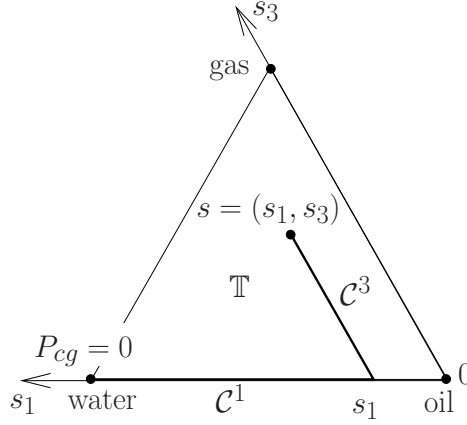


Figure 3: One convenient path for the computation of $\partial P_{cg}/\partial p$.

Derivation of (19) with respect to p shows that the functions $\gamma_j(t) = \partial P_{cg}/\partial p(\mathcal{C}_j(t), p)$ are given by the the differential equations :

$$\begin{cases} \frac{d\gamma^1}{dt} = -\frac{\partial f_1}{\partial p_2}(1 - t + ts_1, 0, p - \beta^1) \frac{dP_c^{12}}{ds_1}(1 - t + ts_1)(1 - s_1)(1 - \gamma^1), & \gamma^1(0) = 0, \\ \frac{d\gamma^3}{dt} = +\frac{\partial f_3}{\partial p_2}(s_1, ts_3, p - \beta^3) \frac{dP_c^{32}}{ds_3}(ts_3) s_3(1 - \gamma^3), & \gamma^3(0) = \gamma^1(1). \end{cases} \quad (20)$$

Both equations in (20) are of the form :

$$\frac{d\gamma}{dt} = \alpha(t)(1 - \gamma), \quad \gamma(0) = \gamma_0 < 1 \quad \iff \quad \gamma(t) = 1 - (1 - \gamma_0) \exp\left\{-\int_0^t \alpha(\tau) d\tau\right\}, \quad (21)$$

so that :

$$\frac{\partial P_{cg}}{\partial p}(s, p) = \gamma^3(1) = 1 - \exp\left\{-\int_0^1 (\alpha^1(\tau) + \alpha^3(\tau)) d\tau\right\}, \quad (22)$$

which shows that *the coefficient $1 - \partial P_{cg}/\partial p$ in the global Darcy law ($\tilde{\gamma}$) is always strictly positive.*

The stability condition (8) that $|\partial P_{cg}/\partial p| < 1$ is then equivalent to :

$$\forall s \in \mathbb{T}, \forall p \in [P_{\min}, P_{\max}] \quad , \quad \exp\left\{-\int_0^1 (\alpha^1(\tau) + \alpha^3(\tau))d\tau\right\} < 2. \quad (23)$$

Derivation of the fractional flows $f_1(s, p_2)$ and $f_3(s, p_2)$ given by (3)(4) with respect to p_2 gives the following expressions for α^1 and α^3 (remember : $kr_3 = 0$ on \mathcal{C}^1) :

$$\alpha^1(t) = -\frac{kr_1 d_1 kr_2 d_2 \left(\frac{d'_1}{d_1} - \frac{d'_2}{d_2}\right)}{(kr_1 d_1 + kr_2 d_2)^2} \times \frac{dP_c^{12}}{ds_1} \times (1 - s_1), \quad (24)$$

$$\alpha^3(t) = +\frac{kr_3 d_3 kr_1 d_1 \left(\frac{d'_3}{d_3} - \frac{d'_1}{d_1}\right) + kr_3 d_3 kr_2 d_2 \left(\frac{d'_3}{d_3} - \frac{d'_2}{d_2}\right)}{(kr_1 d_1 + kr_2 d_2 + kr_3 d_3)^2} \times \frac{dP_c^{32}}{ds_3} \times s_3 \quad (25)$$

where kr_j, d_j, d'_j , $j = 1, 2, 3$ and P_c^{j2} , $j = 1, 3$ are evaluated at saturations and phase pressures associated to the point $\mathcal{C}^1(t)$ (for α_1) or $\mathcal{C}^2(t)$ (for α_2) of \mathbb{T} at the given global pressure level p .

When the fluid densities satisfy :

$$\left\{ \begin{array}{l} \forall s \in \mathbb{T}, \forall p \in [P_{\min}, P_{\max}] : \\ \frac{d'_3}{d_3}(p - P_{cg}(s, p) + P_c^{32}(s_3)) \geq \frac{d'_2}{d_2}(p - P_{cg}(s, p)) \geq \frac{d'_1}{d_1}(p - P_{cg}(s, p) + P_c^{12}(s_1)), \end{array} \right. \quad (26)$$

$\alpha^1(\tau)$ and $\alpha^3(\tau)$ are positive, so that :

$$\forall s \in \mathbb{T}, \forall p \in [P_{\min}, P_{\max}] \quad , \quad 0 \leq \frac{\partial P_{cg}}{\partial p}(s, p) < 1, \quad (27)$$

and the stability condition (8) is satisfied.

Naturally, (26) is only a sufficient conditions for (8). In practice, implementation of the global pressure formulation requires the determination of $\partial P_{cg}/\partial p$ over the ternary diagram \mathbb{T} and the global pressure range of interest $[P_{\min}, P_{\max}]$, for example by formula (22)(24)(25), so one can check directly on $\partial P_{cg}/\partial p$ if condition (8) is satisfied. In the case where condition (8) is not satisfied, it is not known whether this limitation is due to the global pressure formulation, or is the sign that the original equations are not anymore well-posed, or change of type.

Remark 1 In the case of a water-oil-gas system, one has $d'_1 = d'_2 = 0$, and condition (26) is satisfied : the global capillary pressure, when it exists, satisfies always (27). In that case, $\partial P_{cg}/\partial p = 0$ on the water - oil side of \mathbb{T} , so that $\alpha^1 = 0$ and (22) simplifies somewhat. ■

5 TD-interpolation of two-phase data given on the sides of the ternary diagram \mathbb{T}

Let two-phase relative permeabilities and capillary pressure curves be given on the boundary $\partial\mathbb{T}$ of \mathbb{T} for each system of two-fluids :

$$\begin{cases} \text{water - oil} : & s_1 \rightsquigarrow kr_1^{12}(s_1), kr_2^{12}(s_1) \quad P_c^{12}(s_1), \\ \text{water - gas} : & s_1 \rightsquigarrow kr_1^{13}(s_1), kr_3^{13}(s_1) \quad P_c^{13}(s_1) = P_c^{12}(s_1) - P_c^{32}(1 - s_1), \\ \text{gas - oil} : & s_3 \rightsquigarrow kr_3^{23}(s_3), kr_2^{23}(s_3) \quad P_c^{32}(s_3), \end{cases} \quad (1)$$

as well as the three phase mobility functions (see (7)) :

$$p_j \rightsquigarrow d_j(p_j), \quad j = 1, 2, 3, \quad (2)$$

The question arises of whether one can find, for each given global pressure level $P_{\min} \leq p \leq P_{\max}$, three-phase relative permeabilities $s \in \mathbb{T} \rightsquigarrow kr_j(s, p) \in \mathbb{R}$, $j = 1, 2, 3$ (compare with (7)) which ...

1. honor the two-phase data on $\partial\mathbb{T}$,
2. and satisfy the TD-condition (11) on \mathbb{T} .

Satisfying condition 1 and 2 amounts to search for a global capillary pressure function $(s, p) \rightsquigarrow P_{cg}(s, p)$ and a global mobility function $(s, p) \rightsquigarrow d(s, p)$ such that the fractional flow $\nu_j(s, p)$ defined by (10) :

$$\begin{cases} \nu_1(s, p) &= \frac{\partial P_{cg}}{\partial s_1}(s, p) / \frac{dP_c^{12}}{ds_1}(s_1), \\ \nu_3(s, p) &= \frac{\partial P_{cg}}{\partial s_3}(s, p) / \frac{dP_c^{32}}{ds_3}(s_3), \end{cases} \quad (3)$$

produce three-phase relative permeabilities $kr_j(s, p)$:

$$\begin{cases} kr_1(s, p) &= \frac{\nu_1(s, p)}{d_1(p - P_{cg}(s, p) + P_c^{12}(s_1))} d(s, p), \\ kr_2(s, p) &= \frac{1 - \nu_1(s, p) - \nu_3(s, p)}{d_2(p - P_{cg}(s, p))} d(s, p), \\ kr_3(s, p) &= \frac{\nu_3(s, p)}{d_3(p - P_{cg}(s, p) + P_c^{32}(s_1))} d(s, p), \end{cases} \quad (4)$$

which coincide with the given two phase data (1) on $\partial\mathbb{T}$.

5.1 Determination of $P_{cg}(s, p)$ on $\partial\mathbb{T}$.

Let $P_{\min} \leq p \leq P_{\max}$ be given, and denote by

$$\mathcal{C}^{12}(t) = (1-t, 0) \quad , \quad \mathcal{C}^{23}(t) = (0, t) \quad , \quad \mathcal{C}^{13}(t) = (1-t, t) \quad , \quad 0 \leq t \leq 1 \quad (5)$$

a parameterization of the three edges of $\partial\mathbb{T}$. When it exists, the global capillary pressure $\beta^{ij}(t) = P_{cg}(\mathcal{C}^{ij}(t))$, $i, j = 1, 2, 3$, $i < j$ on $\partial\mathbb{T}$ satisfies, according to (11) :

- along the water-oil-gas sides :

$$\left\{ \begin{array}{l} \frac{d\beta^{12}}{dt} = - \underbrace{f_1^{\text{data}}(1-t, 0, p - \beta^{12})}_{\stackrel{\text{def}}{=} \nu_1^{12, \text{data}}(t, p)} \frac{dP_c^{12}}{ds_1}(1-t) , \beta^{12}(0) = 0 , \\ \frac{d\beta^{23}}{dt} = + \underbrace{f_3^{\text{data}}(0, t, p - \beta^{23})}_{\stackrel{\text{def}}{=} \nu_3^{23, \text{data}}(t, p)} \frac{dP_c^{32}}{ds_3}(t) s_3 , \beta^{23}(0) = \beta^{12}(1) . \end{array} \right. \quad (6)$$

- along the water-gas side :

$$\left\{ \begin{array}{l} \frac{d\beta^{13}}{dt} = - \underbrace{f_1^{\text{data}}(1-t, t, p - \beta^{13})}_{\stackrel{\text{def}}{=} \nu_1^{13, \text{data}}(t, p)} \frac{dP_c^{12}}{ds_1}(1-t) \\ \quad + \underbrace{f_3^{\text{data}}(1-t, t, p - \beta^{13})}_{\stackrel{\text{def}}{=} \nu_3^{13, \text{data}}(t, p)} \frac{dP_c^{32}}{ds_3}(t) , \\ \beta^{13}(0) = 0 , \end{array} \right. \quad (7)$$

where $f_1^{\text{data}}(s, p_2)$ and $f_3^{\text{data}}(s, p_2)$ denote, for $s \in \partial\mathbb{T}$, the two-phase fractional flows as function of the oil pressure derived from the data (1)(2) using two phase versions of (3)(4).

Using the TD-condition (11), one sees that the existence of a global capillary function implies that the two-phase data (1)(2) satisfy necessarily the *TD-compatibility condition*

$$\beta^{23}(1) = \beta^{13}(1) , \quad (8)$$

i.e., using (6)(7) and the two-phase fractional flows $\nu_1^{12, \text{data}}, \nu_3^{23, \text{data}}, \nu_1^{13, \text{data}}, \nu_3^{13, \text{data}}$ defined there :

$$\int_0^1 (\nu_1^{12, \text{data}} - \nu_1^{13, \text{data}}) \frac{dP_c^{12}}{ds_1} = \int_0^1 (\nu_3^{23, \text{data}} - \nu_3^{13, \text{data}}) \frac{dP_c^{32}}{ds_3} = 0 \text{ for } P_{\min} \leq p \leq P_{\max} . \quad (9)$$

This compatibility condition is a constraint on weighted means of the fractional flows, and hence a non-linear constraint on the mean values of the two-phase relative permeability data sets (1). When it is satisfied, one sees that the global capillary function P_{cg} has to satisfy the *Dirichlet boundary condition* :

$$P_{cg} = P_{cg}^{\text{data}} \stackrel{\text{def}}{=} \begin{cases} \beta^{12} & \text{(water-oil edge),} \\ \beta^{13} & \text{(water-gas edge),} \\ \beta^{23} & \text{(gas-oil edge),} \end{cases} \quad (10)$$

5.2 Determination of $\frac{\partial P_{cg}}{\partial n}(s, p)$ on $\partial\mathbb{T}$.

Now that P_{cg} is known on $\partial\mathbb{T}$, equation (10) gives, for $s \in \partial\mathbb{T}$:

$$\left\{ \begin{array}{l} \frac{\partial P_{cg}}{\partial s_1}(s, p) = f_1^{\text{data}}(s, p - P_{cg}^{\text{data}}(s, p)) \frac{dP_c^{12}}{ds_1}(s_1) , \\ \frac{\partial P_{cg}}{\partial s_3}(s, p) = f_3^{\text{data}}(s, p - P_{cg}^{\text{data}}(s, p)) \frac{dP_c^{32}}{ds_3}(s_3) . \end{array} \right. \quad (11)$$

Let then n be the unit outer normal to \mathbb{T} . The normal derivative of P_{cg} on $\partial\mathbb{T}$ is given by :

$$\begin{cases} \frac{\partial P_{cg}}{\partial n} = \frac{\sqrt{3}}{3} \left(\frac{\partial P_{cg}}{\partial s_1} - 2 \frac{\partial P_{cg}}{\partial s_3} \right) & \text{(water-oil edge) ,} \\ \frac{\partial P_{cg}}{\partial n} = \frac{\sqrt{3}}{3} \left(\frac{\partial P_{cg}}{\partial s_1} + \frac{\partial P_{cg}}{\partial s_3} \right) & \text{(water-gas edge) ,} \\ \frac{\partial P_{cg}}{\partial n} = \frac{\sqrt{3}}{3} \left(\frac{\partial P_{cg}}{\partial s_3} - 2 \frac{\partial P_{cg}}{\partial s_1} \right) & \text{(gas-oil edge) ,} \end{cases} \quad (12)$$

Combining (11) and (12) shows that P_{cg} satisfies the *Neumann boundary condition*:

$$\frac{\partial P_{cg}}{\partial n} = \frac{\partial P_{cg}^{\text{data}}}{\partial n} \stackrel{\text{def}}{=} \begin{cases} \frac{\sqrt{3}}{3} \nu_1^{12,\text{data}} \frac{dP_c^{12}}{ds_1} & \text{(water-oil edge),} \\ \frac{\sqrt{3}}{3} \left(\nu_1^{13,\text{data}} \frac{dP_c^{12}}{ds_1} + \nu_3^{13,\text{data}} \frac{dP_c^{32}}{ds_3} \right) & \text{(water-gas edge),} \\ \frac{\sqrt{3}}{3} \nu_3^{23,\text{data}} \frac{dP_c^{32}}{ds_3} & \text{(gas oil edge),} \end{cases} \quad (13)$$

where $\nu_1^{12,\text{data}}$, $\nu_3^{23,\text{data}}$, $\nu_1^{13,\text{data}}$, $\nu_3^{13,\text{data}}$ are defined in (6) (7).

Conversely, let P_{cg} satisfy the Dirichlet and Neumann conditions (10) (13). Then, on the water-oil edge for example, (10) and the first line in (6) implies that $\nu_1(\mathcal{C}^{12}(t), p) = \nu_1^{12,\text{data}}(t, p)$, and (12) (11) and the first line of (13) implies that $\nu_3(\mathcal{C}^{12}(t), p) = 0$ for $0 \leq t \leq 1$. Hence the fractional flows associated to a global capillary function which satisfies (10) (13) honor the data on $\partial\mathbb{T}$.

5.3 Determination of $d(s, p)$ on $\partial\mathbb{T}$.

Now that the global capillary pressure P_{cg}^{data} is known on $\partial\mathbb{T}$, honoring the three sets of two-phase relative permeabilities (1) on $\partial\mathbb{T}$ amounts simply to impose on d the *Dirichlet boundary condition* :

$$d = d^{\text{data}} \quad \text{on } \partial\mathbb{T} , \quad (14)$$

where :

$$d^{\text{data}} \stackrel{\text{def}}{=} \begin{cases} kr_1^{12} d_1(p - P_{cg}^{\text{data}} + P_c^{12}) + kr_2^{12} d_2(p - P_{cg}^{\text{data}}) & \text{(water-oil),} \\ kr_1^{13} d_1(p - P_{cg}^{\text{data}} + P_c^{12}) + kr_3^{13} d_3(p - P_{cg}^{\text{data}} + P_c^{32}) & \text{(gas-water),} \\ kr_3^{23} d_3(p - P_{cg}^{\text{data}} + P_c^{32}) + kr_2^{23} d_2(p - P_{cg}^{\text{data}}) & \text{(gas-oil).} \end{cases} \quad (15)$$

5.4 Determination of P_{cg} and d on the interior of \mathbb{T} .

Conditions (10)(13)(15) are the sole conditions to be satisfied to ensure that the TD-three-phase data derived from P_{cg} and d match the three given sets (1)(2) of two-phase data on $\partial\mathbb{T}$ - provided the latter satisfy the TD-compatibility condition (9).

There is hence a large choice of functions P_{cg} and d to choose from to perform TD-interpolation.

For example, one can use the smoothest functions which satisfy the boundary conditions (10)(13)(15) by setting:

$$\begin{cases} \Delta^2 P_{cg} = 0 & \text{in } \mathbb{T}, \\ P_{cg} = P_{cg}^{\text{data}} & \text{on } \partial\mathbb{T}, \\ \frac{\partial P_{cg}}{\partial n} = \frac{\partial P_{cg}^{\text{data}}}{\partial n} & \text{on } \partial\mathbb{T}, \end{cases} \quad (16)$$

and :

$$\begin{cases} -\Delta d = 0 & \text{in } \mathbb{T}, \\ d = d^{\text{data}} & \text{on } \partial\mathbb{T}. \end{cases} \quad (17)$$

These equation can be solved by finite element over the ternary diagram \mathbb{T} .

One can also try to match some a-priori given three phase target permeability model on the interior of \mathbb{T} , knowing that the match will not be exact, unless the target relative permeabilities happen to satisfy the TD-compatibility condition (11). This requires the implementation of an optimization algorithm.

6 Conclusion

1. When the three-phase relative permeabilities and capillary pressure satisfy the *TD-condition (11)*, a global capillary pressure function $P_{cg}(s, p)$ exists such that *the classical compressible immiscible three-phase flow equations are fully equivalent to a global pressure formulation* : the total volumetric flow q of the three phases and the global pressure $P = P_2 + P_{cg}(S, P)$ follow the global Darcy law (7).
2. In the global Darcy law (7), one has always $1 - \partial P_{cg} / \partial p(s, p) > 0$
3. If the compressibility of the fluids increases when their wettability decreases (condition (26)), one has always $1 > 1 - \partial P_{cg} / \partial p(s, p) > 0$, and the *stability condition (8)* is satisfied, which ensures that one can determine P from P_2 and S . Condition (26)) is always satisfied in water-oil-gas flows where the compressibility of water and oil is neglected.
4. TD-three-phase relative permeabilities can be obtained by interpolation of three sets of two-phase data on the sides of the ternary diagram, provided the two-phase data satisfy the *TD-compatibility condition (9)*. TD-interpolation amounts to choose a global capillary function P_{cg} and a total mobility function d which satisfy boundary conditions (10) (13) (14), but can be chosen freely inside the ternary diagram. This interpolation class takes advantage of the lack of information on actual three-phase data inside the ternary diagram to simplify the numerical simulation of the flow.

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