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Long-term
measurements of
VOC concentrations
by PTR-MS

R. Taipale et al.

Technical Note: Quantitative long-term measurements of VOC concentrations by PTR-MS – measurement, calibration, and volume mixing ratio calculation methods

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Abstract

Proton transfer reaction mass spectrometry (PTR-MS) is a technique for online measurements of atmospheric concentrations, or volume mixing ratios, of volatile organic compounds (VOCs). The aim of this paper is to give a detailed description of our measurement, calibration, and volume mixing ratio calculation methods, which have been designed for long-term stand-alone field measurements by PTR-MS. We also show how the information obtained from a calibration can be used to determine the instrument specific relative transmission curve, which enables quantitative mixing ratio calculation for VOCs which are not present in a calibration gas standard. To illustrate the functionality of our measurement, calibration, and calculation methods, we present a one-month period of ambient mixing ratio data measured in a boreal forest ecosystem at the SMEAR II station in southern Finland. During the measurement period 27 March–26 April 2007, the hourly averages of mixing ratios were 0.1–0.5 ppbv for formaldehyde, 0.2–3.0 ppbv for methanol, 0.04–0.39 ppbv for benzene, and 0.03–1.25 ppbv for monoterpenes.

1 Introduction

Volatile organic compounds (VOCs) are emitted into the atmosphere from a wide variety of natural and anthropogenic sources. VOCs may also be formed in the atmosphere as products of the atmospheric transformations of other VOCs. Globally, biogenic VOC emissions (about 1150 Tg (C) per year) are estimated to be approximately ten times higher than emissions due to human activity, but in urban areas anthropogenic VOCs often dominate (Piccot et al., 1992; Guenther et al., 1995). The largest VOC sources are tropical and extra-tropical forests, which emit especially isoprene, monoterpenes, and methanol. Also biomass burning is a large source on a global scale and leads to emissions of numerous VOCs, including aromatic hydrocarbons, nitriles, and oxygenated compounds (Andreae and Merlet, 2001).

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VOCs play a significant role in tropospheric chemistry in urban, rural, and remote areas. They affect concentrations of the hydroxyl radical (OH), the nitrate radical (NO₃), and ozone, and hence the oxidative capacity of the lower atmosphere (Atkinson and Arey, 2003). VOCs are also involved in the formation and growth of atmospheric aerosol particles (Kulmala et al., 2004; Allan et al., 2006; Tunved et al., 2006), which are an important factor in the climate system, either directly through the absorption and scattering of solar radiation, or indirectly by acting as cloud condensation nuclei. In addition, VOCs may have an effect on the optical properties of aerosol particles (Nozière and Esteve, 2005).

Atmospheric VOC measurements are often based on gas chromatographic analyses of air samples collected on adsorbents, in canisters, or in cryostats. Such measurements are very sensitive and give highly detailed information on the atmospheric VOC composition. Due to the required sampling times, these methods are generally too slow to follow rapid changes in the VOC composition. This disadvantage can be partially overcome by using canisters, which can be filled in a few seconds. However, the acquisition and analysis of canister samples is time consuming and labour-intensive, which limits the amount of data that can be collected in any given period.

Proton transfer reaction mass spectrometry (PTR-MS) is a novel technique for online measurements of atmospheric volume mixing ratios of VOCs (Lindinger et al., 1998a). In the PTR-MS instrument, ambient air is continuously pumped through a drift tube reactor and the VOCs in the sample are ionized in proton transfer reactions with hydronium ions (H₃O⁺). This is a soft ionization method, which often does not lead to fragmentation of the product ions, and the mass of the product ion equals the VOC mass plus one. The reagent and product ions are selected according to their masses by a quadrupole mass spectrometer and detected by a secondary electron multiplier. PTR-MS allows measurements of numerous VOCs with a high sensitivity (10–100 parts per trillion by volume (pptv)) and a fast response time (0.1–10 s). The technique does not require any sample treatment, such as drying or pre-separation, and is thus suitable for oxygenated VOCs, which are difficult to detect with other methods. Since PTR-

MS determines only the masses of the product ions, different VOCs with the same mass cannot be distinguished. Therefore, a lot of experimental work has been done to characterize the specificity of PTR-MS for several VOCs (e.g., [de Gouw et al., 2003a](#); [Warneke et al., 2003](#)).

PTR-MS has been used for field and laboratory measurements since the late nineties. Over the years, it has proven to be a valuable tool in atmospheric research (for a review, see [de Gouw and Warneke, 2007](#)). For example, PTR-MS has been utilized in ambient mixing ratio measurements in urban, rural, and remote areas using aircraft-, ship-, vehicle-, or ground-based platforms (e.g., [Crutzen et al., 2000](#); [Holzinger et al., 2001](#); [Wisthaler et al., 2002](#); [de Gouw et al., 2003b, 2004](#); [Karl et al., 2003](#); [Ammann et al., 2004](#); [Jiang et al., 2005](#); [Warneke et al., 2006](#)), in plant chamber experiments to study leaf or shoot scale emissions of VOCs (e.g., [Fall et al., 1999](#); [Karl et al., 2002a](#); [Hayward et al., 2004](#)), in micrometeorological ecosystem scale flux measurements with eddy covariance techniques (e.g., [Karl et al., 2001, 2002b](#); [Rinne et al., 2001](#); [Warneke et al., 2002](#); [Spirig et al., 2005](#); [Brunner et al., 2007](#)), and in laboratory studies of VOC chemistry and aerosol particle formation (e.g., [Wisthaler et al., 2001](#); [Paulsen et al., 2005](#); [Lee et al., 2006a,b](#); [Vartiainen et al., 2006](#)). Much has been learned also about the performance, sensitivity, and specificity of the PTR-MS instrument (e.g., [Hayward et al., 2002](#); [de Gouw et al., 2003a,b](#); [Tani et al., 2003, 2004](#); [Warneke et al., 2003](#); [Ammann et al., 2004](#); [Steinbacher et al., 2004](#)).

Most of the field work with PTR-MS has been conducted in intensive short-term measurement campaigns. In these campaigns, other VOC measurement techniques have often been applied simultaneously with PTR-MS, which has helped the validation and interpretation of the PTR-MS data. The approach to long-term stand-alone field measurements by PTR-MS has to be straightforward to facilitate the acquisition and analysis of the data. It is important that the measurement, calibration, and mixing ratio calculation methods are systematic, practical, and as automatic as reasonable. The PTR-MS instrument has to be calibrated regularly to achieve and maintain the accuracy needed in atmospheric VOC measurements. However, in many cases there are no

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calibration gas standards available for all VOCs measured with PTR-MS. Therefore, it is beneficial if the information obtained from a calibration can be utilized to get quantitative results also for the compounds which are not present in a calibration gas standard.

Our group at the University of Helsinki has been using PTR-MS since 2004 and we have focused on long-term field measurements of biogenic VOCs. The experimental work has been carried out in a boreal forest ecosystem at the SMEAR II (Station for Measuring Ecosystem-Atmosphere Relations II) measurement station in southern Finland (Hari and Kulmala, 2005). Rinne et al. (2005, 2007) have reported the first results from ambient mixing ratio measurements and micrometeorological flux measurements with the disjunct eddy covariance technique. Ruuskanen et al. (2005) have presented a dynamic shoot chamber system, which is suitable for field experiments and combines PTR-MS measurements of VOC emissions with measurements of other trace gases and environmental variables that contribute to the gas exchange of trees.

The aim of this paper is to give a detailed description of our measurement, calibration, and volume mixing ratio calculation methods, which have been designed for long-term stand-alone field measurements by PTR-MS. First, we describe the measurement and calibration setups and routines, and next, we explicitly present the method for calculating mixing ratios. We show how the data from a calibration can be used to determine the sensitivity of the instrument for VOCs in a calibration gas standard and the instrument specific relative transmission curve. This curve enables quantitative mixing ratio calculation for VOCs not present in the gas standard. Finally, to illustrate the functionality of all these methods, we present a one-month period of ambient mixing ratio data for formaldehyde, methanol, benzene, and monoterpenes. The three latter compounds were present in our calibration gas standard while the first one was not. A longer time series will be presented in an accompanying paper¹. These measurements were part of an EUCAARI (European Integrated Project on Aerosol, Cloud,

¹Ruuskanen, T. M., Taipale, R., Rinne, J., Kajos, M. K., Hakola, H., Pohja, T., and Kulmala, M.: Quantitative long-term measurements of VOC concentrations by PTR-MS – Annual cycle of ambient concentrations at a boreal forest site, in preparation, 2008.

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Climate, and Air Quality Interactions) measurement campaign, which was carried out at the SMEAR II station in March–June 2007.

2 Methods

2.1 Measurement site

5 The measurements were conducted at the SMEAR II (Station for Measuring Ecosystem–Atmosphere Relations II) measurement station of the University of Helsinki. The research at the station consists of continuous and comprehensive long-term measurements to study energy and material flows between the forest ecosystem and the atmosphere at different temporal and spatial scales (e.g., [Hari and Kulmala, 2005](#)). The station is located in the south boreal vegetation zone at Hyytiälä, southern Finland (61°51′ N, 24°17′ E, 181 m a.s.l.), about 200 km to the north-west from Helsinki. The largest city near the station is Tampere, located 50 km to the south-west and having about 200 000 inhabitants. A detailed description of the station has been given by [Vesala et al. \(1998\)](#) and [Kulmala et al. \(2001\)](#).

15 The station is surrounded by a rather homogeneous 46-year-old Scots pine (*Pinus sylvestris*) forest. Spruce dominated forest covers 26% of the area of 1600 km² around the station. Other major land use categories are pine dominated forest (23%), mixed forest (21%), water bodies (13%), and agriculture (10%) (for details, see [Haapanala et al., 2007](#)). In addition to the ambient mixing ratio and shoot and ecosystem scale emission measurements with PTR-MS ([Rinne et al., 2005, 2007](#); [Ruuskanen et al., 2005](#)), several VOC measurements have been conducted at the SMEAR II station using gas chromatographic analyses of air samples collected on adsorbents or in canisters (e.g., [Rinne et al., 2000](#); [Janson and de Serves, 2001](#); [Hakola et al., 2003, 2006](#); [Tarvainen et al., 2005](#)).

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2.2 Measurement setup and procedure

Our measurement setup consisted of a proton transfer reaction mass spectrometer (PTR-MS, Ionicon Analytik GmbH), a sampling system, and a calibration system (Fig. 1). The setup was installed in an air-conditioned measurement cabin. There were three sampling lines in the sampling system and they were used for ambient mixing ratio measurements at different heights. The lowest sampling height (4 m) was located in the trunk space of the canopy, the middle one (14 m) in the crown space of the canopy, and the highest one (22 m) above the top of the canopy. The sampling lines were attached to a measurement tower next to the cabin and heated a few degrees warmer than ambient air with Teflon-coated heating cables. All lines were 30 m long, their inner diameter was 8 mm, and they were made of Teflon (PTFE). A continuous flow of 17.5 l min^{-1} was used in each line.

A side flow of 0.1 l min^{-1} was taken from the sampling lines into the PTR-MS via a 1.3 m long PTFE tubing, which had an inner diameter of 1.6 mm. A PTFE filter ($1 \mu\text{m}$ pore size, LI-COR, Inc., part number 9967-008) was installed in front of the PTR-MS inlet to prevent particles from entering the instrument. Solenoid valves (ETFE valve body, Bürkert GmbH & Co., type 117) were used to switch between the sampling lines. The valves were controlled through the analog outputs of the PTR-MS.

The PTR-MS was operating continuously during the EUCAARI measurement campaign, which was carried out in March–June 2007. In this paper, we present ambient mixing ratio data from the period 27 March–26 April. The operating parameters of the PTR-MS were held constant during the measurement period, except for the secondary electron multiplier (SEM) voltage, which was optimized before every calibration (see Sect. 2.3). The drift tube pressure, temperature, and voltage were 2.0 hPa, 50°C , and 450 V, respectively. The parameter E/N was about 106 Td and the reaction time was about $120 \mu\text{s}$ (see Sect. 2.4).

The measurement procedure was controlled with the Balzers Quadstar 422 software of the PTR-MS and it contained three hour-long sequences. Every third hour was allo-

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cated for the ambient mixing ratio measurements at the three sampling heights and for mass scan measurements at 14 m above the ground. The other two sequences were allocated for ecosystem scale flux measurements with the micrometeorological disjunct eddy covariance method and for shoot scale flux measurements with a dynamic chamber method.

In the ambient mixing ratio measurements, five PTR-MS measurement cycles were conducted using the same sampling height and after that the height was switched. This sampling cycle was repeated five times an hour. The PTR-MS measurement cycle consisted of 22 masses and 18 of them were related to VOCs (Table 1). The measurement cycle length was 38 s and the integration, or dwell, time was 2 s for each VOC-related mass. To determine VOC background signals of the PTR-MS, zero air measurements, where VOC-free air was fed to the instrument (see Sect. 2.3), were conducted every third hour within the ecosystem scale flux measurement sequence, right before the ambient mixing ratio measurements. Zero air was measured for about 8 min (12 cycles) at a time and the integration time was 2 s for each VOC-related mass.

2.3 Calibration setup and procedure

The calibration setup (Fig. 1) consisted of a calibration gas standard (Apel-Riemer Environmental, Inc.) and a zero air generator (catalytic converter, Parker Hannifin Corp., ChromGas Zero Air Generator 3501). The calibration gas standard contained 16 VOCs in nitrogen and the mixing ratio of each VOC was about 1 ppmv (part per million by volume; Table 2). Ambient air was fed with an oil-free piston pump (Gardner Denver Thomas, Inc., model number 688CGHI32) through a PTFE filter (1 μ m pore size, LI-COR, Inc., part number 9967-008) to the zero air generator to produce VOC-free air that was used in calibration measurements to dilute the standard gas. Normally, the standard gas was diluted to a mixing ratio range of 15–20 ppbv (parts per billion by volume). The standard gas flow (about 60 ml min⁻¹) and the zero air flow (about 3260 ml min⁻¹) were regulated using needle valves (stainless steel, Swagelok Co., part number SS-SS2) and the flows were measured during each calibration using a primary

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flow meter (Bios International Corp., DryCal DC-2M). The flow meter was installed in the calibration system only during the flow measurement. PTFE tubing (1.6 mm inner diameter) was used in the calibration lines and the calibration system was connected to the PTR-MS in the same way as the main sampling lines. The calibration system was utilized also in the zero air measurements.

The PTR-MS was calibrated four times during the measurement period: on 27 March, 3 April, 13 April, and 18 April. The calibration procedure contained three stages. First, zero air was measured for about 30 min (67 cycles), then the standard gas bottle was opened and a mixture of zero air and standard gas was fed into the PTR-MS for about 90 min (200 cycles), and finally, the standard gas bottle was closed and zero air was measured again for at least 30 min. The standard gas flow and the zero air flow were measured right before the gas bottle was closed. The flows were not changed during the calibration, so each of the four calibrations was performed at a single VOC mixing ratio.

In addition to the protonated masses of the VOCs in the calibration gas standard (Table 2), masses of some fragmentation products were measured in the calibrations. Fragments of isoprene were detected at 41 amu (M41), fragments of acetone at M43, fragments of α -pinene at M81, M82, and M95, and fragments of *cis*-3-hexenol and hexanal at M83 (de Gouw et al., 2003b; Tani et al., 2003; Warneke et al., 2003; Ammann et al., 2004; de Gouw and Warneke, 2007). The length of the PTR-MS measurement cycle was 27 s and the integration time was 1 s for each VOC-related mass.

The SEM of the PTR-MS was checked before every calibration. In these tests, zero air was fed into the PTR-MS and the operating voltage of the SEM was increased by 50 V steps. The signals of the primary ion isotopes (M21) and isoprene (M69) were recorded and the optimal SEM voltage was chosen so that the signals did not increase more than 20% when the voltage was increased by 100 V. Each calibration was considered to be valid until the next SEM test.

The instrumental noises for the compounds in the calibration gas standard were estimated by calculating the standard deviations of the normalized count rates (see

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Eq. 6) observed when a mixture of zero air and standard gas was fed into the PTR-MS. The instrumental noise for formaldehyde was estimated by calculating the standard deviation of the normalized count rate observed in a measurement where the sample air was taken from a plastic bag containing ambient air and a small piece of tissue dipped in a solution of formaldehyde (36.5%), methanol (10%), and water (Riedel-de Haën GmbH). This measurement was performed at a mixing ratio of about 30 ppbv. The standard deviations were used to determine the uncertainties of the measured ambient mixing ratios.

2.4 Volume mixing ratio measurements by PTR-MS

The development and technical properties of the commercially available proton transfer reaction mass spectrometer (PTR-MS, Ionicon Analytik GmbH) have been discussed in detail by [Hansel et al. \(1995\)](#), [Lindinger et al. \(1998a,b\)](#), and [de Gouw and Warneke \(2007\)](#). Briefly, the instrument consists of four main components: an ion source, a drift tube, a mass spectrometer, and an ion detector. Primary ions (H_3O^+) are produced from pure water vapour within the hollow cathode discharge ion source. The proton transfer reactions between the primary ions and VOCs take place in the drift tube, which is maintained at a pressure of approximately 2 hPa. An electric field is applied in the axial direction of the drift tube and ambient air is continuously pumped through the tube at a flow rate of about 10 ml min^{-1} . The primary and product ions are selected according to their molecular masses (to be exact, according to their mass to charge ratios) using a quadrupole mass spectrometer and detected as count rates by a secondary electron multiplier (SEM). As only a single (integer) mass can be selected at a time, different masses must be measured successively. An integration, or dwell, time can be predetermined for each mass, which enables longer integration times to be applied when expected volume mixing ratios are low and vice versa. This increases experimental precision for VOCs at low mixing ratios.

Due to their low proton affinities, the major components of air do not react with the primary ions in the drift tube. However, VOCs possessing a proton affinity higher than

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that of water (691 kJ mol^{-1}) are ionized in proton transfer reactions:



The number concentration of RH^+ ions produced in Reaction (R1) is given by

$$[\text{RH}^+] = [\text{H}_3\text{O}^+]_0 (1 - e^{-k[\text{R}]\Delta t}) \approx [\text{H}_3\text{O}^+]k[\text{R}]\Delta t \quad (1)$$

5 (e.g., [Lindinger et al., 1998a](#); [de Gouw et al., 2003a](#); [de Gouw and Warneke, 2007](#)). In this equation, $[\text{H}_3\text{O}^+]_0$ is the number concentration of the primary ions injected from the ion source, k is the proton transfer reaction rate coefficient, and $[\text{R}]$ is the number concentration of the compound R in the drift tube. The reaction time, Δt , is determined by the length of the drift tube, L , and the average drift velocity, v_{drift} :

$$10 \quad \Delta t = \frac{L}{v_{\text{drift}}} = L \left(\mu_0 N_0 \frac{E}{N} \right)^{-1} \quad (2)$$

([de Gouw et al., 2003a](#); [de Gouw and Warneke, 2007](#)), where μ_0 is the reduced, or normalized, ion mobility of the primary ions and N_0 is the number density of air at the standard pressure (1013.25 hPa) and temperature (273.15 K). The electric field over the length of the drift tube, $E = U_{\text{drift}}/L$, is determined by the drift tube voltage, U_{drift} .
15 The drift tube pressure, p_{drift} , and temperature, T_{drift} , determine the number density of the gas in the drift tube, $N = N_A p_{\text{drift}} / (RT_{\text{drift}})$, where N_A is Avogadro's constant and R is the molar gas constant.

The approximation in Eq. (1) is justified if the term $k[\text{R}]\Delta t$ is small, i.e., if only a small fraction of the primary ions reacts in the drift tube. Equation (1) shows that under these
20 conditions $[\text{RH}^+]$ is linearly proportional to $[\text{R}]$ and $[\text{H}_3\text{O}^+]$, the number concentration of the primary ions at the end of the drift tube. If $[\text{R}]$ is too high, the approximation is no longer valid and the production of RH^+ ions is non-linear in $[\text{R}]$, which should be avoided.

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2.4.1 Calculation of volume mixing ratios

There are some important issues that have to be considered before Eq. (1) is used to calculate the volume mixing ratio of the compound R. Since the observed ion count rates, $I(\text{RH}^+)$ for RH^+ ions and $I(\text{H}_3\text{O}^+)$ for H_3O^+ ions, are linearly proportional to the respective number concentrations in the drift tube (de Gouw et al., 2003a), Eq. (1) can be written

$$[\text{R}] = \frac{1}{k\Delta t} \frac{I(\text{RH}^+)}{T(\text{RH}^+)} \left(\frac{I(\text{H}_3\text{O}^+)}{T(\text{H}_3\text{O}^+)} \right)^{-1} \quad (3)$$

The coefficients $T(\text{RH}^+)$ and $T(\text{H}_3\text{O}^+)$ are the transmission efficiencies for RH^+ and H_3O^+ ions, respectively, and their values range between one and zero. They are determined by the extraction efficiency of ions from the drift tube into the quadrupole mass spectrometer, the transmission efficiency of the mass spectrometer, and the detection efficiency of the SEM. The transmission coefficients are mainly mass dependent but they vary also over time (de Gouw et al., 2003a; Ammann et al., 2004; Steinbacher et al., 2004).

Usually, the signal of the primary ion isotopes, $\text{H}_3^{18}\text{O}^+$, detected at 21 amu (M21) is measured instead of the primary ion signal detected at 19 amu (e.g., Ammann et al., 2004). In this case, the primary ion count rate is calculated using the relation $I(\text{H}_3\text{O}^+) = I(\text{M19}) = 500 \times I(\text{M21})$, where the factor 500 is determined by the isotope ratio $^{16}\text{O}:^{18}\text{O}$. The direct measurement of the primary ion signal would significantly shorten the lifetime of the SEM since the values of $I(\text{M19})$ are typically higher than 5×10^6 counts s^{-1} (cps).

Although PTR-MS uses a soft chemical ionization method, which leads to lower fragmentation than many methods used in gas chromatographic techniques, it has been observed that several VOCs fragment in the drift tube of the PTR-MS (e.g., Tani et al., 2003; Warneke et al., 2003; de Gouw and Warneke, 2007). In addition, the primary ions can cluster with water molecules in the sampled air and the formed water cluster

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ions ($\text{H}_3\text{O}^+\text{H}_2\text{O}$, $\text{H}_3\text{O}^+(\text{H}_2\text{O})_2$, etc.) can ionize VOCs via proton transfer and ligand switching reactions (e.g., Warneke et al., 2001; Tani et al., 2004). Both fragmentation and cluster ion formation depend strongly on the parameter E/N , the ratio of the electric field to the number density of the gas in the drift tube, which is usually expressed in units of Townsend ($1 \text{ Td} = 10^{-17} \text{ V cm}^2$). The degree of fragmentation increases and the degree of cluster ion formation decreases when the parameter E/N is increased. Cluster ion formation depends also on the humidity of the sampled air (Warneke et al., 2001; Ammann et al., 2006).

To take the effects of fragmentation and water cluster ion formation into account, we added a fragmentation coefficient for RH^+ ions, $F(\text{RH}^+)$, and the count rate of $\text{H}_3\text{O}^+\text{H}_2\text{O}$ ions, $I(\text{H}_3\text{O}^+\text{H}_2\text{O})$, to Eq. (3), which then changes to the form

$$\begin{aligned}
 [\text{R}] &= \frac{1}{k\Delta t} \frac{I(\text{RH}^+)}{F(\text{RH}^+)T(\text{RH}^+)} \left(\frac{I(\text{H}_3\text{O}^+)}{T(\text{H}_3\text{O}^+)} + \frac{I(\text{H}_3\text{O}^+\text{H}_2\text{O})}{T(\text{H}_3\text{O}^+\text{H}_2\text{O})} \right)^{-1} \\
 &= \frac{1}{k\Delta t} \frac{I(\text{RH}^+)}{F(\text{RH}^+)T(\text{RH}^+)} \left(\frac{I(\text{H}_3\text{O}^+) + I(\text{H}_3\text{O}^+\text{H}_2\text{O})}{T(\text{H}_3\text{O}^+, \text{H}_3\text{O}^+\text{H}_2\text{O})} \right)^{-1} \\
 &= \frac{1}{k\Delta t} \frac{T(\text{H}_3\text{O}^+, \text{H}_3\text{O}^+\text{H}_2\text{O})}{F(\text{RH}^+)T(\text{RH}^+)} \frac{I(\text{RH}^+)}{I(\text{H}_3\text{O}^+) + I(\text{H}_3\text{O}^+\text{H}_2\text{O})}. \quad (4)
 \end{aligned}$$

In this equation, $F(\text{RH}^+)$ gives the proportion of RH^+ ions to all product ions (i.e., RH^+ and fragment ions) formed in the proton transfer reactions between the primary and water cluster ions and the compound R. For non-fragmenting compounds $F(\text{RH}^+) = 1$. $T(\text{H}_3\text{O}^+\text{H}_2\text{O})$ is the transmission coefficient for the water cluster ions, and $T(\text{H}_3\text{O}^+, \text{H}_3\text{O}^+\text{H}_2\text{O})$ is a combined transmission coefficient for the primary and water cluster ions. This combined coefficient is a new variable, which ensures that the two terms in parentheses in Eq. (4) are equal. We introduced it since the values of $T(\text{H}_3\text{O}^+)$ and $T(\text{H}_3\text{O}^+\text{H}_2\text{O})$ cannot be determined directly. It is not necessary to determine the value of the combined transmission coefficient to be able to calculate VOC mixing ratios (see Sects. 2.4.2 and 2.4.3).

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To extend the lifetime of the SEM, we measured the signal of the water cluster ion isotopes detected at M39 instead of the water cluster ion signal detected at M37. We calculated the water cluster ion count rate using the relation $I(\text{H}_3\text{O}^+\text{H}_2\text{O}) = I(\text{M37}) = 250 \times I(\text{M39})$, where the factor 250 is determined by the isotope ratio $^{16}\text{O}^{16}\text{O}:^{18}\text{O}^{16}\text{O}$. To decrease the instrumental noise in the primary and water cluster ion count rates, we smoothed the observed count rates by using a five-minute running average. Because benzene (M79) and toluene (M93) react only slowly with the water cluster ions (Warneke et al., 2001; de Gouw et al., 2003b), we omitted the term $I(\text{H}_3\text{O}^+\text{H}_2\text{O})$ from Eq. (4) when calculating mixing ratios from the signals detected at M79 and M93.

In PTR-MS measurements, significant offset count rates are normally observed for many VOC-related masses. They are most likely caused by desorption of impurities inside the instrument and the sampling system (Steinbacher et al., 2004). To take account of these VOC background signals, we subtracted the average of the ion count rates observed during the zero air measurements from the count rates observed during the actual measurements:

$$[\text{R}] = \frac{1}{k\Delta t} \frac{T(\text{H}_3\text{O}^+, \text{H}_3\text{O}^+\text{H}_2\text{O})}{F(\text{RH}^+)T(\text{RH}^+)} \left[\frac{I(\text{RH}^+)}{I(\text{H}_3\text{O}^+) + I(\text{H}_3\text{O}^+\text{H}_2\text{O})} - \frac{1}{n} \sum_{i=1}^n \frac{I(\text{RH}^+)_{\text{zero},i}}{I(\text{H}_3\text{O}^+)_{\text{zero},i} + I(\text{H}_3\text{O}^+\text{H}_2\text{O})_{\text{zero},i}} \left(\frac{p_{\text{drift, zero},i}}{p_{\text{drift}}} \right)^{-1} \right], \quad (5)$$

where the subscript zero refers to the zero air measurements, n is the number of zero air measurement cycles, and p_{drift} is the drift tube pressure during the actual measurements. In Eq. (5), we took into account that the primary and water cluster ion count rates as well as the drift tube pressure can vary slightly between the actual and zero air measurements.

The instruments commonly used to generate VOC-free air, such as catalytic converters and charcoal cartridges, do not necessarily remove all VOCs from the air. Further, it is possible that a compound, which is not expected to be removed by the zero air

generator, contributes to the signal of a VOC-related mass. For example, the oxygen isotope, $^{16}\text{O}^{17}\text{O}$, is detected at the same mass as methanol (M33). Such overlap problems are probably less significant than the problem due to the inefficiency of the zero air generator, which is difficult to quantify if there are no zero air references available.

5 When calculating mixing ratios from the signal detected at M33, we subtracted 0.08% (the isotope ratio) of the oxygen count rate (M32) observed during the actual and zero air measurements from the respective M33 count rates.

The normalized count rate of RH^+ ions, expressed in units of normalized counts s^{-1} (ncps), is frequently used in PTR-MS studies to enable comparison of signals observed in different measurements. Our definition of the normalized RH^+ ion count rate is

$$\begin{aligned}
 I(\text{RH}^+)_{\text{norm}} = & I(\text{RH}^+) \left(\frac{I(\text{H}_3\text{O}^+) + I(\text{H}_3\text{O}^+\text{H}_2\text{O})}{I_{\text{norm}}} \right)^{-1} \left(\frac{\rho_{\text{drift}}}{\rho_{\text{norm}}} \right)^{-1} \\
 & - \frac{1}{n} \sum_{i=1}^n I(\text{RH}^+)_{\text{zero},i} \left(\frac{I(\text{H}_3\text{O}^+)_{\text{zero},i} + I(\text{H}_3\text{O}^+\text{H}_2\text{O})_{\text{zero},i}}{I_{\text{norm}}} \right)^{-1} \\
 & \left(\frac{\rho_{\text{drift, zero},i}}{\rho_{\text{norm}}} \right)^{-1}. \tag{6}
 \end{aligned}$$

In this equation, the sum of the primary and water cluster ion count rates is normalized to a count rate of $I_{\text{norm}}=10^6$ cps and the drift tube pressure is normalized to a pressure of $\rho_{\text{norm}}=2$ hPa. Our definition of the normalized count rate resembles the one proposed by Tani et al. (2004). In addition to H_3O^+ and $\text{H}_3\text{O}^+\text{H}_2\text{O}$ ions, the equation presented by Tani et al. (2004) takes into account $\text{H}_3\text{O}^+(\text{H}_2\text{O})_2$ ions, but it does not include the subtraction of the VOC background signals.

According to Eqs. (5) and (6), the number concentration of the compound R is

$$[\text{R}] = \frac{1}{k\Delta t} \frac{T(\text{H}_3\text{O}^+, \text{H}_3\text{O}^+\text{H}_2\text{O})}{F(\text{RH}^+)T(\text{RH}^+)} \frac{\rho_{\text{drift}}}{I_{\text{norm}}\rho_{\text{norm}}} I(\text{RH}^+)_{\text{norm}}. \tag{7}$$

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Finally, we converted the number concentration of the compound R into a volume mixing ratio, VMR, given in units of parts per billion by volume (ppbv, 10^{-9}):

$$\begin{aligned} \text{VMR} &= 10^9 \frac{[\text{R}]}{N} \\ &= 10^9 \frac{\rho_{\text{drift}}}{I_{\text{norm}} \rho_{\text{norm}}} \frac{\mu_0 N_0}{kL} \frac{E}{N^2} \frac{T(\text{H}_3\text{O}^+, \text{H}_3\text{O}^+\text{H}_2\text{O})}{F(\text{RH}^+)T(\text{RH}^+) / (\text{RH}^+)_{\text{norm}}}. \end{aligned} \quad (8)$$

To get this equation, we calculated the reaction time in Eq. (7) according to Eq. (2).

2.4.2 Determination of sensitivities

To be able to calculate volume mixing ratios for the VOCs present in our calibration gas standard, we determined the sensitivity of the PTR-MS for these compounds by a direct calibration (Sect. 2.3). Our definition of the sensitivity is based on Eq. (8). The sensitivity is

$$S = \frac{I(\text{RH}^+)_{\text{norm}}}{\text{VMR}} = 10^{-9} \frac{I_{\text{norm}} \rho_{\text{norm}}}{\rho_{\text{drift}}} \frac{kL}{\mu_0 N_0} \frac{N^2}{E} \frac{F(\text{RH}^+)T(\text{RH}^+)}{T(\text{H}_3\text{O}^+, \text{H}_3\text{O}^+\text{H}_2\text{O})} \quad (9)$$

and its unit is ncps ppbv⁻¹. We calculated the sensitivities from this equation using the known calibration mixing ratios and the corresponding normalized count rates. Once we had determined the sensitivities, we calculated the mixing ratios for the respective compounds according to Eq. (8) using the normalized count rates observed in the actual measurements.

Our definition of the sensitivity resembles the one given by de Gouw et al. (2003a). The differences are due to our definition of the normalized count rate, the fragmentation coefficient, and the combined transmission coefficient. Because we take the drift tube pressure into account in the normalized count rate, there is an additional term, $\rho_{\text{norm}}/\rho_{\text{drift}}$, in Eq. (9), which is not included in the sensitivity defined by de Gouw et al. (2003a). We have also added the fragmentation coefficient and replaced the transmission coefficient of the primary ions with the combined transmission coefficient. The

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term $10^{-9} \times I_{\text{norm}} = 10^{-3}$ cps in our equation agrees with the factor 10^{-3} in the equation of de Gouw et al. (2003a).

2.4.3 Determination of a relative transmission curve

To be able to calculate volume mixing ratios for VOCs not present in our calibration gas standard, we have developed a method for determining a relative transmission curve for the mass range M20–M170. This method is based on the measured sensitivities, and a new transmission curve is determined after every calibration. In this method, we consider only those VOCs in our calibration gas standard that do not fragment significantly (Table 2). First, we calculate relative transmission coefficients for the masses related to the non-fragmenting VOCs. According to Eq. (9), the relative transmission coefficient is

$$T(\text{RH}^+)_{\text{rel}} = \frac{T(\text{RH}^+)}{T(\text{H}_3\text{O}^+, \text{H}_3\text{O}^+\text{H}_2\text{O})} = 10^9 \frac{\rho_{\text{drift}}}{I_{\text{norm}} \rho_{\text{norm}}} \frac{\mu_0 N_0}{kL} \frac{E}{N^2} S. \quad (10)$$

For the reduced ion mobility, we use a value of $\mu_0 = 2.8 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$, and for the proton transfer reaction rate coefficient the values reported by Zhao and Zhang (2004) (Table 2). If there is no data available for a certain VOC, we use a generic value of $k = 2 \times 10^{-9} \text{ cm}^3 \text{ s}^{-1}$. To calculate the electric field and the number density, we use the drift tube voltage, pressure, and temperature measured during the calibration. The length of the drift tube is 9.5 cm in our instrument.

Depending on the calibration gas standard used in the calibration, we calculate the relative transmission coefficient for eight or ten VOC-related masses (Table 2). The corresponding mass ranges are M33–M107 and M33–M129. To be able to obtain the relative transmission curve for the mass range M20–M170, we determine six empirical parameters from the relative transmission coefficient data. The criteria for these parameters are: (1) The maximum of the relative transmission curve is the average of the two highest relative transmission coefficients, (2) the second parameter is the median of the relative transmission coefficients related to the masses that are smaller

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than the mass of the maximum point, (3) the third parameter is the median of the relative transmission coefficients related to the masses that are higher than the mass of the maximum point, (4) the relative transmission coefficient for M20 is 80% of the value calculated for M33 (methanol), (5) the relative transmission coefficient for M129 is 70% of the value calculated for M107 (m- and o-xylene), and (6) the relative transmission coefficient for M170 is 40% of the value calculated for M107. When the relative transmission coefficient for M129 is calculated directly, the fifth criterion is: The relative transmission coefficient for M151 is 70% of the value calculated for M129 (naphthalene). Finally, the relative transmission curve is determined by fitting a piecewise cubic Hermite interpolation function (e.g., [Fritsch and Carlson, 1980](#)) to the parameters.

Since there is no theoretical basis for the shape of the relative transmission curve ([Ammann et al., 2004](#); [Steinbacher et al., 2004](#)), we have decided to use this practical method instead of a more mathematical one. However, the criteria for the parameters 1–3 are based on the calculated relative transmission coefficients. The percentage values for the parameters 4–6 have been estimated using averages and subjective interpretation of a data set containing information from several calibrations. In addition, the automatic implementation of our method is straightforward, which is an important advantage when the PTR-MS is used for continuous long-term measurements.

Once we had determined the relative transmission curve, we used the following equation to calculate mixing ratios for the VOCs not present in our calibration gas standard:

$$\text{VMR} = 10^9 \frac{\rho_{\text{drift}}}{I_{\text{norm}} \rho_{\text{norm}}} \frac{\mu_0 N_0}{kL} \frac{E}{N^2} \sum_{i=1}^m \frac{I(M_i)_{\text{norm}}}{T(M_i)_{\text{rel}}}, \quad (11)$$

where m is the number of different product ions, M_i (i.e., RH^+ ions and possible fragment ions). This equation is derived from Eq. (8) by using the definition of the relative transmission coefficient (Eq. (10)) and the fact that $\sum_{i=1}^m F(M_i) = 1$. The summation is unnecessary for non-fragmenting compounds since for them $m=1$. The advantage of this equation is that it is not necessary to determine the values of the fragmentation

coefficients. It is sufficient to determine the relative transmission curve and to measure the signal of RH^+ ions and the signals of all the major fragmentation products. However, due to the uncertainties of the reported proton transfer reaction rate coefficients and the relative transmission curve, the accuracy of the data calculated using Eq. (11) is significantly lower than the accuracy of the data based on the measured sensitivities.

3 Results and discussion

To achieve and maintain the accuracy needed in atmospheric VOC measurements, we calibrated the PTR-MS regularly with a gas standard. We calculated the mixing ratios for the compounds in our gas standard using the measured sensitivities (Eqs. 8 and 9). To calculate the mixing ratios for the compounds not present in the gas standard, we determined the relative transmission curve using the information obtained from the calibrations (Eqs. 10 and 11). We also took the following details into account when calculating the mixing ratios: (1) subtraction of the VOC background signals determined frequently with a reliable zero air generator, (2) normalization of the product ion count rates using the measured primary and water cluster ion count rates and the drift tube pressure, which reduces the effect of ambient humidity on the sensitivity, (3) for the compounds reacting slowly with the water cluster ions, only the primary ion count rate and the drift tube pressure were used in the normalization, (4) to reduce the instrumental noise, the primary and water cluster ion count rates were smoothed using a 5-min running average, (5) the effect of fragmentation was included in the measured sensitivities, and (6) for the compounds not present in the calibration gas standard, fragmentation was taken into account by summing the mixing ratios of all product ions (i.e., RH^+ ions and major fragment ions).

Figure 2 illustrates the effect of the subtraction of the VOC background signals. It shows the hourly averages of the normalized count rates of formaldehyde, methanol, benzene, and monoterpenes (the highest values not visible) observed in the ambient

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3.1 Calibrations

We calibrated the PTR-MS four times during the measurement period 27 March–26 April 2007. To illustrate the stability of calibration over a longer time scale, we present results also from four calibrations that we conducted in July and August 2007. The calibration setup and procedure were similar in all calibrations, except for the calibration gas standard (Table 2).

The sensitivities shown in Fig. 3 were calculated according to Eq. (9) in all calibrations. The highest values, 26–38 ncps ppbv⁻¹, were observed for acetonitrile (M42), acetaldehyde (M45), acetone (M59), methacrolein and methyl vinyl ketone (M71), and methyl ethyl ketone (M73). The sensitivities for methanol (M33), isoprene (M69), and benzene (M79) were 16–22 ncps ppbv⁻¹. There was a decreasing trend between toluene (M93), m- and o-xylene (M107), 1,2,4-trimethylbenzene (M121), and naphthalene (M129). The sensitivity for α -pinene (M137) was 6–8 ncps ppbv⁻¹ and the sensitivity for its major fragmentation product (M81) was 8–11 ncps ppbv⁻¹. For *cis*-3-hexenol and hexanal (M101) the sensitivity was low, 3–6 ncps ppbv⁻¹, but for their fragments (M83) it was 25–27 ncps ppbv⁻¹ (Fig. 3a). This indicates that these compounds fragment strongly in the drift tube since the difference between the transmission coefficients

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for the respective masses cannot alone explain such a big difference in the sensitivity. The sensitivities for the fragments of isoprene (M41), acetone (M43), and α -pinene (M82 and M95) were lower than 5 ncps ppbv⁻¹ (Fig. 3a). These fragments seem to be minor fragmentation products in our PTR-MS under the operating conditions used in the measurements. Since the sensitivity for 1,2,4-trichlorobenzene (M182) was practically zero (Fig. 3b), it is probable that this compound did not come out of the standard gas bottle properly.

In general, the sensitivity of our instrument was lower in July and August than in March and April. There is also variation within the data sets in Fig. 3. These facts prove that regular calibrations are needed to maintain the accuracy of PTR-MS measurements. The changes in the sensitivity can be attributed to changes in the transmission and the humidity of the sampled air. The main reason for the changes in the transmission was probably the detection efficiency of the SEM. Although we took the water cluster ions into account when calculating the sensitivities (see Eqs. 6 and 9), this hardly completely removed the effect of humidity.

The sensitivities measured in this work are generally somewhat lower than the values measured by de Gouw et al. (2003b) and Warneke et al. (2003). The most remarkable difference is related to α -pinene (7 vs. 29 and 36 ncps ppbv⁻¹). However, our definition of the normalized count rate differs slightly from the one used by de Gouw et al. (2003b) and Warneke et al. (2003), so the sensitivities are not totally comparable.

3.2 Relative transmission curves

The principle of our method for determining a relative transmission curve becomes clear from Fig. 4a. The relative transmission coefficients (solid circles) were calculated from Eq. (10) using the sensitivities measured for the VOCs marked with a circle in Table 2 (except for 1,2,4-trichlorobenzene). These compounds do not fragment significantly and their detection is not remarkably interfered by other compounds or fragments (de Gouw et al., 2003a,b; Warneke et al., 2003; de Gouw and Warneke, 2007). The parameters used for fitting the relative transmission curve (open circles) were determined

according to the criteria explained in Sect. 2.4.3.

The compatibility of the relative transmission curves with the relative transmission coefficients in Fig. 4a is reasonable. The extrapolation for the masses below M33 and above M107 or M129 was based on the parameters that were determined using the relative transmission coefficients for M33, M107, and M129 together with the empirical percentage values. For example, if we had extrapolated according to straight lines fitted to the relative transmission coefficients before and after the maximum point of the curve, the results for the light masses would have been practically similar whereas the results for the heavy masses would have been significantly lower. However, according to the data collected from several calibrations during the summer 2007 (not presented in this paper), the decreasing trend between the relative transmission coefficients for M93, M107, M121, and M129 was not linear. The transmission decreased slower than in the linear case. We could also have used a non-linear extrapolation method, but its application would have been limited to the calibrations made with the gas standard, which contained 1,2,4-trimethylbenzene (M121) and naphthalene (M129). Therefore, we decided to use the more practical approach described in Sect. 2.4.3.

Our method proved to be sensitive enough to capture the changes in the transmission over time (Fig. 4b). Although the general level of the relative transmission curve varied, the shape of the curve remained rather constant. Since in all cases the two highest relative transmission coefficients were those of M79 (benzene) and M93 (toluene), the maximum of the curve was always at M86. Within the mass ranges M20–M70 and M100–M170, the relative transmission derived from the calibrations in March and April was higher than in the case of the calibrations in July and August. This is due to the differences in the sensitivities for the light compounds (methanol, acetonitrile, acetaldehyde, methacrolein, methyl vinyl ketone, and methyl ethyl ketone) and for m- and o-xylene.

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3.3 Ambient volume mixing ratio measurements

Figure 5 shows the mixing ratios of formaldehyde, methanol, benzene, and monoterpenes measured in the crown space of the Scots pine canopy (at 14 m above the ground) in 27 March–26 April 2007. Air temperature and photosynthetically active radiation were measured above the top of the canopy, at 16.8 and 18.0 m, respectively.

The hourly averages of the mixing ratios were 0.1–0.5 ppbv for formaldehyde, 0.2–3.0 ppbv for methanol, 0.04–0.39 ppbv for benzene, and 0.03–1.25 ppbv for monoterpenes (the highest mixing ratios not visible in Fig. 5). The uncertainties of the hourly averages, σ_{avg} , were 0.2, 0.5, 0.07, and 0.10 ppbv, respectively. They were calculated from the equation $\sigma_{\text{avg}} = \sigma / \sqrt{n}$, where σ represents the uncertainty of an individual measurement due to the instrumental noise and n is the number of individual measurements contributing to the average. The instrumental noise was estimated by calculating the standard deviation of the normalized count rate observed when a constant VOC mixing ratio was fed into the PTR-MS (Sect. 2.3).

The mixing ratios did not have clear diurnal cycles, but in general the maximum values were observed at night. During the warm period on 15 and 16 April, the mixing ratios of formaldehyde, methanol, and monoterpenes were above the average level of the whole month while the mixing ratio of benzene remained at the average level. On the other hand, the mixing ratios of formaldehyde, methanol, and benzene were high at the beginning of the measurement period (27–30 March) while the rise in the monoterpene mixing ratio was not remarkable. These facts may indicate that monoterpenes had a strong local source, benzene had remote anthropogenic sources, and formaldehyde and methanol had both local and remote sources.

Formaldehyde was not present in our calibration gas standard, and we had to determine its relative transmission coefficient (Sect. 2.4.3) to calculate the mixing ratios. Our PTR-MS measurements gave slightly lower results than the measurements with a chemical derivatization method at the same site in March–April 2003 (Hellén et al., 2004). Ambient humidity affects the detection of formaldehyde by PTR-MS significantly

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(Hansel et al., 1997; Inomata et al., 2008). However, the correlation coefficient between the hourly averages of the formaldehyde mixing ratio and the 30-min averages of the ambient water vapour mixing ratio was only -0.13 . On the other hand, the correlation coefficient between the ambient water vapour mixing ratio and the normalized water cluster ion count rate, calculated according to Eq. (6), was 0.98. We suppose that we could reduce the effect of ambient humidity on the detection of formaldehyde since we took the abundance of the water cluster ions into account when determining the relative transmission coefficient and calculating the mixing ratios.

The mixing ratios of methanol, benzene, and monoterpenes were calculated using the measured sensitivities and therefore the accuracy was better for these compounds than for formaldehyde. The methanol mixing ratios were somewhat lower than those measured with PTR-MS at the same site in July 2004 (Rinne et al., 2005). This can be partly due to the seasonal variation in the tropospheric chemistry and emissions of methanol, but also the fact that the PTR-MS was not calibrated with a gas standard in 2004 can explain the difference. Methanol has not been measured with alternative methods at the SMEAR II station, but the results of the present PTR-MS measurements agree well with the lower limit of the representative mixing ratio range for coniferous and deciduous forests suggested by Heikes et al. (2002). The mixing ratios of benzene and monoterpenes presented in this work are in the same range with the results of gas chromatographic measurements at the same site during the same season (Hakola et al., 2003). Similar monoterpene mixing ratios have been observed also at another boreal forest site in Finland in May (Hakola et al., 2000).

Figure 6 illustrates the relation between the monoterpene mixing ratios derived from the M81 and M137 signals. It shows all individual measurements conducted at the three sampling heights and the corresponding hourly averages. The correlation is stronger for the hourly averages than for the individual measurements. Since the M81 and M137 signals are not measured simultaneously, the differences in the individual measurements are partly due to short-term variations in mixing ratios caused by turbulent eddies. However, the correlation is strong in both data sets, and the slopes and

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the offsets of the straight lines fitted to the data in a least squares sense are close to one and zero, respectively. This indicates that the fragmentation patterns of the major monoterpenes in ambient air were similar to that of α -pinene, which was the only monoterpene used in the calibrations, and that there were no major interfering compounds or fragments detected at M81 and M137. It has been observed that α -pinene contributes most to the total monoterpene mixing ratio at the SMEAR II station, but in spring the contributions of β -pinene and 3-carene are also significant (Hakola et al., 2003). Tani et al. (2003) noticed that the fragmentation patterns of these monoterpenes were quite similar in their PTR-MS and according to Fig. 6 that seems to apply to our instrument too. We suppose that the differences between the monoterpene mixing ratios derived from the M81 and M137 signals are due to turbulent eddies, instrumental noise, and minor interfering compounds. However, de Gouw et al. (2003b) and Warneke et al. (2003) found that the sensitivity of their instrument for α -pinene was lower than for β -pinene and 3-carene. Therefore, it is possible that there was a positive bias in our monoterpene measurements if there were periods when the contributions of β -pinene and 3-carene to the total monoterpene mixing ratio were enhanced.

4 Conclusions

In this paper, we presented our measurement, calibration, and volume mixing ratio calculation methods in detail. These methods have been designed for quantitative long-term stand-alone field measurements by PTR-MS and are therefore systematic, practical, and as automatic as reasonable. They have proven to be functional and effective in our long-term measurements at the SMEAR II station.

We showed that the PTR-MS has to be calibrated regularly with a gas standard to achieve and maintain the accuracy needed in atmospheric VOC measurements. We also showed how the information obtained from a calibration can be used to determine the instrument specific relative transmission curve, which enables quantitative mixing ratio calculation for VOCs not present in a calibration gas standard. The automatic

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implementation of our method for determining this curve is straightforward, which is an important advantage when the PTR-MS is used for continuous long-term measurements. We illustrated that the relative transmission curves determined with our method were compatible with the relative transmission coefficients derived from the sensitivities measured for the non-fragmenting VOCs in our calibration gas standards. The general level of the relative transmission curve varied according to the changes in the sensitivity, but the shape of the curve remained rather constant.

We presented a one-month period of ambient mixing ratio data for formaldehyde, methanol, benzene, and monoterpenes to illustrate the functionality of our measurement, calibration, and calculation methods. The formaldehyde, benzene, and monoterpene mixing ratios measured with PTR-MS were of the same order of magnitude as those measured with other techniques at the same site earlier. The monoterpene mixing ratios derived from the M81 signal corresponded to those derived from the M137 signal. This shows that the fragmentation patterns of the major monoterpenes in ambient air were similar to that of α -pinene, the only monoterpene used in the calibrations, and that there were no major interfering compounds detected at M81 and M137. In summary, our mixing ratio calculation method seems to give reasonable results for formaldehyde, which was not present in the calibration gas standards, and naturally also for methanol, benzene, and monoterpenes, which were present in the gas standards.

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Table 1. PTR-MS measurement cycle in the ambient volume mixing ratio measurements, the compounds contributing to the measured masses, and the PTR-MS integration, or dwell, times. The cycle length was 38 s.

Protonated mass [amu] and contributing compound(s)	Formula	Dwell time [s]
21 water isotope	H ₂ ¹⁸ O	0.2
25 (control mass)		0.2
31 formaldehyde	CH ₂ O	2.0
32 oxygen*	O ₂	0.2
33 methanol	CH ₄ O	2.0
39 water cluster isotope	H ₂ OH ₂ ¹⁸ O	0.2
42 acetonitrile	C ₂ H ₃ N	2.0
45 acetaldehyde	C ₂ H ₄ O	2.0
59 acetone	C ₃ H ₆ O	2.0
69 isoprene	C ₅ H ₈	2.0
methylbutenol fragment		
71 methacrolein	C ₄ H ₆ O	2.0
methyl vinyl ketone	C ₄ H ₆ O	
73 methyl ethyl ketone	C ₄ H ₈ O	2.0
79 benzene	C ₆ H ₆	2.0
81 monoterpene fragment		2.0
hexenal fragment		
87 methylbutenol	C ₅ H ₁₀ O	2.0
93 toluene	C ₇ H ₈	2.0
99 hexenal	C ₆ H ₁₀ O	2.0
101 <i>cis</i> -3-hexenol	C ₆ H ₁₂ O	2.0
hexanal	C ₆ H ₁₂ O	
113		2.0
137 monoterpenes	C ₁₀ H ₁₆	2.0
141		2.0
169 monoterpene oxidation products	C ₁₀ H ₁₆ O ₂	2.0

* molecular mass

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Table 2. Compositions of the calibration gas standards. The standard A was used in the calibrations conducted in March and April 2007 and the standard B was used in July and August 2007. The manufacturer (Apel-Riemer Environmental, Inc.) estimated that the uncertainty of volume mixing ratio (VMR) was not more than 6% for *cis*-3-hexenol and methyl vinyl ketone (in A) and not more than 5% for the other compounds. The last column contains the proton transfer reaction rate coefficients (k) reported by Zhao and Zhang (2004).

VOC and its protonated mass [amu]	Formula		VMR in A [ppmv]	VMR in B [ppmv]	k [$10^{-9} \text{ cm}^3 \text{ s}^{-1}$]
33 methanol	CH ₄ O	•	1.03	1.05	2.33
42 acetonitrile	C ₂ H ₃ N	•	1.08	1.01	4.74
45 acetaldehyde	C ₂ H ₄ O	•	1.06	0.99	3.36
47 ethanol	C ₂ H ₆ O		1.06	–	
59 acetone	C ₃ H ₆ O		1.09	1.05	
69 isoprene	C ₅ H ₈		1.09	1.02	
71 methacrolein	C ₄ H ₆ O	•	1.08	–	3.55
71 methyl vinyl ketone	C ₄ H ₆ O	•	0.92	0.92	3.83
73 methyl ethyl ketone	C ₄ H ₈ O	•	1.08	1.06	3.48
79 benzene	C ₆ H ₆	•	1.07	1.03	1.97
93 toluene	C ₇ H ₈	•	1.07	1.04	2.12
101 <i>cis</i> -3-hexenol	C ₆ H ₁₂ O		0.96	–	
101 hexanal	C ₆ H ₁₂ O		0.97	0.90	
107 m-xylene	C ₈ H ₁₀	•	1.07	1.03	2.26
107 o-xylene	C ₈ H ₁₀	•	1.07	1.05	2.32
121 1,2,4-trimethylbenzene	C ₉ H ₁₂	•	–	0.98	2.40
129 naphthalene	C ₁₀ H ₈	•	–	1.00	2.59
137 α -pinene	C ₁₀ H ₁₆		1.05	0.93	
182 1,2,4-trichlorobenzene	C ₆ H ₃ Cl ₃	•	–	1.01	

• These compounds do not fragment significantly in the drift tube of the PTR-MS. They were taken into account in the determination of a relative transmission curve, except for 1,2,4-trichlorobenzene.

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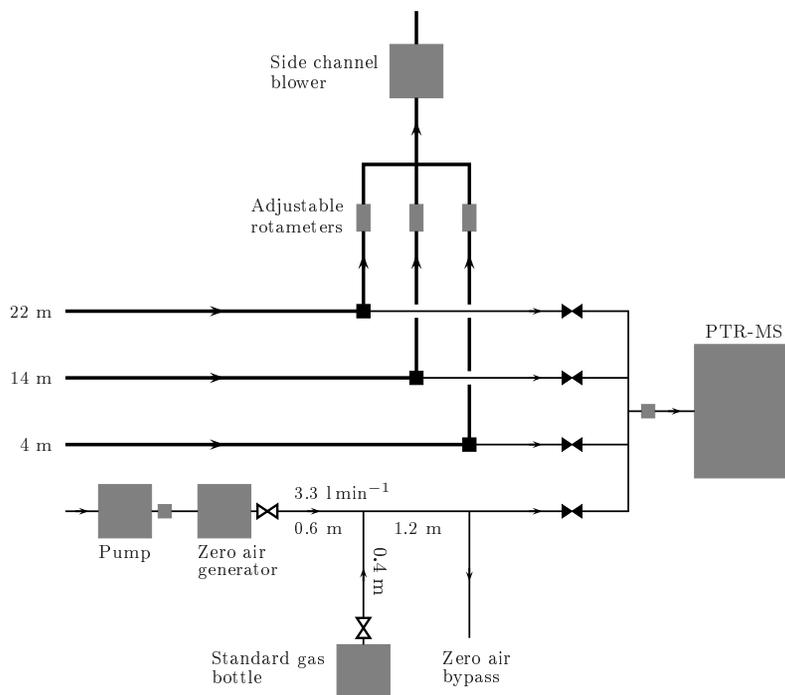
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- T-connector (PTFE) ⚡ Solenoid valve (ETFE) ⚡ Needle valve (stainless steel)
- Filter (PTFE)

- PTFE tubing: flow 17.5 l min^{-1} , inner diameter 8 mm, length 30 m (from the sampling height to the T-connector)
- PTFE tubing: flow 0.1 l min^{-1} , inner diameter 1.6 mm, length 1.3 m (from the T-connector or the zero air bypass to the PTR-MS inlet)

Fig. 1. Measurement and calibration setup used for long-term measurements of VOC mixing ratios by PTR-MS. The sampling heights were 4, 14, and 22 m.

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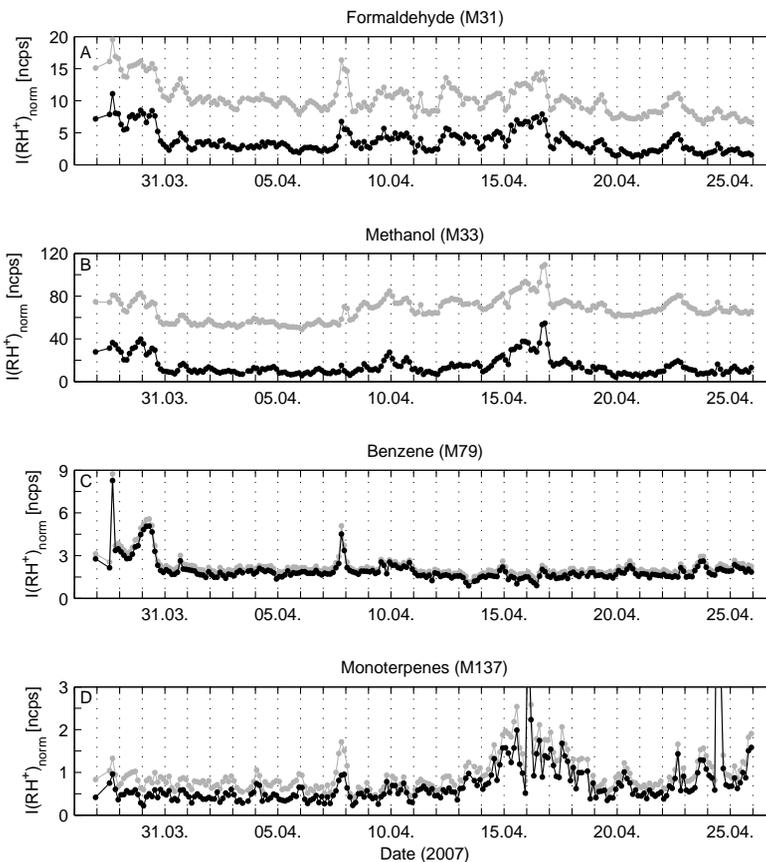


Fig. 2. Hourly averages of the normalized count rates of VOCs during the measurement period 27 March–26 April 2007. The black circles represent the normalized count rates that were calculated according to Eq. (6) and subsequently converted into volume mixing ratios (see Fig. 5). The grey circles show the normalized count rates when the VOC background signals were not subtracted.

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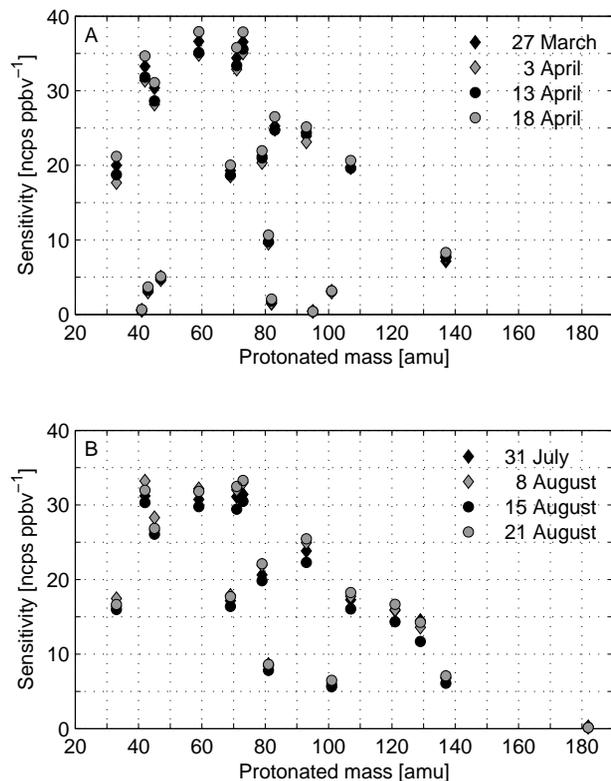


Fig. 3. Measured sensitivities for the VOCs in the calibration gas standards. The calibration setup and procedure were similar in all calibrations, except for the gas standard (Table 2). The calibrations were performed in 2007.

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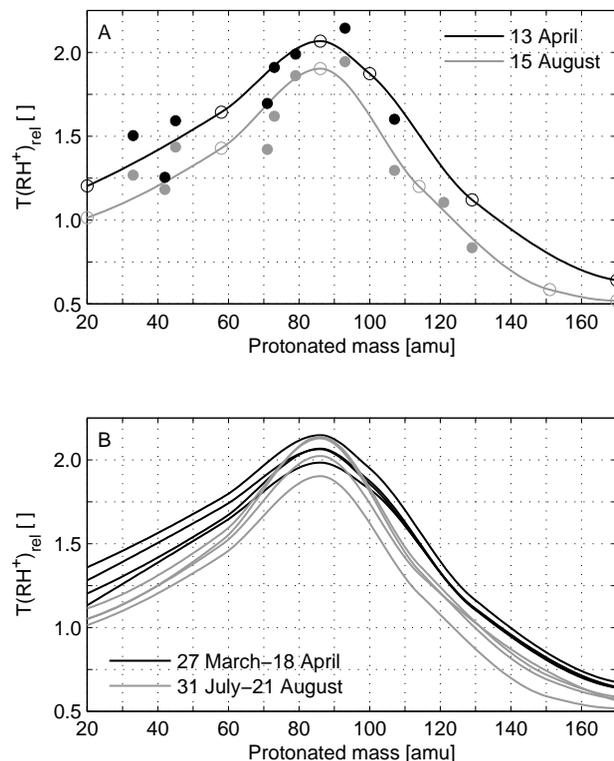


Fig. 4. Principle of the method for determining a relative transmission curve **(A)** and the relative transmission curves **(B)** derived from the calibrations shown in Fig. 3. The relative transmission coefficients (solid circles) were calculated using the measured sensitivities and the parameters used for fitting the curves (open circles) were determined according to the criteria explained in Sect. 2.4.3.

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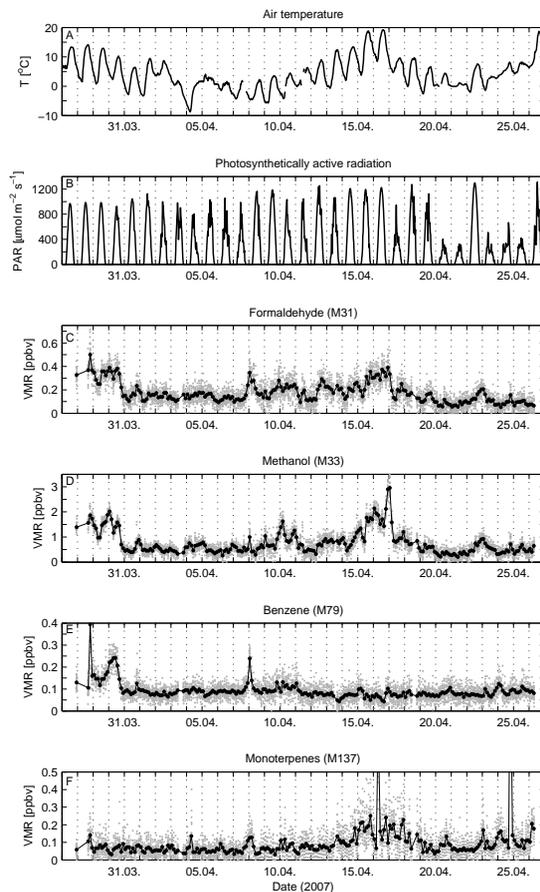


Fig. 5. Air temperature, photosynthetically active radiation, and VOC mixing ratios at the SMEAR II station during the measurement period 27 March–26 April 2007. The grey and black circles represent individual measurements and hourly averages, respectively.

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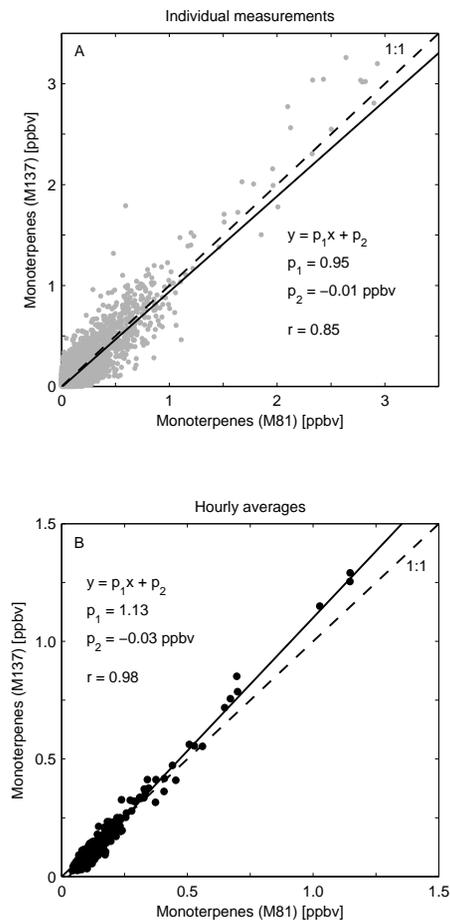


Fig. 6. Relation between the monoterpene mixing ratios derived from the M81 and M137 signals.

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