

Characterization and Locking of Optical Mini-Resonators for Microwave Sources Stabilization

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BIOGRAPHY

Pierre-Henri Merrer received the Master's degree in Photonics and Optical Telecommunications from ENSSAT (Lannion, France), in 2005. He is currently Ph.D. student in LAAS (Laboratory for Analysis and Architecture of Systems), in the research group MOST (microwaves and opto-microwaves for telecommunication systems) and works on microwave-optical systems and high Q optical resonator.

INTRODUCTION

Investigations towards a resonator featuring a high quality factor in a reduced volume are a very important and interesting point in the microwave field. Such resonator could be used for time-frequency applications. In particular, it could be an alternative solution to the ultra-stable BAW oscillator for space applications. Other applications may also concern radars or telemetry with very high sensitivity, and telecommunication applications. The resonators used in these applications are often too big and it is important to reduce their size without loosing the quality factor, especially in embedded systems. Today high spectral purity sources are dielectric resonator oscillators, which includes ceramic and monocristalline resonators (mainly sapphire). The main problem with sapphire resonator is its size and the main problem with ceramic resonator is the $Q \cdot f$ parameter which remains below around 10^{14} (f in Hz). Finally, the technologies for high spectral purity microwave sources are reaching their limits when the goal is to get simultaneously high performance in term of phase noise, small size (integration) and high frequency operation. Therefore, an original idea is to transpose the microwave wavelength in the optics field and to trap the signal in an optical resonator. Contrary to the conventional microwave resonators, the optical-microwave resonator features an equivalent Q at microwave frequencies which increases as the microwave frequency increase. The first microwave source using an optical frequency reference

has been proposed in 1994 [1]. This source was based on an optical delay line which features a typical equivalent microwave quality factor in the range of $Q \sim 10^6$ at 10 GHz [2]. It is today a well known technique, already commercialized. The main problem with these optical-electronic oscillators (OEO) is their size and their sensitivity to temperature changes. A recently proposed alternative approach [3] replaces the optical delay line by an optical mini-resonator, which allows an important decrease in size while keeping a relatively high Q factor. Depending on the type of optical resonators (SiO_2 minisphere, or monocristalline disk) their optical quality factor can reach values from 10^8 to 10^{10} , which results in an equivalent Q from 10^4 to 10^6 at 20 GHz.

HIGH Q OPTICAL MINI-RESONATORS

The first step in this study has been to develop a measurement protocol in order to obtain the optical quality factor of the mini-resonators. Two measurement benches have been set-up to characterize various type of high Q optical mini-resonator: one based on the technique of cavity ring down in ENSSAT-FOTON, and the other one based on wavelength scan in LAAS-CNRS.

The LAAS-CNRS mini-resonator measurement bench has been described in details elsewhere [4]. It uses piezoelectric components which allow the control of the resonator coupling with a submicron scale precision in 3D displacement. Moreover, it protected from air flow and dust which could modify the coupling value and quality factor resonator value.

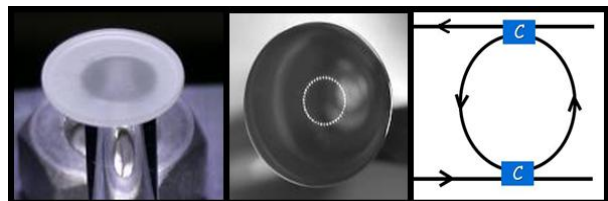


Figure 1: Quartz 7 mm minidisc (left), silica 3 mm minisphere (middle), and fiber ring resonator (right).

The resonators which have been characterized in this study are SiO₂ micro- and mini-spheres, a polished disk of monocrystalline material and a fiber ring resonator (figure 1).

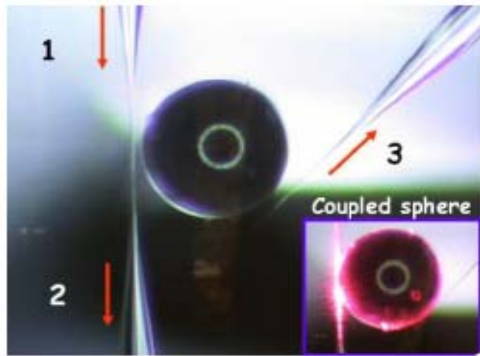


Figure 2: Microsphere of 400 μm diameter with a tapered and a half-tapered fiber coupling configuration. The laser is transmitted through the sphere from (1) to (3) and the uncoupled light can be measured in (2). Inset: microsphere coupled to a visible laser.

SiO₂ microspheres, realised in ENSSAT-FOTON, are formed by fusion and surface tension which confers to them a very good surface state. This type of resonator presents a very high Q , but the quality factor decreases if they are not isolated from humidity [5]. Experimentally, a Q factor larger than 10^9 has been demonstrated [6]. This Q factor is however limited by light absorption in silica. The diameters of the silica spheres realised are in the order of 400 μm, featuring therefore a mode spacing between the main modes of 160 GHz [4]. In figure 2, the way these resonators are coupled to optical fibers is shown.

In order to get a smaller mode spacing between the main modes, silica spheres with a larger diameter have been realized using a different technique based on a CO₂ laser. The size of these spheres is 3.3 mm in diameter, which leads to a mode spacing of 20 GHz. It is also coupled on the input side to a tapered fiber and on the output side, to an half tapered fiber. This coupling technique is efficient, but it is sensitive to vibrations.

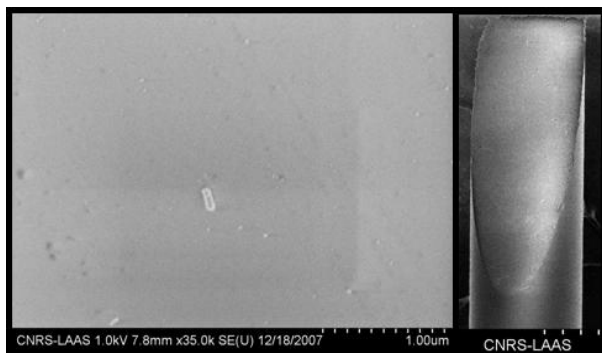


Figure 3: Angle polished fiber (right) and image of its surface quality (left) with SEM.

In addition to the well-known prism coupler, another technique which has been investigated is the one of the angle polished fiber. The results obtained currently with this technique are not satisfactory, but the improvement of the surface quality of these angle polished fibers is in

progress and the technique will be soon effective and more robust than tapered fiber. It is important especially in embedded systems. Such an angle polished fiber is show figure 3, together with SEM (Scanning Electron Microscopy) image of its polished surface.

In figure 4, whispering gallery mode (WGM) resonance of the 3.3 mm silica sphere is examined using the method of wavelength scan. The sphere is coupled using a biconic taper (waist < 2 μm). The WGM resonance is scanned by tuning over 6.5 GHz around $\lambda = 1550$ nm of a 100 kHz linewidth laser. We obtain a full width at half maximum (FWHM) of $\Delta f_{FWHM} = 830$ kHz, which corresponds to a quality factor of $Q = 2 \cdot 10^8$.

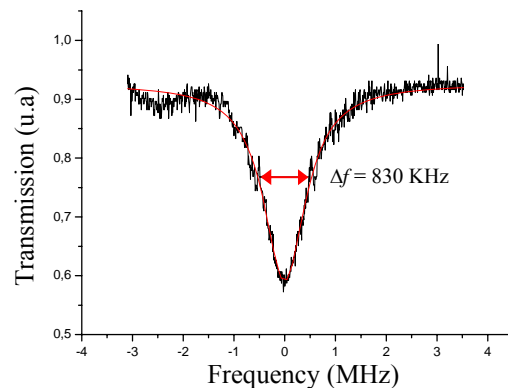


Figure 4: Experimental data (black curve) of the transmission response of 3.3 mm silica sphere with the method of wavelength scan. The red curve is the Lorentzian function approximation of the experimental curve.

An alternative to fused silica resonators is to use a monocrystalline material featuring very low optical losses. This approach theoretically allows higher Q factors, and the resonator is less sensitive to humidity absorption. However, the condition to reach high Q factors is to realize a good curved surface state on these resonators. A quartz disk resonator of 7 mm in diameter has been realized, corresponding to a mode spacing of 8 GHz.

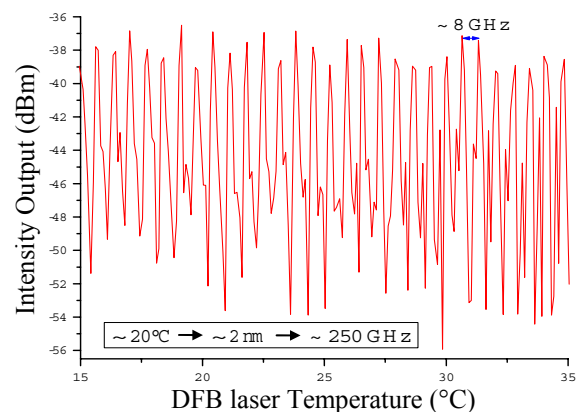


Figure 5: Experimental data of the transmission response of Quartz minidisc with wavelength scan with DFB laser. The minidisc is excited with the same coupling configuration described in the figure 2.

Figure 5 shows the main resonances of this resonator every 8 GHz on a 250 GHz bandwidth. To perform this measurement, a temperature tuned DFB laser has been used. However, the spectral linewidth of this laser is larger than the resonator half bandwidth. It is thus

impossible to estimate the optical quality factor for this resonator. This technique using the DFB laser allows to have only the resonances chart on a wide frequency range.

The last resonator which has been studied is a fiber ring resonator. It is formed by two optical waveguides coupled to a single fiber ring resonator. The first optical fiber loop realized has a total length close to 1 m, which leads to mode spacing of 205 MHz.

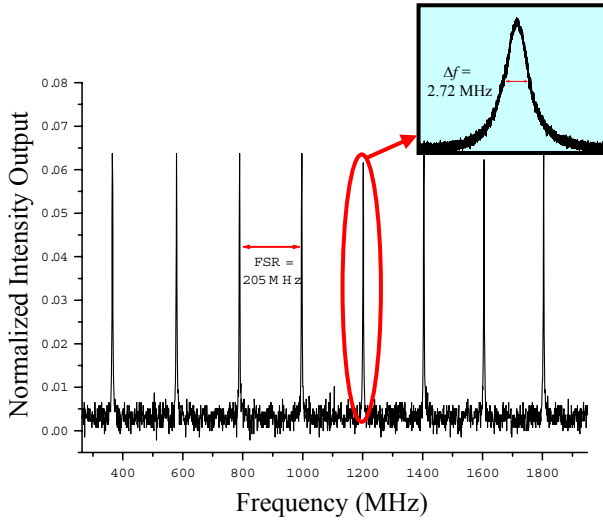


Figure 6: Experimental data of the intensity response of for fiber ring resonator with the method of wavelength scan. The resonances are scanned by tuning the laser temperature around $\lambda = 1550$ nm of a 1 kHz linewidth laser.

This type of resonator has an optical quality factor close to the one of the mini-resonators studied. Of course, the size of this resonator is larger than the 3D resonators, but it is a good test system to exhibit the problems of mini-resonator. For example, the dynamical thermal behaviour of an optical resonator and the hysteretic wavelength response have been observed with this resonator (see next paragraph). Moreover, its 2D shape makes its integration easy in a system where the equipments are assembled on a relatively large planar substrate (at least 10 cm x 10 cm). In figure 6, the 205 MHz spacing between the modes and the measurement of the Q factor are examined using the method of wavelength scan.

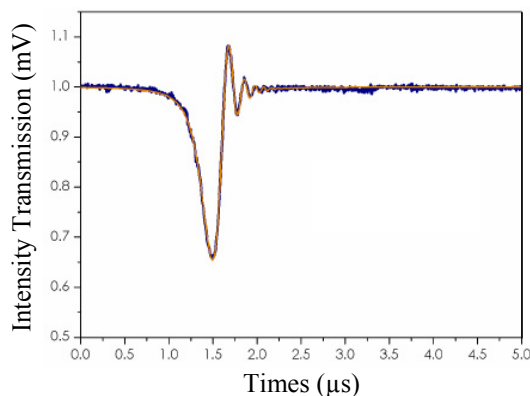


Figure 7: Experimental data (red curve) and theoretical model (blue curve) of the transmission response of fiber ring resonator with the method of cavity ring down

We obtain $\Delta f_{FWHM} = 2.72$ MHz which corresponds to a quality factor of $Q = 7.1 \cdot 10^7$. Figure 7 shows an example of cavity ring down measurement realised at ENSSAT-FOTON of the fiber ring resonator. By direct treatment of the exponential decay of the maxima [7], we deduce $Q = 7.5 \cdot 10^7$.

RESONATOR DYNAMICAL THERMAL-BEHAVIOR AND FEEDBACK CONTROL

It is difficult to get an efficient resonator coupling, because of the mode shift with temperature when the light is induced in the resonator. This is clearly seen in figure 8, which corresponds a thermal resonant-drift of optical fiber loop during wavelength scan. During the downscan, the resonance is narrowed. The reason for this behavior is that during the down wavelength scan the thermal effect is opposed to the laser shift. While the resonator frequency follows the laser frequency during the up wavelength scan. In the case, the resonance is expanded because of self heating.

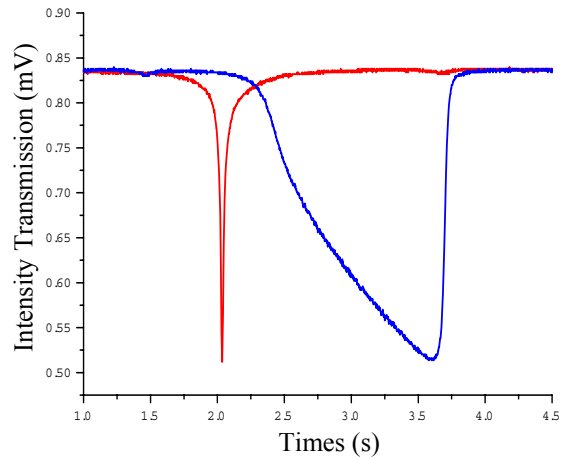


Figure 8: Dynamical thermal behaviour of fiber ring resonator during the up wavelength scan (blue curve) and during the down wavelength scan (red curve).

The solution to achieve maximum loading of the resonator is to lock the laser onto the resonator frequency. This has been realized using a Pound-Drever feedback loop [8, 9]. A schematic of the experimental setup is shown in figure 9. The validity of this approach has been verified experimentally on an optical fiber ring resonator.

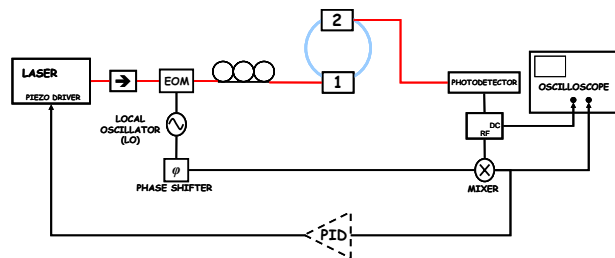


Figure 9: Detailed configuration of a Pound-Drever feedback loop with the fiber ring resonator.

When the Pound-Drever loop is closed, the resonator transmission is locked to its maximum value, ie the laser is locked onto the resonance. If the controller gain and

integration time of the proportional integrator differentiator (PID) have been correctly chosen, the correction maintains the laser locked onto the resonance for a long time [10]. Figure 10 shows the resonator transmission versus time, when the feedback Pound-Drever loop is closed or not.

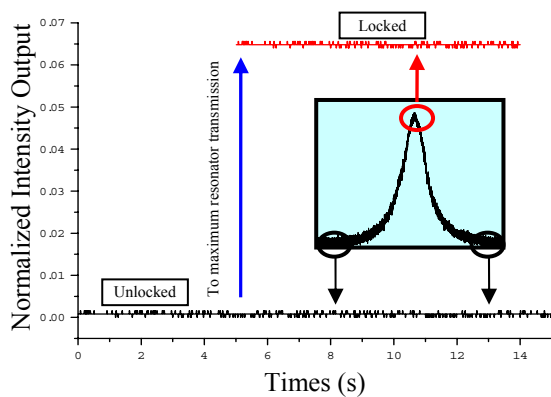


Figure 10: Experimental data of the intensity response of fiber ring resonator showing the laser locked onto the resonance (red) in comparison with Pound-Drever unlocked cavity (black).

As soon as the laser is locked onto the resonance, it is possible to use the system for microwave applications. For example, the optical fiber ring resonator can play the role of a microwave filter. For this, a Mach-zehnder modulator (MZM) must be added in the experimental setup described in figure 11.

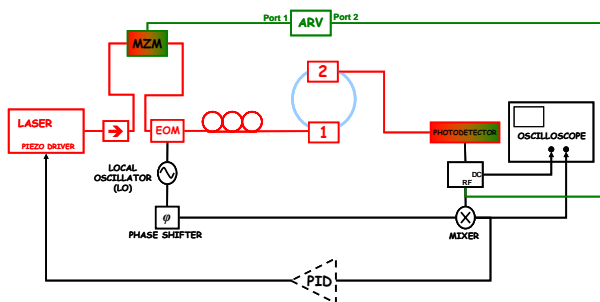


Figure 11: Detailed configuration of a microwave filter with the optical fiber ring resonator.

When the cavity transmission is locked to its maximum value, the RF or microwave modulation signal can be filtered by the optical resonator. The modulation goes through the two lateral side modes, and is filtered by these modes. Thus the optical transfer function is brought back in the microwave range. A high quality RF resonance is observed on the network analyser, featuring a spectral width of 2.4 MHz (figure 12).

Such a spectral width is interesting for microwave applications, and particularly in the upper microwave range (above 20 GHz) or in the millimetre wave range. As an example, it corresponds to a loaded Q factor of 10000 at 24 GHz, which is a value which cannot be obtained with conventional ceramic dielectric resonator.

Of course, our goal is to replace the fiber loop resonator by the mini-resonators. However, the results obtained with the fiber loop resonator are already interesting for applications, and the laser frequency stabilization approach studied with this resonator can easily be applied

to the case of the miniresonator.

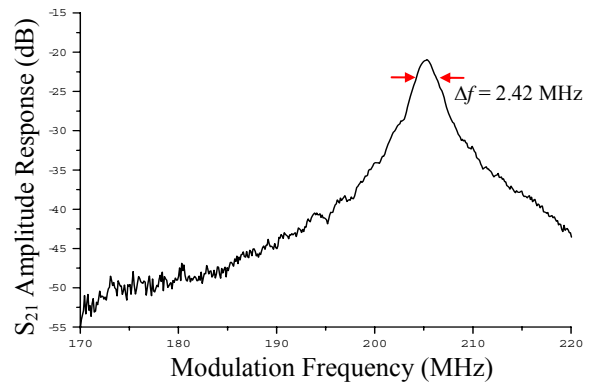


Figure 12: Measurement data of the amplitude response of S_{21} for the fiber ring resonator.

The next step will be to realize an optical-microwave oscillator with this resonator, such as the one depicted in figure 13. This oscillator should be competitive with classical microwave oscillators, because the additive phase noise of optical links is relatively weak [11].

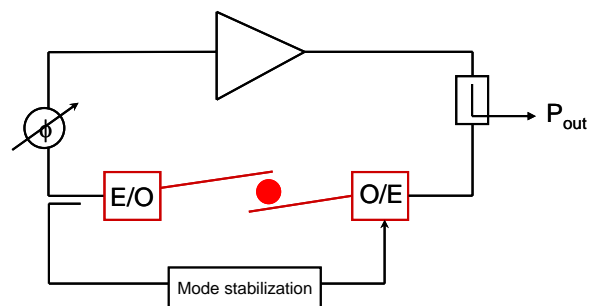


Figure 13: Configuration of optical-microwave oscillator with the different types of miniresonator.

The main noise contribution is the white noise floor due to the losses in the electrical to optical and optical to electric conversion, but the additive optical $1/f$ noise is surprisingly low [11]. If realized in the millimetre wave range, these oscillators will take benefit of the ultra high Q factor of the optical resonator and will thus exhibit an exceptional spectral purity.

CONCLUSION

In this paper, a characterization approach dedicated to microwave optical miniresonators and optical resonant fiber loops has been described.

This approach uses a high precision set up with nanometre scale control of the coupling factor (case of miniresonator) and a laser stabilization technique based on a Pound-Drever feedback loop.

The interest of the approach is demonstrated using a fiber loop resonator, with which a narrow band RF or microwave filter has been realized.

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