

# quantitative analysis of the critical current due to vortex pinning by surface corrugation.

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The transport critical current of a Niobium (Nb) thick film has been measured for a large range of magnetic field. Its value and variation are quantitatively described in the framework of the pinning of vortices due to boundary conditions at the rough surface, with a contact angle well explained by the spectral analysis of the surface roughness. Increasing the surface roughness using a Focused Ion Beam results also in an increase of the superficial critical current.

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## INTRODUCTION

The understanding of the nature of the critical current in superconductors has triggered a lot of work for many years [1, 2]. Practically speaking, quantitative predictions of the critical current values is a key point for most of the applications. More fundamentally, the question of the interaction of the vortex lattice with pinning centers is also a prototype system for understanding the behaviour of an elastic medium submitted to a disorder potential [3]. It is well known that a perfect vortex lattice (VL) submitted to a bulk transport current is subject to a flow, that leads to a finite electro chemical field and gives rise to dissipation [4]. The ability of the VL not to move when it is submitted to a transport current is generally explained by the pinning interactions between pinning centers and VL. Unfortunately, the exact nature of the pertinent pinning centers, and the way they are acting, is not straightforward. In soft samples where superconducting parameters vary slowly in the sample, cristallographic bulk inhomogeneities are usually supposed to play the role of pinning centers [2]. One can notice that this collective bulk pinning description leads to quite complex critical current expressions and to a corresponding lack of quantitative interpretation and prediction. On the other hand, experimental observation of the strong influence of surface quality on VL pinning has been evidenced in pioneering experiments [5]. This surface influence can be described in the framework of surface roughness interacting with VL, as proposed by Mathieu-Simon (MS) in a continuum approach. For any real sample, which presents a surface roughness at the VL scale, the respect of the boundary conditions [6] of terminating vortices at the surface imposes local bending. This defines a contact angle  $\theta$  ( $\theta=0$  for a flat surface) and leads to a near-surface supercurrent. At the sample scale, this offers a lot of metastable equilibrium states. The ability of the system

to sustain a macroscopic supercurrent is then directly linked to the surface roughness via an average contact angle  $\theta_c$ . The macroscopic critical current (per unit of width) is simply given by

$$i_c(A/m) = \varepsilon \cdot \sin(\theta_c) \quad (1)$$

where  $\varepsilon$  is the vortex potential, i.e. the thermodynamical potential describing the equilibrium state. "Pinning" is then nothing else than the consequence of vortex boundary conditions applied to a real surface [8]. This should a priori act in every sample. The remaining question is: what is the contribution of this surface critical current with respect to the overall critical current? The vortex potential can be measured from the reversible magnetic moment  $M = -\int_V \varepsilon \delta V$  of a superconducting volume  $V$ , or calculated using, for example, Abrikosov's solution close to  $B_{c2}$ . Using an iteration procedure proposed by E.H. Brandt [10],  $\varepsilon$  can be also obtained over the whole mixed state via numerical solutions of the Ginzburg-Landau equations. Now if one assumes a physical value of  $\theta_c = 0-20$  deg, a good order of magnitude of  $i_c$  is deduced [9]. A careful inspection of the surface state should in principle enable to extract a more precise value of this critical angle. If the usual measurement of surface roughness is the rms (root-mean-square) height  $h$  of the surface bumps, the pertinent parameter is here more the distribution  $\theta(x) = \arctan(\frac{dh}{dx})$  of local slopes over the width of the surface. The rms value of this angle is given by the integration of the spectral density  $\overline{\theta^2} = \int_{k_{min}}^{k_{max}} S_{\theta\theta} dk$  over the appropriate  $k$  boundaries [11].  $S_{\theta\theta}$  is the Fourier transform of the autocorrelation of  $\theta(x)$  (Wiener-Khintchine theorem), which represents the spatial distribution of  $\theta$ . The aim of the present study is to measure the critical current of a Niobium thick film, with various surface corrugation, and to compare the experimental values to those obtained with the

simple expression (1).  $\varepsilon$  will be calculated using Brandt's approach, and  $\theta_c$  compared to  $\sqrt{\overline{\theta^2}}$ .

## EXPERIMENTAL

The sample used is a film of Niobium (thickness= 3000 Å) deposited at 780C on a sapphire substrate by the ion beam technique. The film has a resistivity of about 0.5  $\mu\Omega$ .cm at the critical temperature  $T_c = 9.15$  K and exhibits a low surface rms roughness ( $R_a \lesssim 5$  nm), measured by Atomic Force Microscopy (Nanoscope III, Digital Instruments). Microbridges of  $W=10 \mu\text{m} \times L=30 \mu\text{m}$  have been patterned using a scanning electronic microscope, this irradiation step being followed by a reactive ion etching process. The critical currents have been measured by mean of the standard four-probe technique, at the following temperatures of 4.2, 5.2, 6.2 K in the whole range of field covering the mixed state. The critical current values  $I_c$  were determined with a voltage criteria of 10 nV.

## RESULTS AND DISCUSSION

Let us first discuss the general behavior of the  $I_c(\omega)$  data (fig.1) for the virgin microbridge at different temperatures ( $\omega$  is the vortex field inside the sample and corresponds to the vortex density  $n=\frac{\omega}{\phi_0}$ ). Note that the demagnetization factor due to the geometry of the thin film renormalizes the apparent first critical field  $B_{c1}$  up to about 0.015  $B_{c1bulk}$ . It implies that the mixed state is created for the lowest field value applied ( $\approx 30Gauss$ ). Except for this peculiarity,  $I_c(\omega)$  exhibits the same field variation as the reversible magnetization curve of a type II superconductor, in agreement with the expected variation of superficial currents  $i_c$  (equation 1 with  $\theta_c \approx cte$ ). We also notice that the curves taken at 4.2, 5.2 or 6.2 K are self similar, that is they can be superimposed by a mere rescaling. As first noted in pioneering work on vortex pinning [12], the change of critical current with temperature can be totally attributed to the change in primary superconducting properties. It is evidenced in figure 2 where the low field value of  $I_c$  is shown to be simply proportional to  $B_{c2}$  for the three temperatures and both for the virgin and for the damaged sample. This shows that the variation of  $I_c$  with temperature is simply due to the variation of the vortex potential  $\varepsilon(T)$  (i.e. the variation of superfluid density), without the need of involving other thermal effects such as vortex thermal diffusion. Now if we want to verify quantitatively equation (1), we first need to know the vortex potential  $\varepsilon$ . It is usually approximated using the Abrikosov calculations from  $B_{c2}$  down to 0.4-0.5  $B_{c2}$ , and by the London expression at very low fields  $B \gtrsim B_{c1}$ . For low kappa superconductors such as pure Niobium ( $\kappa \approx 1$  for a sample with properties

very close to ours [13][14]), only the Abrikosov expression is quantitatively correct and it is necessary to use numerical calculations to solve the Ginzburg Landau equations over the whole field range, following for example Brandt's iterative method [15]. The result is presented in figure 3, for  $\kappa = 1$ . We can now deduce the critical angle needed to account for the measured critical current. For a pure surface pinning and following equation (1), the expected value of  $\theta_c$  is given by  $\theta_c \approx \arcsin(i_c/\varepsilon)$ . Using the numerical values of  $\varepsilon$ , we find  $\theta_c \approx 0.4-1$  deg (see figure 4), in agreement with the mere expectation of a physical angle. The order of magnitude is promising, but the complexity of the (multiscale) surface disorder needs a careful surface analysis. We have therefore measured the microbridge roughness using AFM in tapping mode (see fig. 5).

Following the simple analysis described in the introduction, we obtain the spectral density  $S_{\theta\theta}$  with the use of the Fourier transform of the autocorrelation of  $\theta(x)$  (Wiener-Khintchine theorem). The main value of the statistically representative angle is given by the integration of the spectral density [11]:  $\overline{\theta^2} = \int_0^{k_{max}} S_{\theta\theta} dk$ . The boundary of the integral have been chosen as the natural scale for the vortex lattice, considering that a vortex does not see a roughness less than its core size ( $k_{max} = \frac{2\pi}{\xi}$ ). Note that the choice of this cutoff frequency does not significantly change the results. This calculation gives  $\sqrt{\overline{\theta^2}} \approx 0.60 \pm 0.18$  deg. The agreement with the value deduced from the critical current measurements (a mean value of  $0.70 \pm 0.15$  deg) is quite promising. More precisely, this is, within error bars, what we obtained for the magnetic field values higher than about 1000 Gauss. It is worth noting that the main value that we calculate is statistically representative but gives also a value that is supposed to be independent of the frequency. We are fully aware that a more rigorous analysis should take into account a kind of matching effect between the VL periodicity and the scale of surface disorder. It is even possible to expect a peculiar variation of  $i_c(\omega)$  in the case of a very rough surface at a restricted spatial scale. In this respect, one can see that the highest angles observed for low fields  $B \lesssim 0.1$  T ( $a_0 \gtrsim 0.5 \mu\text{m}$ ) are quite consistent with the highest angles observed in the surface profile for a periodicity of about  $1 \mu\text{m}$ .

We decided also to compare this virgin microbridge with one whose surface structure was modified. The idea was to use a Focused Ion Beam to etch its surface following a controlled geometry. The expected shape was that of "corrugated iron" with  $12 \mu\text{m}$  by  $0.1 \mu\text{m}$  trenches regularly spaced by  $1 \mu\text{m}$ . Also, the etched depth should be high compared to the initial roughness of the surface, that is 30nm here. Several attempts have been performed using different Ga ion doses, which should be as low as possible in order to minimize the effect of Ga irradiation, leading to the best control of the etched surface. Thus,

the final procedure was eight identical patterns ( $12\mu\text{m} \times 0.10\mu\text{m} \times 0.03\mu\text{m}$ ), etched parallel using an ion current of 4 pA corresponding to a total ion dose about  $150 \text{ pC}/\mu\text{m}^2$ . The sample was tilted by 45 degrees and the magnification used was 25kX. Figure 6 is a SEM image of the resulting etched microbridge; the trenches are evenly spaced and they yield geometric parameters close to those expected (width about  $0.15 \mu\text{m}$ ). Such low energy irradiation leads also to an implantation of  $\text{Ga}^+$  ions, but simulations using Monte-Carlo calculations [16] indicate that it affects only a range of no more than  $100 \text{ \AA}$ . Furthermore, we observe neither any change in the critical temperature ( $T_c = 9.15\text{K}$ ), nor in the normal state resistivity ( $\rho_n \approx 0.50\mu\Omega.\text{cm}$ ) and critical fields within experimental accuracy. In order to evaluate more precisely the influence of the Ga irradiation, another microbridge was etched using a single rectangular pattern ( $12\text{m} \times 8\text{m} \times 0.03\text{m}$ ), that is covering the whole width of the microbridge. The sample was tilted of 45 and the total ion dose close to  $190\text{pC}/\mu\text{m}^2$ . Critical current and resistivity measurements were performed on this microbridge and were compared to those on the virgin microbridge. We observed the same properties and specially that the critical current is very similar (within few percents) in the two cases. This confirmed that the Ga irradiation had no influence on the bulk physical properties of the film. The FIB treatment, contrary to highest energy irradiation, has not modified the bulk crystalline lattice of the material and that the important modification is in the surface structure. We can therefore use the term "surface" damages. The main obvious result is the increase of the critical current, as shown in fig. 7. Following the same procedure that we performed for the virgin microbridge, one obtains  $\sqrt{\theta^2} \approx 2.2 \pm 0.3 \text{ deg}$  in good enough agreement with the  $1.5 \pm 0.2 \text{ deg}$  deduced from the critical current values. We note that the kind of treatment we performed leads to an increase of the roughness for a periodicity of about  $0.1\text{-}1 \mu\text{m}$ . In the inset of figure 7, one can evidence that the critical angle is almost unchanged for the highest magnetic field values  $\omega \gtrsim 3000 \text{ G}$ . For those values, the intervortex distance is less than  $0.1 \mu\text{m}$  and we find using the AFM that the treated microbridge exhibits the same kind of roughness as the virgin microbridge for this periodicity. Again, the spatial dependence of the surface roughness is certainly linked with the exact  $\theta_c(\omega)$  variation, with  $\omega$  fixing the spatial scale of the pertinent surface disorder. More work is needed to fully describe this problem.

Finally, we conclude from this analysis that the critical current of our sample is given by equation (1) with a good agreement, for the virgin and for the surface damaged microbridges. We conclude that taking into account the surface defects as main sources of pinning enables to explain the experimental critical current values. Expressed in the form of a surface critical current and due to the

small surface corrugation of the Nb Film (a roughness of few nm rms), the critical current appears to have standard and even relatively small values for this low kappa superconductor ( $i_c \approx 10\text{-}30 \text{ A/cm}$  at low fields). If one expresses the critical current in the form of a density as it is usually made, this leads to a high value ( $J_c \approx 0.5 - 1.5 \cdot 10^6 \text{ A/cm}^2$ ). We emphasize that this notion of density is by definition not justified in the case of a current flowing under the surface and not uniformly in the bulk. As an example, Niobium crystals with a thickness of  $7.6 \cdot 10^{-3} \text{ cm}$  exhibit a critical current density of roughly  $3.10^3 \text{ A/cm}^2$  at  $0.1 \text{ T}$  and  $4.2 \text{ K}$  [17]. This gives  $i_c=13.1 \text{ A/cm}$  compared to  $12.5 \text{ A/cm}$  (our thin film) under the same ( $\omega, \text{T}$ ) conditions. So, The surface critical current is almost the same. It follows that the difference of thickness makes this apparent (but not physically significant in terms of pinning "force") difference in the critical current density values. Note that the same remark apply to other types of clean superconductors [18].

Now, if one increases a lot the number of bulk defects to obtain a spacing say less than the intervortex distance, we can obtain a so-called hard superconductor. In this case, a bulk subcritical current can flow by a percolating-like behavior. Anyway, in this case, the critical current density was shown, in a lot of cases, to be proportional both to the difference in equilibrium magnetization across the internal boundaries and to the area of internal interface per unit volume [19, 20, 21]. It is worth noting that this is the same kind of pinning by surface interactions, but in this case with internal interfaces.

In summary, we have observed that the value of the critical current of a thick film of a standard type II superconductor is quantitatively explained with the vortex pinning by surface roughness. We have also observed the increase of this critical current caused by an increase of the surface corrugation. Furthermore, it gives a simple explanation for the high critical current density observed in this kind of clean thin films, compared to the moderated one observed in (thick) bulk crystals. We hope that it gives also evidence that the interaction between the surface corrugation and the vortex elasticity is a key point for the understanding of vortex lattice pinning and dynamics.

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FIG. 1: The critical current of the virgin niobium microbridge as function of the vortex field for three different temperatures.

FIG. 2: The critical current at 30 Gauss as function of the second critical field for the three temperatures and the virgin and surface damaged microbridges.

FIG. 3: The variation of the vortex potential (or equilibrium magnetization) as function of the magnetic field for  $\kappa=1$  calculated with Ginzburg-Landau equations and following the method explained in [10]. The two are respectively normalized over  $H_{C2}$  and  $B_{C2}$ . The dashed line is the Abrikosov line.

FIG. 4: The variation of the critical angle  $\theta_c$  deduced from the  $\arcsin(\frac{i_c}{\epsilon})$ . The straight line corresponds to the main value extracted from the surface analysis.

FIG. 5: AFM picture of the surface roughness for the virgin microbridge. In the inset is shown the corresponding variation of local slopes  $\theta$  over the width of the sample.

FIG. 6: a/ SEM image of the treated microbridge showing the eight trenches (arrowed) in the niobium film. b/ Detail of one trench showing its geometric characteristics.

FIG. 7: comparison of the critical currents for the virgin microbridge and for the one degraded with the FIB. In the inset is shown the critical angle variation deduced from equation (1).